

**VILLAGE PARKWAY  
TENTATIVE SUBDIVISION MAP**

Prepared by:



**March 8, 2021**

# **VILLAGE PARKWAY**

## **TENTATIVE SUBDIVISION MAP**

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**March 8, 2021**



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## VILLAGE PARKWAY TENTATIVE MAP

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Washoe County Assessor’s Office Map

## VILLAGE PARKWAY TENTATIVE MAP

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### **Attachments:**

Preliminary Engineering Plans  
Preliminary Engineering Reports  
Preliminary Landscape Plan  
Preliminary Geotechnical Investigation  
Traffic Impact Analysis

# VILLAGE PARKWAY TENTATIVE MAP

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## Introduction

This application includes the following request:

- A **Tentative Subdivision Map** to allow for 166 detached single family units and 183 attached single family units in the High Density Suburban (HDS) regulatory zone.

## Project Location

The Village Parkway properties (APN #'s 087-400-11, 23, and 24) consist of 124.6± acres located on the west side of Village Parkway, north of Cold Springs Drive in the Cold Springs Area Plan. Mud Springs Drive (private) traverses the site along the eastern property boundary. Figure 1 (below) depicts the project location.

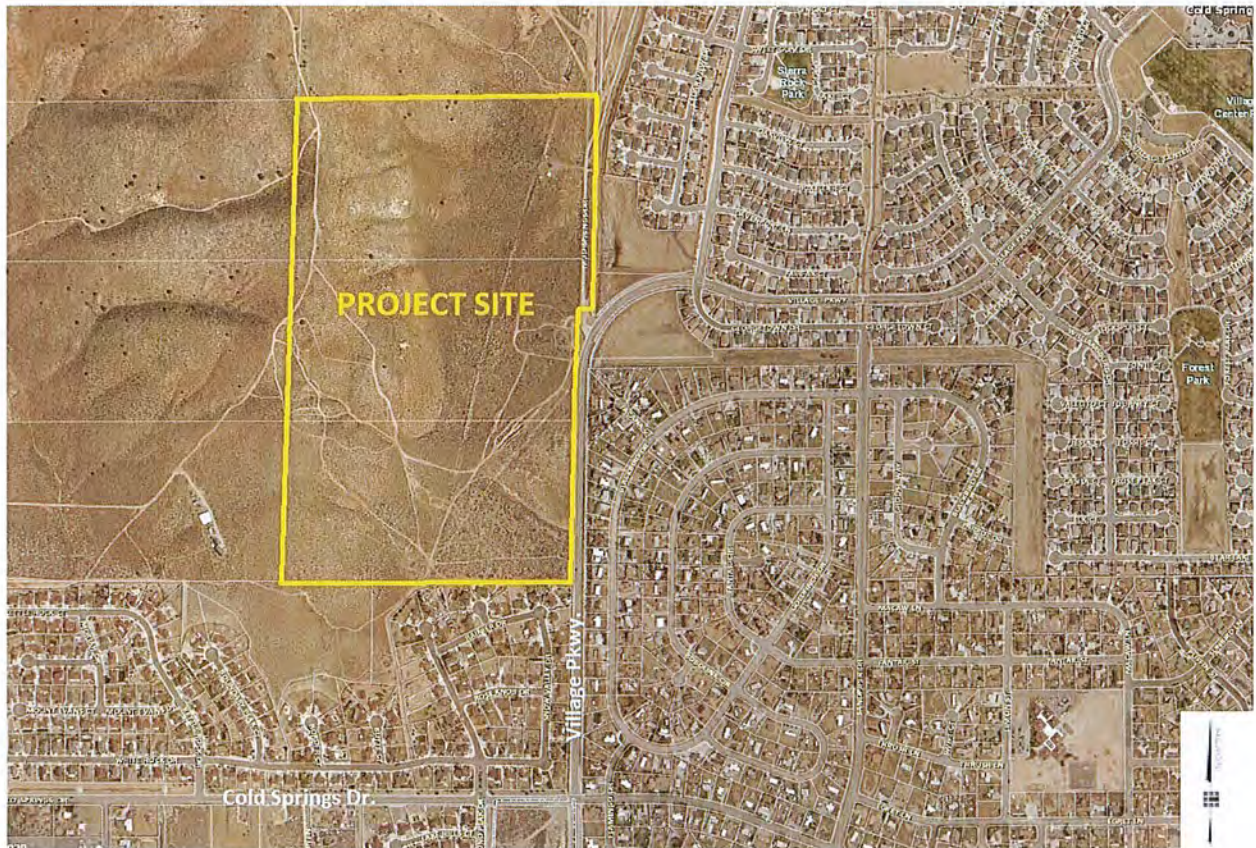


Figure 1 – Vicinity Map



# VILLAGE PARKWAY TENTATIVE MAP

## Existing Conditions

Currently, the project site is vacant. The western side of the properties is characterized by steep slopes and a ridgeline that separates the parcels from large lot residential uses to the west. The eastern portion of the property is relatively flat and easily accessed from Village Parkway. Surrounding land use included single family suburban residential to the east, south, and northeast, and large-lot residential to the north and west.

The site topography is reflected in the current Master Plan designations for the site. The western portions of the property are designated as Rural while the eastern half of the site is Suburban Residential. Figure 2 (below) depicts the existing Master Plan designations for the site and surrounding area.

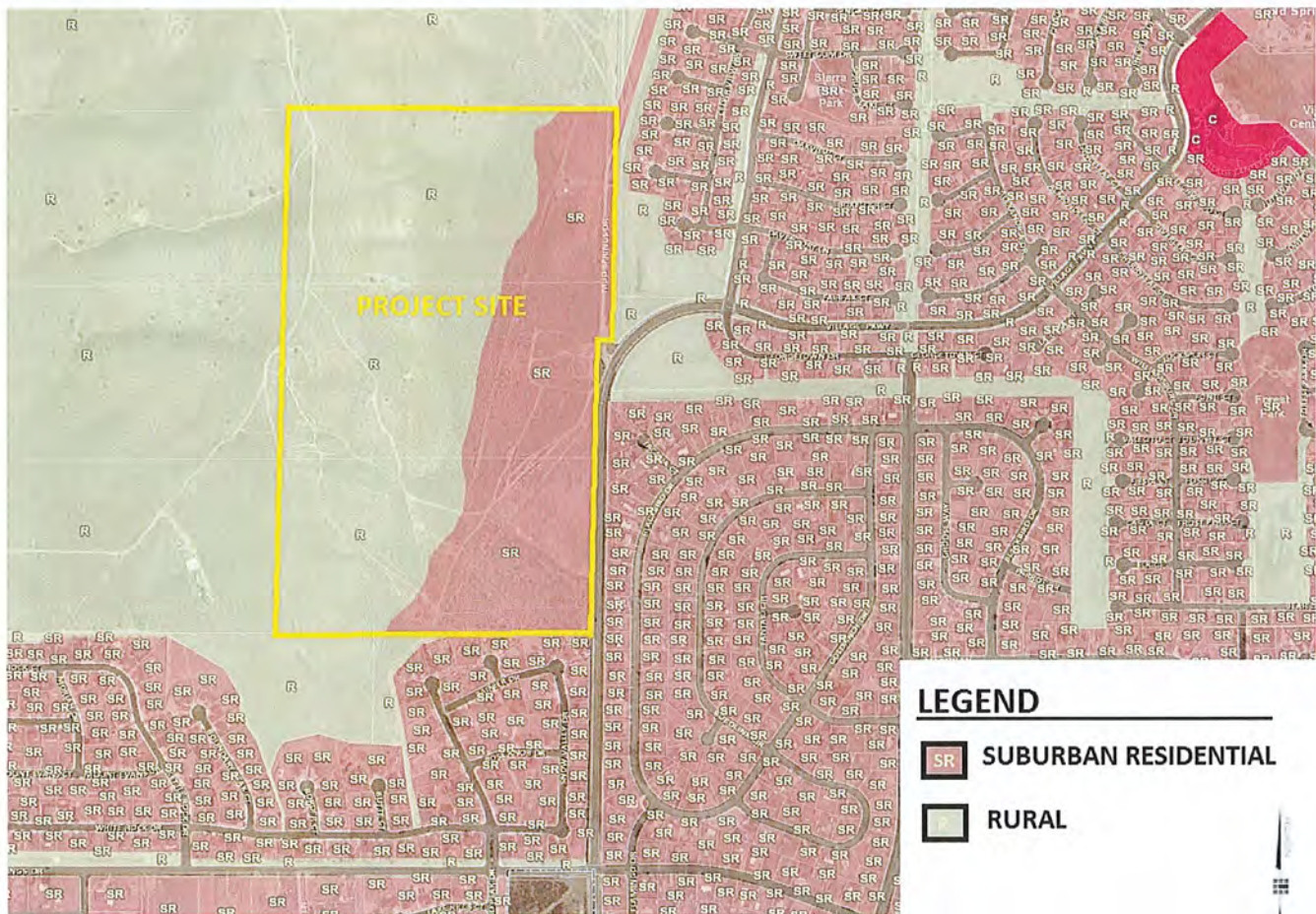


Figure 2 – Master Plan Land Use



## VILLAGE PARKWAY TENTATIVE MAP

The project site includes split zoning. The western side of the property is zoned General Rural (GR) while the eastern portion of the site is designated as High Density Suburban (HDS). The HDS portion of the site includes 47.2± acres of HDS zoning which allows for 7 dwelling units per acre for detached single family and 9 units per acre for attached single family use.

Figure 3 (below) depicts the existing site zoning.

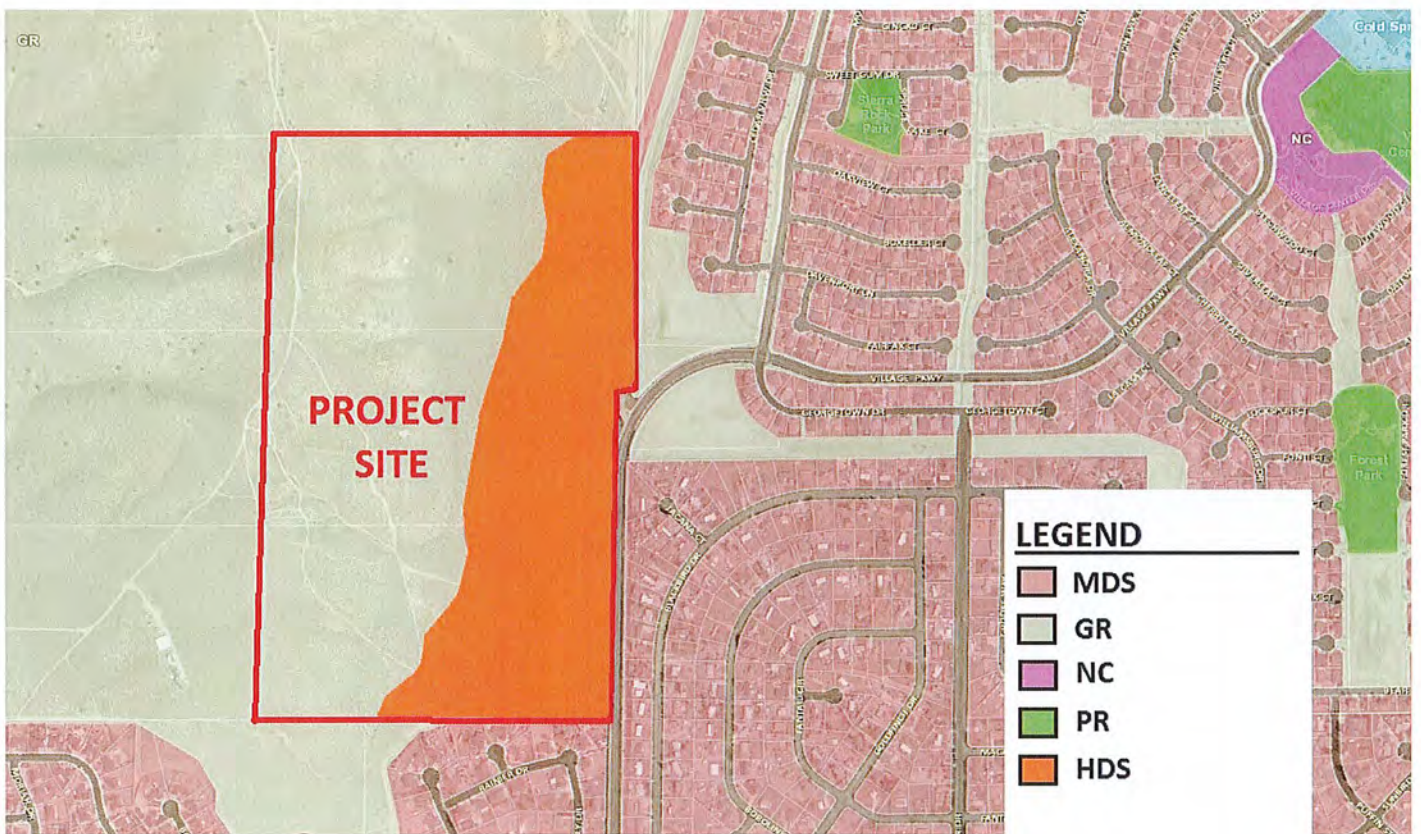


Figure 3 - Zoning



## VILLAGE PARKWAY TENTATIVE MAP

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Figure 4 (below) and 5 (following page) depict the existing onsite conditions.

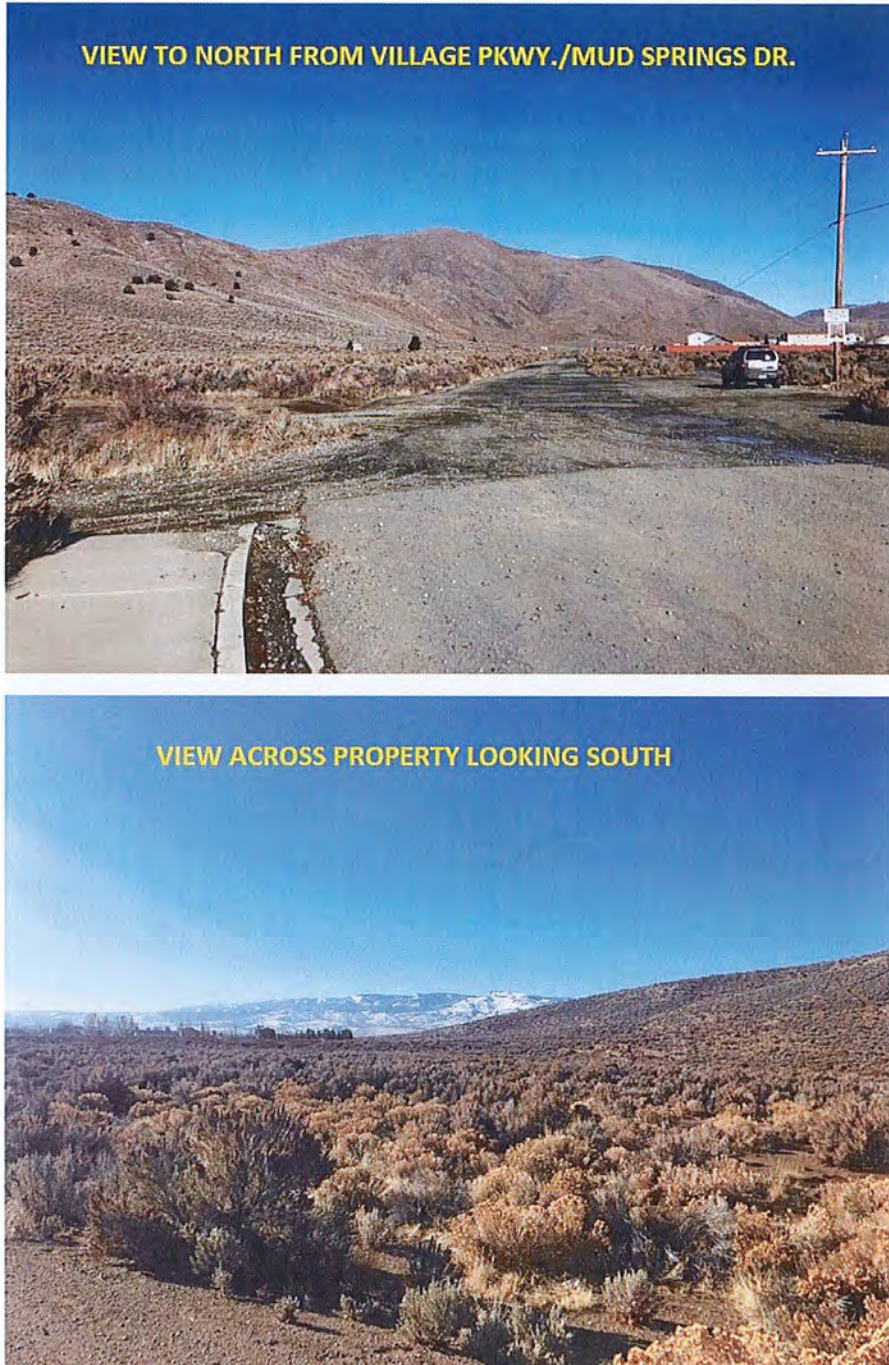


Figure 4 – Existing Conditions



## VILLAGE PARKWAY TENTATIVE MAP

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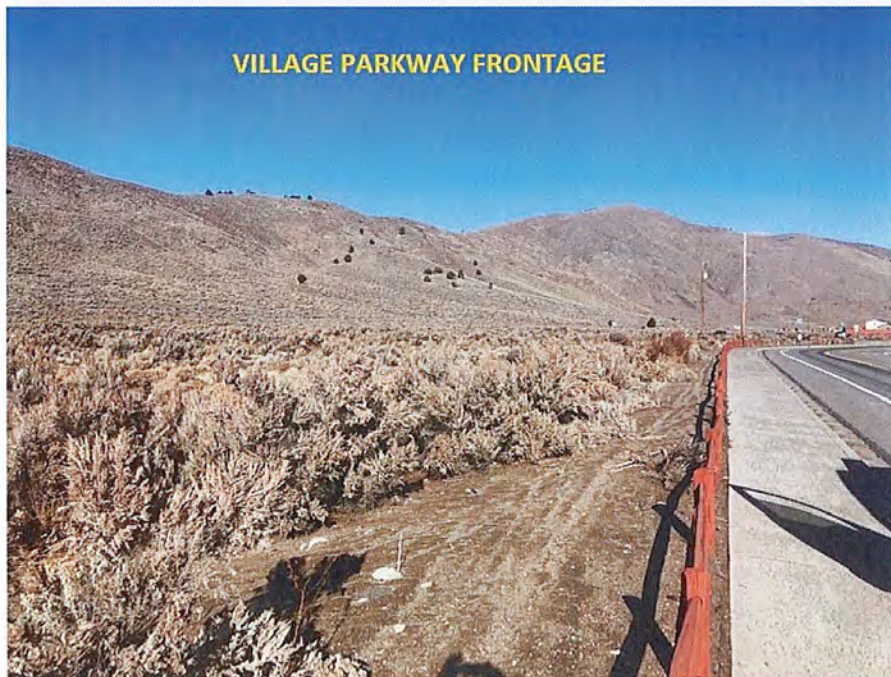
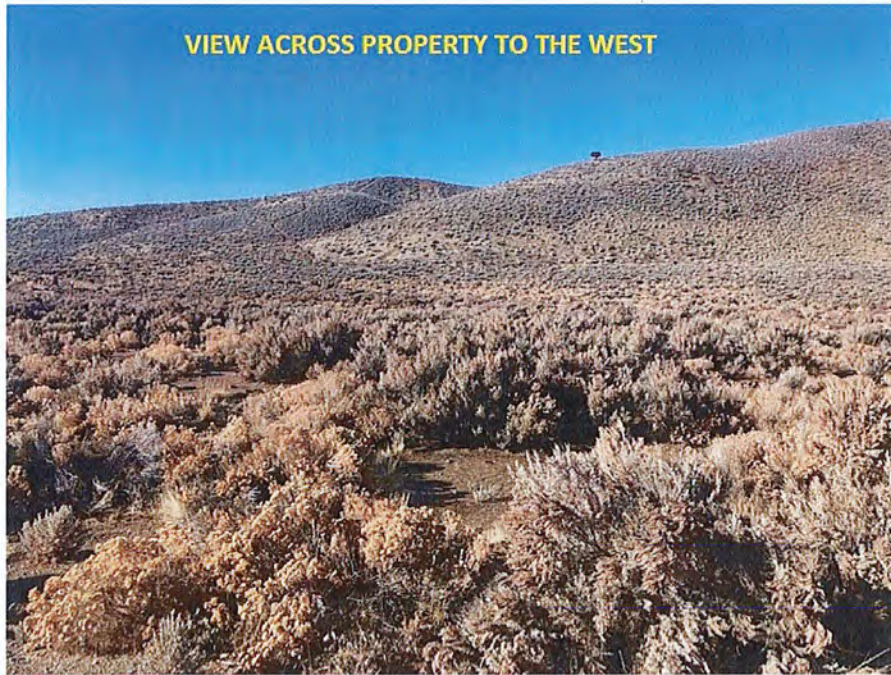


Figure 5 – Existing Conditions



## VILLAGE PARKWAY TENTATIVE MAP

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### Request Summary

This application includes a request for a Tentative Subdivision Map to allow for a mix of attached and detached single family units totaling 349. Attached single family product (townhomes) is clustered at the southern portion of the project site with detached single family units located at the central and northern portions of the project area. The project utilizes a Common Open Space Development concept which preserves the General Rural (GR) zoned portion of the site and steeper slopes located at the west side of the existing parcels. Units are proposed to be clustered within the HDS zoning area.

Primary access to the project will be via a new divided entry along Village Parkway. This entry will serve as the primary access for both the townhome and detached units. Two secondary emergency access roads located at the southern boundary and north-central portion of the site will provide additional connection to Village Parkway ensuring all emergency access requirements are met. The secondary access roads will be gated to limit access to emergency vehicles only.

The Village Parkway Tentative Map is somewhat unique in that it provides for two distinct housing types. Townhome units will be located at the southern portion of the project site and are designed to face landscaped common areas/paseos within the project. These common areas create an attractive outdoor living space for residents and encourage outdoor gathering, recreation, etc. The design of the townhome portion of the tentative map includes alley-loaded garages. As a result, building facades facing the landscaped paseos are not dominated by garages and provide for a safe pedestrian environment free of vehicles.

Townhome units are expected to range in size from 900± square feet to 2,000± square feet and will include a mix of one, two, and three story floorplans (not to exceed 35 feet in height). Alleyways within the townhome area will be private and maintained by a homeowner's association (HOA). The HOA will also be responsible for the ongoing maintenance of paseos, landscape common areas, and exterior maintenance of units. A separate HOA for the townhome units (not to include the single family detached units) may be enacted with final map.

Each townhome unit will include a garage along the internal alleys. Additionally, parking "pods" are provided and dispersed throughout the community within proximity to units, providing guest and visitor parking. Parking areas are located to not interfere with paseo functionality and include an additional 114 spaces, ensuring all Washoe County Development Code requirements are satisfied. A parking summary is also included on the attached site plan.

Townhomes will share a common wall(s) with adjoining units. As attached single family products, residents will own the individual parcel of land on which the townhome is located. The townhome concept serves to diversify residential offerings within Cold Springs and broadens home ownership opportunities for residents in the area by offering a lower maintenance, more affordable housing option. A total of 183 townhome units are proposed.

# VILLAGE PARKWAY TENTATIVE MAP

Figure 6 (below) depicts the preliminary site plan for the Village Parkway Tentative Map. A full size copy of the plan is included as an attachment to this report.



### GENERAL NOTES

- 1) ALL PLANTING AND IRRIGATION SHALL BE INSTALLED PER LOCAL GOVERNING CODES.
- 2) TREES
  - ONE HALF OF ALL DECIDUOUS TREES SHALL HAVE A MINIMUM CALIPER OF 2 INCHES THE REMAINING MAY HAVE A CALIPER OF 1" AT TIME OF PLANTING.
  - ONE HALF OF ALL EVERGREEN TREES SHALL HAVE A MINIMUM HEIGHT OF 7 FEET, THE REMAINING MAY HAVE A HEIGHT OF 5 FEET AT TIME OF PLANTING.
- 3) FINAL PLANT SELECTION AND LAYOUT WILL BE BASED ON SOUND HORTICULTURAL PRACTICES RELATING TO MICRO-CLIMATE, SOIL AND WATER REGIMES. ALL TREES WILL BE STAKED SO AS TO REMAIN UPRIGHT AND PLUMB FOLLOWING INSTALLATION. PLANT SIZE AND QUALITY AT TIME OF PLANTING WILL BE PER THE AMERICAN STANDARD FOR NURSERY STOCK (ANSI Z60.1-1990).
- 4) ALL SHRUB BEDS WILL RECEIVE 4" DEPTH MULCH WITH WEED CONTROL.
- 5) ALL LANDSCAPING WILL BE AUTOMATICALLY IRRIGATED. CONTAINER PLANTINGS WILL BE DRIP IRRIGATED BASED ON THE SPECIFIC HORTICULTURAL REQUIREMENTS OF EACH SPECIES. A REDUCED-PRESSURE-TYPE BACKFLOW PREVENTOR WILL BE PROVIDED ON THE IRRIGATION SYSTEM AS REQUIRED PER CODE.
- 6) PLAN IS CONCEPTUAL. PLANT QUANTITIES INDICATED ARE PER CITY OF RENO CODE REQUIREMENTS. PLANT LOCATIONS, FINAL SPECIES SELECTION AND SIZE AT PLANTING SHALL BE DETERMINED DURING DEVELOPMENT OF THE FINAL CONSTRUCTION DOCUMENTS.

### PLANT LEGEND

- FLOWERING TREE
- DECIDUOUS SHADE TREE
- EVERGREEN TREE
- COMMON AREA LANDSCAPING
- STREETSCAPE
- RE-VEGETATION AREA

### LANDSCAPE DATA

- DEVELOPMENT SITE AREA = 2,034,819 SQ FT (46.7 ACRES)  
 ZONING: HDG (HIGH DENSITY SUBURBAN)  
 TOWNHOME REQUIRED LANDSCAPE AREA = 146,400 SQ FT (3.36 ACRES) MIN.  
 (20% OF TOWNHOME DEVELOPMENT SITE 732,000 SQ FT (16.8 ACRES))  
 INCLUDES
- COMMON AREA LANDSCAPE
  - FRONT, BACK AND SIDE YARDS WHERE ADJACENT TO THE STREET
  - STREETScape ALONG WOODLAND VILLAGE PARKWAY - 1 TREE PER 50 LN FT
- SINGLE FAMILY
- 1 TREE PER LOT OR 80 LN FT OF STREET FRONTAGE FOR FRONT AND SIDE YARDS
  - 1 TREE PER 50 LN FT ALONG WOODLAND VILLAGE PARKWAY
- PARKING TREES REQUIRED
- 1 TREE PER 20 LN FT IN OFF-SET ROWS FOR PARKING SCREENING BETWEEN MF AND SF
  - 1 TREE PER 10 PARKING SPACES
- NOTE: FINAL NUMBERS OF TREES SHOWN IN COMMON AREAS TO BE DETERMINED DURING FINAL DESIGN.

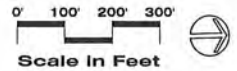


Figure 6 – Preliminary Site Plan



## VILLAGE PARKWAY TENTATIVE MAP

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As Figure 6 depicts, detached single family units are located at the central and northern portions of the tentative map area. The detached units take on a more traditional neighborhood concept and include lots sizes ranging from 3,645± square feet to 8,257± square feet. New units will be accessed via an internal street network with no units accessed directly from Village Parkway. Roadways within the detached unit area will be public and are designed to Washoe County standards. In all, a total of 166 detached units are proposed.

Grading of the project site will include cutting into a small portion of the GR zoned property located on the west side of the tentative map area to provide fill within eastern portions of the site. In accordance with Washoe County grading standards, cuts will be less than 10 feet in height and will be screened from the view of Village Parkway by the intervening homes. No units are proposed within the GR zoned portion of the existing parcels. Improvements within the GR area include limited grading along the eastern edge as well as a portion of roadway that will provide access to detached units at the north end of the site.

Landscaped common area will be located along the Village Parkway frontage. This will provide for a visually appealing streetscape and incorporates required onsite detention. Additionally, a larger detention basin, central to the project site, is located at the western side of the tentative map area to ensure all Washoe County requirements related to stormwater and drainage are implemented. Similar to the Village Parkway frontage, the detention area will include landscaping and is incorporated as a community amenity. Landscape improvements and detention areas are located within dedicated common area and will be maintained by the project HOA. A trail (as shown on the attached plans) will be included at the western side of the site, connecting to open space areas to the west.

The project will be constructed in phases. Townhomes and detached products may be phased separately but could include concurrent phases of development. It is anticipated that each product type may include up to 4 individual phases with project buildout estimated at 5 to 7 years.

The current HDS zoning allows for up to 9 units per acre for attached single family and 7 units per acre for detached single family housing. Thus, under the current conditions, up to 424 units could be developed at the project site. Under the proposed mix, 349 units are proposed. The townhome portion of the project accounts for approximately 45% of the site area (21.24± acres), resulting in a proposed density of 8.6 units per acre. Detached single family products account for the remaining 25.96± acres of the site, resulting in a detached density of 6.4 units per acre. Overall project density is 7.4 dwelling units per acre. This is fully compliant with the existing HDS zoning and Suburban Residential Master Plan designation.

Per the Common Open Space Development provisions of the Washoe County Development Code, units are clustered within the portion of the site zoned HDS which includes approximately 47.2± acres. The remaining 77.4± acres zoned GR will be dedicated as open space with no future development. Therefore, the overall gross density for the project is 2.8 dwelling units per acre.

## VILLAGE PARKWAY TENTATIVE MAP

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The proposed units and densities not only comply with the underlying land use designations assigned by Washoe County, but are also compatible with the surrounding area as well. Per the Land Use Compatibility Matrix included in the Washoe County Development Code, HDS zoning and its associated permitted density, has the highest compatibility rating with MDS zoning which is located immediately to the south. GR portions of the site will remain undeveloped and are included as dedicated common area/open space. Preservation of this area, including steep slopes and ridgelines, will preserve viewsheds within Cold Springs and serves to ensure that the project provides a proper land use transition to the west.

The Common Open Space approach to the project is highly logical given the site location, characteristics, and product types proposed. Dedicated common areas will include landscape areas, resident amenities (within the townhome portion of the site) and stormwater facilities. These areas provide visual breaks within the community and add aesthetic appeal within neighborhoods. By including these areas and facilities within common area, long term maintenance by the HOA will occur, reducing the burden upon Washoe County. One of the most important considerations of the Common Open Space provisions is the preservation and protection of the western side of the site (areas zoned GR). This will ensure the permanent protection of steep slopes and the adjoining ridgeline. These areas help frame the west side of the Cold Springs Valley and dedicating them as common area/open space preserves views for residents of the entire area.

A detailed traffic impact analysis for the Village Parkway Tentative Map has been prepared by Solaegui Engineers to evaluate the traffic impacts resulting from development of the project. The study was done in conjunction with the Village Center project which is also being developed by Lifestyle Homes/Lissner family. Thus, the analysis provides for a more comprehensive analysis to account for all projects occurring within the area that may impact the local and regional roadway network. Recommendations from the traffic analysis are incorporated into the project design and identified mitigation measures can be conditioned (as necessary) with this tentative map request.

Based on trip generation data published by the Institute of Transportation Engineers (ITE), the townhome units (ITE Land Use Code 230) are expected to generate 1,063 average daily trips (ADT) with 81 am and 95 pm peak hour trips. The detached units (ITE Land Use Code 210) will generate 1,580 ADT with 125 am and 166 pm peak trips. Total estimated traffic generation is 2,643 ADT with 206 am and 261 pm peak trips at full buildout. It is important to note that this is a cumulative impact with the completion of all project phases. Per the recommendations of the traffic analysis, improvements and mitigations to the roadway network will occur to ensure that all traffic impacts are properly mitigated, and acceptable levels of service are maintained for area roadways.



## VILLAGE PARKWAY TENTATIVE MAP

The following table provides for an overall executive summary of the project:

Village Parkway Tentative Map - Development Summary	
Project Component	Proposed with Tentative Map
Project Area	124.6± acres
Development Area (HDS zoning)	47.2± acres
Townhome Units (Single Family Attached)	183 units
Detached Single Family Units	166 units
Total Units	349 units
Gross Project Density	2.8 dwelling units per acre
Net Project Density (Tentative Map Area)	7.4 dwelling units per acre
Smallest Detached Lot Size	3,645± square feet
Largest Detached Lot Size	8,257± square feet
Average Detached Lot Size	4,250± square feet
Smallest Attached Lot Size	800± square feet
Largest Attached Lot Size	1,348± square feet
Average Attached Lot Size	1,047± square feet
Total Lot Area	20.48± acres
Public Right-of-Way Area	6.65± acres
Common Area <sup>1</sup>	97.47± acres

<sup>1</sup> – includes private roadway area.

### Cold Springs Area Plan

The Village Parkway Tentative Map and its associated design and density fully complies with the current HDS regulatory zoning and Suburban Residential Master Plan land use designations. The proposed unit mix will serve to diversify the Cold Springs housing market and offers much needed housing opportunities that are more affordable than traditional single family homes on larger lots located within the area. This will appeal to a wide range of residents, including the “missing middle” which has been identified as an area of critical concern by regional agencies, including Washoe County, Truckee Meadows Regional Planning, and the Economic Development Authority of Western Nevada (EDAWN).

The project, as proposed, will either support or implement the following policies from the Cold Springs Area Plan. It is also important to note that the project does not conflict with any provisions outlined in the Area Plan. The site is located within the Cold Springs Suburban Character Management Area which is identified as the area where new growth is to occur within the Cold Springs Valleys.

Relevant policies:

*CS.1.1.3 Any residential land use more dense than one dwelling unit per five acres (1du/5 acres) must be located within the Cold Springs Suburban Character Management Area (CSCMA).*



## VILLAGE PARKWAY TENTATIVE MAP

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*CS.2.7 Landscape designs for new development will emphasize the use of native and/or drought tolerant vegetation, with non-native and atypical vegetation integrated sparingly into any landscaped area.*

*CS.2.7.1 Where landscaping is required in yards adjoining streets, residential subdivisions shall offer at least two (2) options for drought tolerant (i.e. climate adaptive) and native type landscaping.*

*CS.2.7.2 Large expanses of turf shall be discouraged, except for necessary use in parks and recreational facilities. The use of treated effluent shall be used whenever feasible for irrigation of large turf areas.*

*CS.2.8 To avoid long, continuous sections of solid fencing along street frontages, especially collectors and arterials, subdivision design should avoid platting large numbers of continuous linear lots with back yards and fences directly abutting the public right of way (see Photo 13). This design approach not only creates a "tunnel" effect, but can also result in maintenance problems, graffiti, and illegal access issues. If this design situation cannot be avoided, the following shall be required:*

*a. Fences may not exceed six (6) feet in height and shall be set back at least fifteen (15) feet from the edge of pavement or right-of-way, whichever is greater;*

*b. Fences shall employ offsetting articulation every other section;*

*c. Fences shall be either open (e.g. split rail) or (if not open) constructed of materials other than wood and metal, such as block masonry, brick, or stucco; and,*

*d. The creation of a Homeowners Association will be encouraged (for unified maintenance of common area and fencing).*

*CS.2.10 Prevent future suburban residential subdivisions from locating residences directly adjacent to major highways or railroad easements. Effective shielding and buffering will be planned to provide noise abatement with health and safety precautions.*

*CS.3.1 The policy level of service (LOS) for local and regional transportation facilities in the Cold Springs planning area is LOS "C" or better for roadway volume (i.e. flow rates) and LOS "D" or better for intersections. All development proposals must demonstrate how the adopted level of service for local transportation facilities will be maintained.*

*CS.3.2 Washoe County will work with the Regional Transportation Commission (RTC) and neighboring jurisdictions to ensure that potential impacts arising from development in neighboring jurisdictions are mitigated and consistent with the intent of policy CS.3.1.*

*CS.3.3 The necessary right-of-way and intersection requirements identified in the Regional Transportation Plan will be protected through dedication, setback or other method deemed adequate and appropriate by the Regional Transportation Commission and Washoe County.*

## VILLAGE PARKWAY TENTATIVE MAP

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*CS.4.1 Ensure that the scenic and ecologic qualities of the mountains and hills in the Cold Springs planning area are preserved.*

*CS.4.1.1 Development on hillsides shall disturb the smallest area possible. All graded or disturbed areas, exposed slopes and areas of soil or landform disturbance not designated for development shall be revegetated after grading in order to mitigate adverse visual impacts, improve soil conditions, minimize erosion and stabilize necessary cut and fill slopes with plant roots. Drought tolerant/fire resistant and/or native species should be used whenever possible.*

*CS.4.1.2 Revegetation should be conducted as soon as practicable after disturbance while considering factors favorable to successful outcomes, such as weather and seasonal conditions.*

*CS.4.1.3 During development review, preference will be given to proposals that minimize hillside disturbance or otherwise conserve steep slopes.*

*CS.4.1.4 Development and/or disturbance of slopes in excess of 30% shall be prohibited except for necessary utility and infrastructure facilities. Any area of 30% slopes disturbed for utility or infrastructure purposes shall be mitigated by the provision of undisturbed open space elsewhere on the site at a 2:1 ratio.*

*CS.4.1.5 Unique geological landforms, landmarks, and natural rock outcroppings shall be preserved.*

*CS.4.2 The following shall be considered in all grading activities:*

- a. Minimize disruption to natural topography.*
- b. Utilize natural contours and slopes.*
- c. Complement the natural characteristics of the landscape.*
- d. Preserve existing vegetation and ground coverage where possible to minimize erosion.*
- e. Minimize cuts and fills.*

*CS.4.3 Encourage techniques such as transfer of development rights and conservation easements to protect sensitive areas. For example, development rights on the upper slopes of Peavine, Fred's and Petersen Mountains could be transferred or purchased for use in more suitable areas.*

*CS.4.5 Fencing installed along common open space areas within subdivisions should consist of an "open fence" design (e.g. split rail or equivalent).*



## VILLAGE PARKWAY TENTATIVE MAP

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*CS.5.1 Prior to the approval of master plan amendments, tentative maps, or public initiated capital improvements in the Cold Springs planning area, the Nevada Department of Conservation and Natural Resources will be contacted and, if the department requests, an appropriate archaeological investigation will be conducted.*

*CS.6.1 All development and planning activities, regardless of agency, shall be reviewed for compatibility with, and potential implementation of, the Recreational Opportunities Plan map.*

*CS.6.1.1 Certain proposed trail alignments follow existing street alignments in order to provide overall connectivity and linkage to school and park facilities. These alignments are considered "proposed" because at present only the street right-of-way is available for pedestrian and bike use. Concrete sidewalks, dirt and gravel paths, bike lanes, signage, and/or other improvements should be constructed along these alignments as part of future street maintenance, development, or other capital improvements. These proposed routes represent desired designated bike and pedestrian routes within the community.*

*CS.9.3 Open space areas, including privately owned common open space, should be linked together to the greatest extent possible (to form unbroken corridors) and allow barrier free access to wildlife.*

*CS.9.4 South facing slopes with good sun exposure, particularly slopes with bitterbrush and mature vegetation, should receive a higher priority in the designation of open space to protect winter range habitat for Mule Deer and other wildlife.*

*CS.9.5 The Petersen Mountain Range is used as critical winter range by local Mule Deer herds and is of particular importance to overall Mule Deer habitat within the planning area. Washoe County strongly supports the preservation of this habitat and associated migration corridors and encourages the Bureau of Land Management to conduct additional planning for this area.*

*CS.10.1 Development proposals within the Cold Springs Valley will conform to Regional Water Management Plan Policy 3.1.c, "Flood Plain Storage Outside the Truckee River Watershed," as well as locally specific flood control requirements as amended and adopted by the Washoe County Department of Water Resources and the Regional Water Planning Commission.*

*CS.10.2 Increases or displacement in volume of storm drainage runoff as a result of development will be mitigated per procedures set forth in Washoe County Code Chapter 110 (i.e. the Development Code), the Regional Water Management Plan, and the Truckee Meadows Low Impact Development Manual.*

*CS.10.3 The use of Low Impact Development (LID) techniques is strongly encouraged to help implement Goal Ten (10) and associated policies. For guidance implementing this policy, consult the Truckee Meadows Low Impact Development Manual developed for the Cities of Reno and Sparks and Washoe County under the guidance of the Truckee Meadows Storm Water Permit Coordinating Committee.*



## VILLAGE PARKWAY TENTATIVE MAP

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*CS.11.2 New development shall comply with Regional Water Management Plan Policy 1.3.e: "Water Resource Commitments."*

*CS.11.3 New development shall comply with Regional Water Management Plan Policy 2.1.a: "Effluent Reuse – Efficient Use of Water Resources and Water Rights."*

### **Tentative Map Findings**

Section 110.608.20 of the Washoe County Development Code establishes legal findings that must be made by the Planning Commission or Board of County Commissioners in order to approve a Tentative Map request. These findings are listed below and are addressed in **bold face** type.

- (a) **Environmental and Health Laws.** Environmental and health laws and regulations concerning water and air pollution, the disposal of solid waste, facilities to supply water, community or public sewage disposal and, where applicable, individual systems for sewage disposal;

**The Village Parkway Tentative Map will be served by municipal water through an extension of existing Great Basin Water Company facilities. Sewer service will be provided by Washoe County at the Cold Springs Water Reclamation Facility which has ample capacity to accommodate the 349 proposed units ( a will serve letter is included in the appendices of this report). Waste Management will provide solid waste removal and is already operating in the immediate area.**

- (b) **Availability of Water.** The availability of water which meets applicable health standards as well as requirements for water rights, quality or will-serve commitments;

**The project will be served by Great Basin Water Company. An intent to serve letter from the water company is included as an attachment to this report.**

- (c) **Utilities.** The availability and accessibility of utilities;

**The project will be served by all municipal utilities, infrastructure, and services as detailed within this report and on the attached engineering plans.**

- (d) **Public Services.** The availability and accessibility of public services such as schools, police and fire protection, transportation, recreation and parks;

**Public services, including sheriff patrols are already occurring within the surrounding neighborhoods. With construction of the new elementary school in Cold Springs, the Washoe County School District has indicated that there is ample capacity to accommodate new students from this project. The project site is within a two minute response time of the TMFPD Cold Springs station and is within walking distance of existing park facilities.**

## VILLAGE PARKWAY TENTATIVE MAP

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- (e) Plan Consistency. General conformance with the Development Code and Master Plan;

The project, as proposed, is consistent with Washoe County Development Code standards, including the Article 408/Common Open Space provisions. Project density is in full compliance with the existing HDS zoning and Suburban Residential Master Plan designations.

- (f) Impact on Existing Streets. The effect of the proposed subdivision on existing public streets and the need for new streets or highways to serve the subdivision;

A detailed traffic impact analysis has been completed by Solaegui Engineers, concurrent with this tentative map request. The traffic study identifies required roadway improvements and mitigation measures that can be conditioned with this request to ensure all impacts associated with the project are properly mitigated and appropriate levels of service are retained.

- (g) Physical Characteristics. Physical characteristics of the land such as flood plain, slope and soil;

The site is well suited for the type and intensity of development proposed, as discussed in the previous section of this report. Development is focused on flat portions of the site with very little disturbance proposed within GR designated areas. The Common Open Space approach will preserve steeper slopes and the ridgeline that runs within the western portion of the parcel boundaries.

- (h) Agency Review. The recommendations and comments of the entities reviewing the tentative map; and

Copies of this report and the included plans will be circulated to all applicable reviewing agencies for review and comment. Specific requirements and relevant comments can be included as conditions tied to this request and implemented with final map(s).

- (i) Impact on Existing Drainage System. The effect of the proposed subdivision on the existing natural and man-made drainage system.

The project will provide for onsite detention at various locations within the site, compliant with Washoe County standards. Run-off from the site will not be increased in the post development condition. A detailed drainage study is included as an attachment to this report.



# APPENDICES

## Washoe County Development Application

Your entire application is a public record. If you have a concern about releasing personal information, please contact Planning and Building staff at 775.328.6100.

<b>Project Information</b>		Staff Assigned Case No.: _____	
Project Name: <b>Village Parkway Tentative Map</b>			
Project Description: A tentative subdivision map request to allow for 166 detached and 183 attached single family units in the HDS zone.			
Project Address: West side of Village Parkway, north of Cold Springs Drive			
Project Area (acres or square feet): <b>124.6 acres</b>			
Project Location (with point of reference to major cross streets <b>AND</b> area locator):			
<small>The site is located on the west side of Village Parkway, north of Cold Springs Drive in Cold Springs. Mud Springs Drive traverses along the eastern property boundary. See attached vicinity map.</small>			
Assessor's Parcel No.(s):	Parcel Acreage:	Assessor's Parcel No.(s):	Parcel Acreage:
087-400-11	42.43 acres	087-400-24	41.26 acres
087-400-23	40.91 acres		
Indicate any previous Washoe County approvals associated with this application: Case No.(s). WRZA20-0004			
<b>Applicant Information (attach additional sheets if necessary)</b>			
<b>Property Owner:</b>		<b>Professional Consultant:</b>	
Name: Lifestyle Homes TND, LLC		Name: Christy Corporation, Ltd.	
Address: 4790 Caughlin Pkwy., Suite 519		Address: 1000 Kiley Pkwy.	
Reno, NV	Zip: 89519	Sparks, NV	Zip: 89436
Phone: (775) 750-5537	Fax:	Phone: (775) 502-8552	Fax:
Email: rlissner@gmail.com		Email: mike@christynv.com	
Cell: (775) 750-5537	Other:	Cell: (775) 250-3455	Other:
Contact Person: Bob Lissner		Contact Person: Mike Railey	
<b>Applicant/Developer:</b>		<b>Other Persons to be Contacted:</b>	
Name: Same as Above		Name: Summit Engineering Corporation	
Address:		Address: 5405 Mae Anne Ave.	
	Zip:	Reno, NV	Zip: 89523
Phone:	Fax:	Phone: (775) 747-8550	Fax:
Email:		Email: robert@summitnv.com	
Cell:	Other:	Cell: (775) 787-4331	Other:
Contact Person:		Contact Person: Robert Gelu, P.E.	
<b>For Office Use Only</b>			
Date Received:	Initial:	Planning Area:	
County Commission District:		Master Plan Designation(s):	
CAB(s):		Regulatory Zoning(s):	



## Property Owner Affidavit

**Applicant Name:** Lifestyle Homes TND, LLC

The receipt of this application at the time of submittal does not guarantee the application complies with all requirements of the Washoe County Development Code, the Washoe County Master Plan or the applicable area plan, the applicable regulatory zoning, or that the application is deemed complete and will be processed.

STATE OF NEVADA     )  
  )  
COUNTY OF WASHOE    )

I, Robert Lissner  
(please print name)

being duly sworn, depose and say that I am the owner\* of the property or properties involved in this application as listed below and that the foregoing statements and answers herein contained and the information herewith submitted are in all respects complete, true, and correct to the best of my knowledge and belief. I understand that no assurance or guarantee can be given by members of Planning and Building.

**(A separate Affidavit must be provided by each property owner named in the title report.)**

Assessor Parcel Number(s): 087-400-11, 23, and 24

Printed Name Robert Lissner

Signed R. LISSNER

Address 4790 Caughlin Plwy #519  
Reno, NV 89519

Subscribed and sworn to before me this 10<sup>th</sup> day of February, 2021.

[Signature]  
Notary Public in and for said county and state

My commission expires: 10/16/21

(Notary Stamp)



\*Owner refers to the following: (Please mark appropriate box.)

- Owner
- Corporate Officer/Partner (Provide copy of record document indicating authority to sign.)
- Power of Attorney (Provide copy of Power of Attorney.)
- Owner Agent (Provide notarized letter from property owner giving legal authority to agent.)
- Property Agent (Provide copy of record document indicating authority to sign.)
- Letter from Government Agency with Stewardship

Community Services Department  
Planning and Building  
TENTATIVE SUBDIVISION MAP  
APPLICATION



Community Services Department  
Planning and Building  
1001 E. Ninth St., Bldg. A  
Reno, NV 89512-2845

Telephone: 775.328.6100



## Tentative Subdivision Map Application Supplemental Information

(All required information may be separately attached)

1. What is the location (address or distance and direction from nearest intersection)?

The project site is on the west side of Village Parkway approximately 1,300 feet north of Cold Springs Drive.

2. What is the subdivision name (proposed name must not duplicate the name of any existing subdivision)?

Village Parkway Homes

3. Density and lot design:

a. Acreage of project site	124.6 acres
b. Total number of lots	349
c. Dwelling units per acre	2.8 du/ac
d. Minimum and maximum area of proposed lots	800 sq.ft. minimum/8,257 sq.ft. maximum
e. Minimum width of proposed lots	18 feet (attached product)
f. Average lot size	4,250 sq.ft. (detached)/1,047 sq.ft. (attached)

4. What utility company or organization will provide services to the development:

a. Sewer Service	Cold Springs Water Treatment Facility
b. Electrical Service	NV Energy
c. Telephone Service	AT&T or Charter Communications
d. LPG or Natural Gas Service	NV Energy
e. Solid Waste Disposal Service	Waste Management
f. Cable Television Service	AT&T or Charter Communications
g. Water Service	

5. For common open space subdivisions (Article 408), please answer the following:

- a. Acreage of common open space:

97.47 acres

- b. What development constraints are within the development and how many acres are designated slope, wetlands, faults, springs, and/or ridgelines:

The west side of the site contains slope areas (approximately 77.37 acres)

- c. Range of lot sizes (include minimum and maximum lot size):

800 square feet (attached) to 8,257 square feet (detached)

d. Proposed yard setbacks if different from standard:

Detached - 20' to garage/10' to house (front), 3' to property line/10' to buildings (side), 10' (rear). Attached - 0' with 10' between buildings.

e. Justification for setback reduction or increase, if requested:

The adjusted setbacks allow for a new product type in the Cold Springs market that is much needed and provides more attainable housing for a wide demographic.

f. Identify all proposed non-residential uses:

Various common area and open space is provided. Refer to attached plans.

g. Improvements proposed for the common open space:

Common areas will be landscaped as shown on the attached landscape plan. Slopes on the west side of the property will remain as natural open space.

h. Describe or show on the tentative map any public or private trail systems within common open space of the development:

Refer to the attached plan for trails, paths, and pedestrian improvements.

i. Describe the connectivity of the proposed trail system with existing trails or open space adjacent to or near the property:

A trail is provided at the western portion of the project providing connection to open space areas.

j. If there are ridgelines on the property, how are they protected from development?

Ridgelines on the west side of the property are preserved as permanent open space.

k. Will fencing be allowed on lot lines or restricted? If so, how?

Privacy fencing between detached homes will be permitted per WCDL standards.

l. Identify the party responsible for maintenance of the common open space:

A homeowner's association will be established to provide ongoing maintenance of common areas and community amenities.

6. Is the project adjacent to public lands or impacted by "Presumed Public Roads" as shown on the adopted April 27, 1999 Presumed Public Roads (see Washoe County Engineering website at <http://www.washoecounty.us/pubworks/engineering.htm>). If so, how is access to those features provided?

Public land exists beyond GR zoned areas. A trail is provided to allow access to this area. Refer to attached plans.

7. Is the parcel within the Truckee Meadows Service Area?

Yes

No



8. Is the parcel within the Cooperative Planning Area as defined by the Regional Plan?

<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	If yes, within what city?
------------------------------	--	---------------------------

9. Has an archeological survey been reviewed and approved by SHPO on the property? If yes, what were the findings?

Not applicable.

10. Indicate the type and quantity of water rights the application has or proposes to have available:

a. Permit #		acre-feet per year	
b. Certificate #		acre-feet per year	
c. Surface Claim #		acre-feet per year	
d. Other #		acre-feet per year	

a. Title of those rights (as filed with the State Engineer in the Division of Water Resources of the Department of Conservation and Natural Resources):

A water service acknowledgement from Great Basin Water Company is attached.

11. Describe the aspects of the tentative subdivision that contribute to energy conservation:

Homes will include energy efficient building materials and solar orientation is a consideration in the placement of building envelopes (to the extent possible).

12. Is the subject property in an area identified by Planning and Building as potentially containing rare or endangered plants and/or animals, critical breeding habitat, migration routes or winter range? If so, please list the species and describe what mitigation measures will be taken to prevent adverse impacts to the species:

Not applicable.

13. If private roads are proposed, will the community be gated? If so, is a public trail system easement provided through the subdivision?

Alleys will be private but no gating is proposed.

14. Are there any applicable policies of the adopted area plan in which the project is located that require compliance? If so, which policies and how does the project comply?

Refer to attached report for a detailed policy analysis.

15. Are there any applicable area plan modifiers in the Development Code in which the project is located that require compliance? If so, which modifiers and how does the project comply?

Not applicable.

16. Will the project be completed in one phase or is phasing planned? If so, please provide that phasing plan:

The project is expected to take 5 to 7 years to complete with up to 4 phases for each product type.

17. Is the project subject to Article 424, Hillside Development? If yes, please address all requirements of the Hillside Ordinance in a separate set of attachments and maps.

<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	If yes, include a separate set of attachments and maps.
------------------------------	--	---

18. Is the project subject to Article 418, Significant Hydrologic Resources? If yes, please address Special Review Considerations within Section 110.418.30 in a separate attachment.

<input type="checkbox"/> Yes	<input checked="" type="checkbox"/> No	If yes, include separate attachments.
------------------------------	--	---------------------------------------

## Grading

Please complete the following additional questions if the project anticipates grading that involves: (1) Disturbed area exceeding twenty-five thousand (25,000) square feet not covered by streets, buildings and landscaping; (2) More than one thousand (1,000) cubic yards of earth to be imported and placed as fill in a special flood hazard area; (3) More than five thousand (5,000) cubic yards of earth to be imported and placed as fill; (4) More than one thousand (1,000) cubic yards to be excavated, whether or not the earth will be exported from the property; or (5) If a permanent earthen structure will be established over four and one-half (4.5) feet high:

19. How many cubic yards of material are you proposing to excavate on site?

Refer to attached engineering plans and reports for a full grading plan including cut/fill analysis.
--

20. How many cubic yards of material are you exporting or importing? If exporting of material is anticipated, where will the material be sent? If the disposal site is within unincorporated Washoe County, what measures will be taken for erosion control and revegetation at the site? If none, how are you balancing the work on-site?

Import of fill material will occur. Refer to attached engineering plans for full details.
---

21. Can the disturbed area be seen from off-site? If yes, from which directions, and which properties or roadways? What measures will be taken to mitigate their impacts?

Areas of cut will be fully screened from adjoining properties by new homes and landscaping.
---

22. What is the slope (Horizontal/Vertical) of the cut and fill areas proposed to be? What methods will be used to prevent erosion until the revegetation is established?

Revegetation and rip-rap (as needed) will be used to stabilize disturbed slopes. Slopes are proposed at 3:1, consistent with Washoe County policy.
--

23. Are you planning any berms and, if so, how tall is the berm at its highest? How will it be stabilized and/or revegetated?

Berms will be included adjacent to detention areas and include a mix of native revegetation and formal landscape treatments.
--

24. Are retaining walls going to be required? If so, how high will the walls be, will there be multiple walls with intervening terracing, and what is the wall construction (i.e. rockery, concrete, timber, manufactured block)? How will the visual impacts be mitigated?

Refer to attached grading plan for specific wall details and heights. Walls are located at the western edge of the project.
---



25. Will the grading proposed require removal of any trees? If so, what species, how many, and of what size?

Not applicable.

26. What type of revegetation seed mix are you planning to use and how many pounds per acre do you intend to broadcast? Will you use mulch and, if so, what type?

Refer to attached landscape plan for revegetation specifications.

27. How are you providing temporary irrigation to the disturbed area?

Temporary irrigation can be provided via a connection with domestic service planned for landscaped common areas.

28. Have you reviewed the revegetation plan with the Washoe Storey Conservation District? If yes, have you incorporated their suggestions?

WSCD will be a reviewing agency of this request and suggestions can be conditioned as appropriate.

## Request to Reserve New Street Name(s)

The Applicant is responsible for all sign costs.

### Applicant Information

Name: Lifestyle Homes TND, LLC  
 Address: 4790 Caughlin Pkwy., Suite 519  
The project site is on the west side of Village Parkway approximately 1,300 feet north of Cold Springs Drive.  
 Phone : \_\_\_\_\_ Fax: \_\_\_\_\_  
% Private Citizen                      % Agency/Organization

### Street Name Requests

(No more than 14 letters or 15 if there is an "i" in the name. Attach extra sheet if necessary.)

Street names will be requested with final map	

If final recordation has not occurred within one (1) year, it is necessary to submit a written request for extension to the coordinator prior to the expiration date of the original

### Location

Project Name: Village Parkway Tentative Map  
% Reno                      % Sparks                      % Washoe County  
 Parcel Numbers: \_\_\_\_\_  
% Subdivision                      % Parcelization                      % Private Street

Please attach maps, petitions and supplementary information.

Approved: \_\_\_\_\_ Date: \_\_\_\_\_  
 Regional Street Naming Coordinator  
% Except where noted  
 Denied: \_\_\_\_\_ Date: \_\_\_\_\_  
 Regional Street Naming Coordinator

Washoe County Geographic Information Services

1001 E. Ninth Street  
 Reno, NV 89512-2845

Phone: (775) 328-2325 - Fax: (775) 328-6133



Washoe County Treasurer  
 Tammi Davis

Account Detail

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CollectionCart			
Collection Cart	Items	Total	
Collection Cart	0	\$0.00	<a href="#">Checkout</a> <a href="#">View</a>

Pay Online
No payment due for this account.

Washoe County Parcel Information			
Parcel ID	Status	Last Update	
08740011	Active	3/5/2021 1:40:37 AM	
<b>Current Owner:</b> LIFESTYLE HOMES TND LLC  4790 CAUGHLIN PKWY 519 RENO, NV 89519		<b>SITUS:</b> 1050 MUD SPRINGS DR WCTY NV	
<b>Taxing District</b> 4000	<b>Geo CD:</b>		

Tax Bill (Click on desired tax year for due dates and further details)					
Tax Year	Net Tax	Total Paid	Penalty/Fees	Interest	Balance Due
2020	\$649.45	\$649.45	\$0.00	\$0.00	\$0.00
2019	\$617.92	\$617.92	\$0.00	\$0.00	\$0.00
2018	\$589.62	\$589.62	\$0.00	\$0.00	\$0.00
2017	\$565.85	\$565.85	\$0.00	\$0.00	\$0.00
2016	\$552.33	\$552.33	\$0.00	\$0.00	\$0.00
Total					\$0.00

**Disclaimer**

- **ALERTS:** If your real property taxes are delinquent, the search results displayed may not reflect the correct amount owing. Please contact our office for the current amount due.
- For your convenience, online payment is available on this site. E-check payments are accepted without a fee. However, a service fee does apply for online credit card payments. See Payment Information for details.

**Pay By Check**

Please make checks payable to:  
**WASHOE COUNTY TREASURER**

**Mailing Address:**  
 P.O. Box 30039  
 Reno, NV 89520-3039

**Overnight Address:**  
 1001 E. Ninth St., Ste D140  
 Reno, NV 89512-2845

**Payment Information**

**Special Assessment District**

**Installment Date Information**

**Assessment Information**

Washoe County Treasurer  
 P.O. Box 30039, Reno, NV 89520-3039  
 ph: (775) 328-2510 fax: (775) 328-2500  
 Email: [tag@washoetxonly.us](mailto:tag@washoetxonly.us)

Washoe County Treasurer  
 Tammi Davis

Account Detail

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CollectionCart			
Collection Cart	Items	Total	
Collection Cart	0	\$0.00	<a href="#">Checkout</a> <a href="#">View</a>

**Pay Online**

No payment due for this account.

**Washoe County Parcel Information**

Parcel ID	Status	Last Update
08740023	Active	3/5/2021 1:40:37 AM

**Current Owner:**  
 LIFESTYLE HOMES TND LLC  
 4790 CAUGHLIN PKWY 519  
 RENO, NV 89519

**SITUS:**  
 17811 VILLAGE PKWY  
 WASHOE COUNTY NV

**Taxing District:**  
 4000

**Geo CD:**

**Tax Bill (Click on desired tax year for due dates and further details)**

Tax Year	Net Tax	Total Paid	Penalty/Fees	Interest	Balance Due
2020	\$344.56	\$344.56	\$0.00	\$0.00	\$0.00
2019	\$327.55	\$327.55	\$0.00	\$0.00	\$0.00
2018	\$312.55	\$312.55	\$0.00	\$0.00	\$0.00
2017	\$299.95	\$299.95	\$0.00	\$0.00	\$0.00
2016	\$293.17	\$293.17	\$0.00	\$0.00	\$0.00
<b>Total</b>					\$0.00

**Disclaimer**

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- For your convenience, online payment is available on this site. E-check payments are accepted without a fee. However, a service fee does apply for online credit card payments. See Payment Information for details.

**Pay By Check**

Please make checks payable to:  
**WASHOE COUNTY TREASURER**

**Mailing Address:**  
 P.O. Box 30039  
 Reno, NV 89520-3039

**Overnight Address:**  
 1001 E. Ninth St., Ste D140  
 Reno, NV 89512-2845

**Payment Information**

**Special Assessment District**

**Installment Date Information**

**Assessment Information**



Washoe County Treasurer  
 Tammi Davis

Account Detail

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CollectionCart			
Collection Cart	Items	Total	
Collection Cart	0	\$0.00	<a href="#">Checkout</a> <a href="#">View</a>

**Pay Online**

No payment due for this account.

Washoe County Parcel Information		
Parcel ID	Status	Last Update
08740024	Active	3/5/2021 1:40:37 AM
<b>Current Owner:</b> LIFESTYLE HOMES TND LLC  4790 CAUGHLIN PKWY 519 RENO, NV 89519		<b>SITUS:</b> 17901 VILLAGE PKWY WASHOE COUNTY NV
<b>Taxing District</b> 4000	<b>Geo CD:</b>	

Tax Bill (Click on desired tax year for due dates and further details)					
Tax Year	Net Tax	Total Paid	Penalty/Fees	Interest	Balance Due
2020	\$385.68	\$385.68	\$0.00	\$0.00	\$0.00
2019	\$366.71	\$366.71	\$0.00	\$0.00	\$0.00
2018	\$349.91	\$349.91	\$0.00	\$0.00	\$0.00
2017	\$335.81	\$335.81	\$0.00	\$0.00	\$0.00
2016	\$328.12	\$328.12	\$0.00	\$0.00	\$0.00
<b>Total</b>					\$0.00

**Disclaimer**

- ALERTS:** If your real property taxes are delinquent, the search results displayed may not reflect the correct amount owing. Please contact our office for the current amount due.
- For your convenience, online payment is available on this site. E-check payments are accepted without a fee. However, a service fee does apply for online credit card payments. See Payment Information for details.

**Pay By Check**

Please make checks payable to:  
**WASHOE COUNTY TREASURER**

**Mailing Address:**  
 P.O. Box 30039  
 Reno, NV 89520-3039

**Overnight Address:**  
 1001 E. Ninth St., Ste D140  
 Reno, NV 89512-2845

- [Payment Information](#)
- [Special Assessment District](#)
- [Installment Date Information](#)
- [Assessment Information](#)



Great Basin  
Water Co.™

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## NOTICE OF INTENT TO SERVE

**Re: Mud Springs Condos**

**329 Townhouses – Washoe County Parcels 87-400-11, 23 and 24**

**Type: Central Water**

**Utility Service Provider Name: Great Basin Water Co.**

The undersigned Utility Service Provider agrees to provide the aforementioned Mud Springs Condos (aka Village Parkway) project (“the Project”) water service in accordance with the terms and conditions of the then current utility tariffs approved by the Public Utilities Commission of Nevada (PUCN) and subject to the conditions set forth herein and agreed to by the developer of the Project (“Developer”) who has countersigned below. Developer and Utility Service Provider shall cooperate to seek approval from the Public Utilities Commission of Nevada (“PUCN”) to annex the Project area into the Utility Service Provider’s certificated service area.

This commitment to serve is conditioned upon the Utility Service Provider’s receipt of necessary approvals from all required government agencies, including but not limited to the annexation approval from the PUCN, the Developer’s satisfaction of all tariff and development requirements of Utility Service Provider. Such development requirements of Utility Service Provider include the Developer’s payment of all appropriate fees and Developer’s dedication and Utility Service Provider’s acceptance of any and all required infrastructure and water rights in good standing with the Nevada Division of Water Resources (“NDWR”) and adequate for provision of water service to the Project. For the avoidance of doubt, Utility Service Provider shall have no obligation to provide service to the Project unless and until all Developer obligations are satisfied which shall include any necessary regulatory approvals from Nevada Division Water Resources or any other agency with jurisdiction for Utility Service Provider’s use of the water rights Developer dedicates to the Utility Service Provider for its provision of service to the Project.

Utility Service Provider intends to service the proposed development with potable water service for 329 Townhouses. This Project requires an estimated 46.3 AFA (using permit Nos. 65056 and 65058) calculated at .12 AFA per unit plus 2.0 acres of landscaping calculated at 3.41 AFA per acre based on GBWC Division Tariff 1-W (Water) Rule No. 21, C. Water Rights Dedication Requirements for an Intent to Serve, Cold Springs – Spanish Springs. Utility Service Provider’s intent to serve is conditioned upon the availability and adequacy of water under these water rights dedicated by Developer.

This document is agreed to under the signature of an agent of the Utility Service Provider authorized to sign the agreement and Developer’s authorized agent. This notice of Intent to Serve will expire and become null and void if the service for the aforesaid parcel is not applied for with the Utility Service



Provider within two years of the date of this document in accordance with the terms of the utility's tariffs in force at such time.

Name of Lifestyle Homes TND, LLC agent: Robert Lissner

Robert Lissner 1/8/20

Signature of Authorized Agent of Developer

Date

Name of Utility Service Provider's authorized agent: Wendy Barnett, President, GBWC

Wendy Barnett 1-8-20

Signature of Authorized Agent of Water Provider

Date

Recd 2/8/21

ADDENDUM TO INTENT TO SERVE  
Mud Springs Condos – January 8, 2020

**Subject:** December 16, 2020 update:

1. Name -- From Mud Springs Condos to Village Parkway
2. From 329 Townhouses to 191 Townhouses and 181 Single Family Residences
3. Change in water right permit Nos. and total AFA requirement

Developer had previously proposed the development as Mud Springs Condos (now Village Parkway) for 329 Townhouses and is now altering the plans to have 191 Townhouses and 181 Single Family Residences (3600 sq ft). Originally, the development was to use 46.3 AFA using two permit Nos. Now the development will use 73.03 AFA that will come from Permit No. 65058 only.

This intent to serve is conditioned upon GBWC's receipt of necessary approvals from all required government agencies.

IN WITNESS WHEREOF, this Agreement is executed on the date above first written.

Lifestyle Homes TND, LLC agent

R. LUSNER 2/8/21

By:

Its: MANAGER

Great Basin Water Co.

Sean Twomey

By: Sean Twomey

Its: President



**WASHOE COUNTY**  
**COMMUNITY SERVICES DEPARTMENT**  
**Engineering and Capital Projects**

1001 EAST 9<sup>TH</sup> STREET  
PO BOX 11130  
RENO, NEVADA 89520-0027  
PHONE (775) 328.3600  
FAX (775) 328.3699

January 27, 2021

Robert Lissner  
Woodland Village North, LLC  
4790 Caughlin Parkway #519  
Reno, NV 89519

**SUBJECT: Intent to Serve Village Parkway Homes**  
**APN: 087-400-11; 087-400-24; 087-400-23**  
**372 Units**

To whom it may concern:

The Washoe County Community Services Department, Engineering and Capital Projects Division, has reviewed the preliminary plans for the subject project and has committed to serve the project under the following conditions:

1. Final building permit plans are submitted to Washoe County Utilities for review and approval per Washoe County ordinance and design standards.
2. Adhere to all sections of NAC 278.290 & NAC 278.430 that require all necessary improvements to the collection system or treatment facility be approved by Washoe County Utilities and constructed and/or the financial assurance made prior to the approval of the building permit.

Review of the information submitted does not constitute an application for service, imply the process of planning and construction of the facilities necessary for service have been completed, is not a will serve letter nor does it imply that any sewer connection fees have been paid. Capacity assurance will be determined after all fees have been paid and accepted.

Sincerely,

Dwayne E. Smith, P.E.  
Director Engineering & Capital Projects

c: Timothy Simpson, P.E., Licensed Engineer



INTEGRITY



EFFECTIVE  
COMMUNICATION



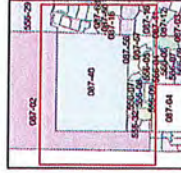
QUALITY  
PUBLIC SERVICE



**LAND MAP #45**  
 MAP OF DIVISION INTO LARGE PARCELS  
 PORTION OF SECTION 17  
 T21N - R18E

Assessor's Map Number  
**087-40**

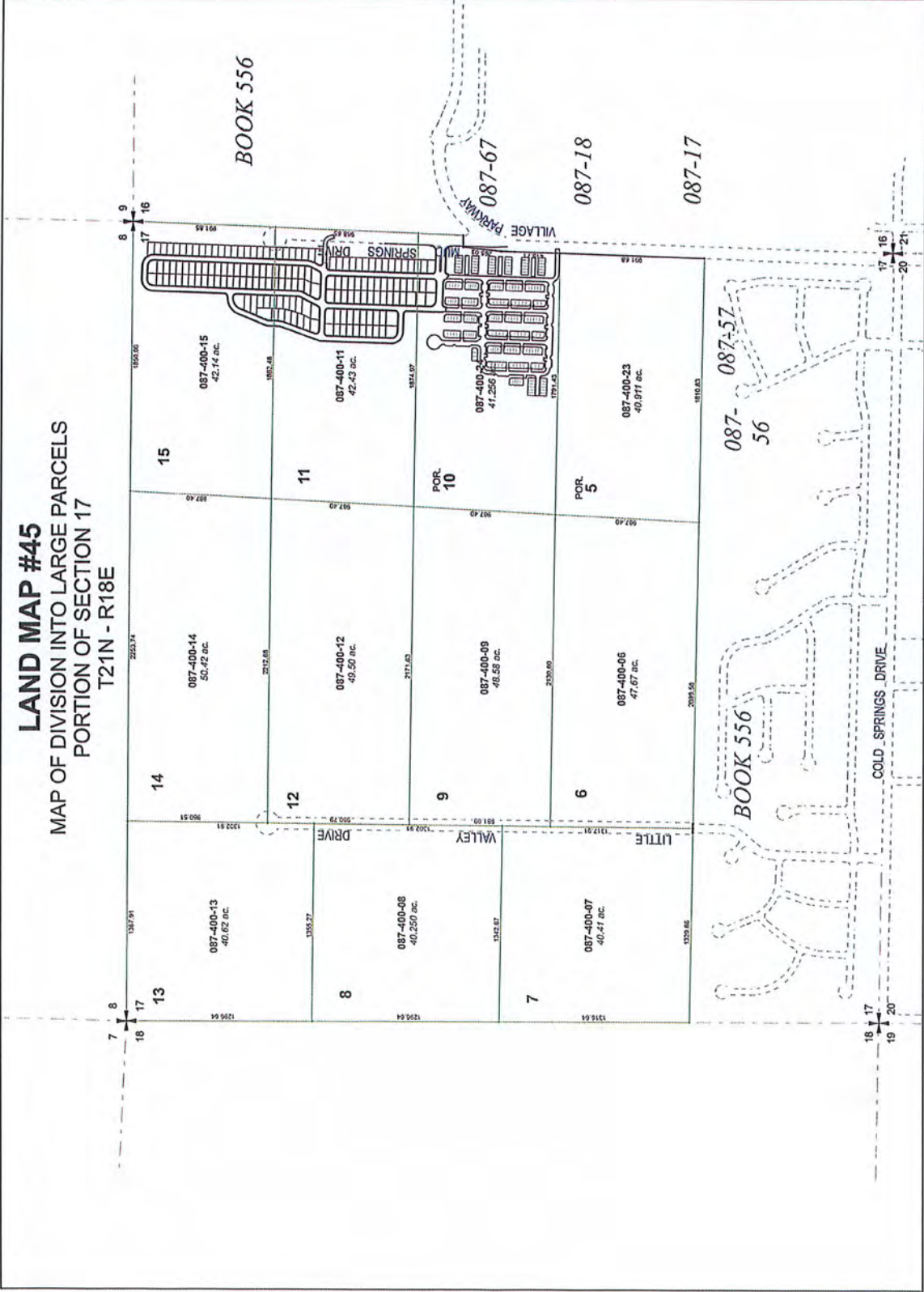
STATE OF NEVADA  
**WASHOE COUNTY**  
 ASSESSOR'S OFFICE  
 Michael E. Clark, ASSESSOR  
 1001 East Main Street  
 Reno, Nevada 89502  
 (775) 335-2231



created by: **EMG 6/26/2015**  
 last updated:

area previously shown on map(s)  
**087-02**

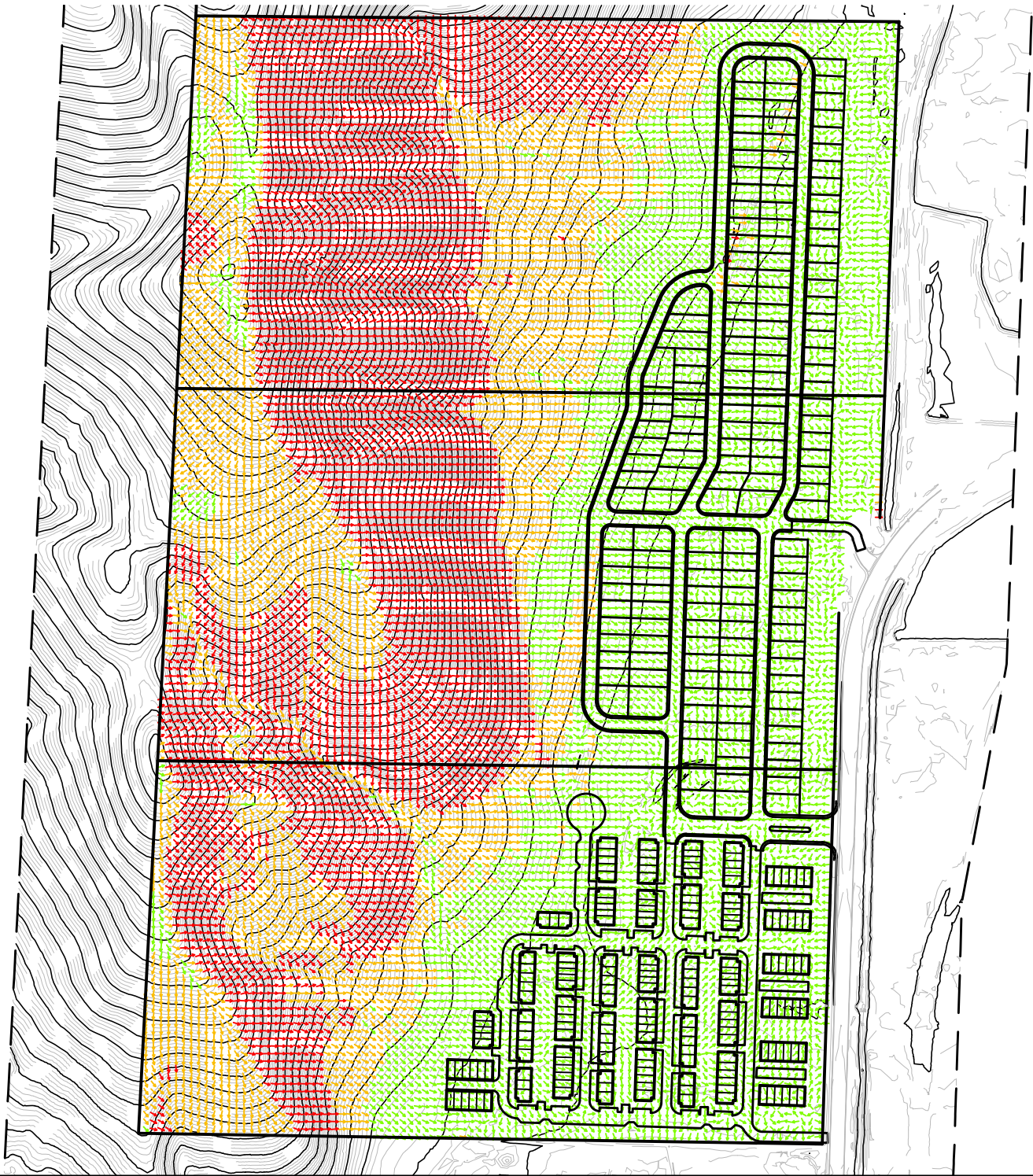
NOTE: This map was prepared for the use of the Washoe County Assessor for assessment and a survey of the premises. No liability is assumed as to the public utility or accuracy of the data presented herein.





SLOPE STATISTICS FOR SUBJECT PROPERTY

■ 0 TO 15 Percent	46.20%	57.55 AC.
■ 15 TO 30 Percent	22.90%	28.52 AC.
■ > 30 Percent	30.90%	38.49 AC.
TOTALS	100%	124.56 AC.



VILLAGE PARKWAY  
HOMES  
SLOPE MAP

SCALE: 1" = 400'

Copyright SUMMIT ENG 2021

**SUMMIT** ENGINEERING CORPORATION  
5405 MAE ANNE AVENUE, RENO, NV, 89523  
PHONE: (775) 747-8550 FAX: (775) 747-8559

SHEET  
1

OF  
1

**PRELIMINARY  
SANITARY SEWER REPORT  
FOR  
VILLAGE PARKWAY  
HOMES**

Prepared for

LIFESTYLE HOMES TND, LLC  
4790 CAUGHLIN PARKWAY #519  
RENO, NV 89519

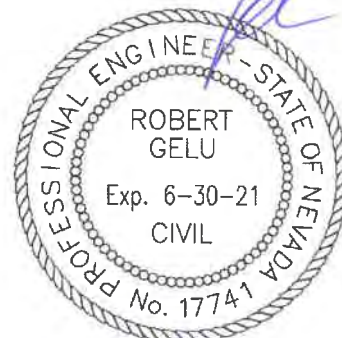
Prepared by



**SUMMIT ENGINEERING CORPORATION**  
5405 MAE ANNE AVENUE  
RENO, NEVADA 89523  
(775) 747-8550

Job # 31097

MARCH 2021



3-8-21



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INTRODUCTION.....	1
DESIGN STANDARDS.....	1
EXISTING SANITARY SEWER FACILITIES.....	2
PROPOSED SANITARY SEWER FACILITIES.....	2
SEWER ANALYSIS.....	2
CONCLUSION.....	3

**APPENDIX A**

VICINITY MAP

ON-SITE SANITARY SEWER DISPLAY

ALTERNATE 1 SEWER DISPLAY

ALTERNATE 2 SEWER DISPLAY

**APPENDIX B**

PIPE CAPACITIES AND DEMANDS

## **INTRODUCTION**

The following report represents the sanitary sewer analysis for Village Parkway Homes with two alternate options to carry wastewater to the sewer treatment plant. The project is a proposed 349-unit single-family development located in Section 17, Township 21 North, Range 18 East, Reno, Nevada. The purpose of this study is to estimate the peak sewer flows, in accordance with the criteria set forth in the Washoe County Department of Water Resources. The information for the proposed subdivision is listed below:

APN: 087-400-11

Area: 42.43 Acres

APN: 087-400-24

Area: 41.26 Acres

APN:087-400-23

Area: 40.91 Acres

The property surrounding this project is as follows:

North:	APN 087-400-15, Lee K Pearson
South:	Peavine View Estates (Existing)
East:	Village Parkway (Existing)
West:	APN 087-400-12, Liscom Family Trust; APN 087-400-09, Tonniel R Strickland, APN 087-400-06, Ferrel Family Trust

## **DESIGN STANDARDS**

The following design standards were used in designing the mains within Village Parkway Homes, and in analyzing the effects of connecting the Village Parkway Homes development to existing sewer facilities (reference Washoe County Department of Water Resources):

- Manning's roughness coefficient,  $n = 0.012$
- Pipe capacity in terms of one-half full. Maximum allowed by Washoe County is  $0.8D$ , where  $D$  is the nominal diameter of the pipe.

- Peak discharge of 270 gallons per capita per day
- Peaking factor of 3
- Minimum mean velocity of 2.5 feet per second
- Maximum mean velocity of 10 feet per second

### **EXISTING SANITARY SEWER FACILITIES**

Village Parkway Homes will utilize the existing treatment facility located west of Woodland Village Phase 22 and 23, for sewer treatment and disposal. Alternate 1 ties into an existing 10-inch gravity sewer main north of the site with a minimum slope of 0.0058 ft/ft. This existing sewer main carries wastewater directly to the sewer treatment plant. Alternate 2 ties into an existing 10-inch gravity sewer main east of the site with a minimum slope of 0.003 ft/ft. This existing sewer main carries wastewater to the Woodland Village lift station. Reference the *Update to Technical Memorandum 3 (2017 Facility Plan)*, performed by Farr West Engineering, for existing lift station and force main information.

### **PROPOSED SANITARY SEWER FACILITIES**

Village Parkway Homes will be served by proposed sanitary sewer mains comprised of 8-inch diameter SDR 35 PVC pipes. These mains will connect to a proposed on-site sanitary sewer lift station which will carry flows to the existing sewer mains in both alternate options via a sewer force main.

### **SEWER ANALYSIS**

The approximate location of the proposed sanitary sewer system servicing Village Parkway Homes is illustrated on the display map in the appendix of this report. Using the Washoe County Gravity Sewer Collection Design Standards, these 349 units will generate a peak flow of 282,690 gallons per day (gpd). The 80% capacities were found using Flowmaster. The flattest section of the on-site gravity sanitary sewer is an 8-inch diameter SDR 35 PVC pipe which has a slope of 0.005 ft/ft, the 80% full capacity of this pipe is 478,602 gpd and a half-full velocity of 3.1 ft/s and can serve approximately 591 units. The flow will then go through a proposed on-site sanitary lift station and a proposed sewer force main that will be designed by others.

Alternate 1 will combine 349 units from Village Parkway Homes and 480 units from the Diamond Peak lift station (per the *Update to Technical Memorandum 3 (2017 Facility Plan)*, by Farr West Engineering) for a



total demand of 671,490 gpd. The existing 10” sewer main carrying these flows at a slope of 0.0058 ft/ft has an 80%-full capacity of 1,141,937 gpd and velocity of 3.78 fps. These flows are carried to the sewer treatment plant through an existing 12-inch pipe with a slope of 0.0053 ft/ft. The 80%-full capacity of this is 1,775,072 gpd and has a velocity of 4.08 fps. Woodland Village contributes 1,087 units to this pipe as well, which brings the total combined demand to 1,551,960 gpd. These existing pipes will satisfy the demand for Alternate 1.

Alternate 2 will combine 349 units from Village Parkway Homes and 501 units from Woodland Village for a total demand of 688,500 gpd. The existing 10” sewer main carrying these flows at a minimum slope of 0.003 ft/ft has an 80%-full capacity of 827,275 gpd and velocity of 2.72 fps. These flows are then directed to the existing Woodland Village lift station, which will carry the flows to the existing sewer treatment plant. The remaining capacities for the Woodland Village lift station and force mains are shown in Table 1 (per the *Update to Technical Memorandum 3 (2017 Facility Plan)*, by Farr West Engineering). These numbers are based on the existing 1,085 ERU at the time. The adjusted capacities referenced in Table 1 shows additional contributions from Woodland Village and the proposed Village Parkway Homes, for a total demand of 1,672 ERU’s. The existing facilities will satisfy the demand for Alternate 2.

**Table 1: Remaining Capacity for Woodland Village Lift Station**

<b>Component</b>	<b>2017 Woodland Village Remaining Capacity (ERU’s)</b>	<b>Adjusted Woodland Village Remaining Capacity (ERU’s)</b>
Wet Well Storage	1,140	553
Force Main	1,184	597
Pump	4,120	3,533

**CONCLUSION**

The Village Parkway Homes will consist of 349 units that will generate a proposed peak flow demand of 282,690 gpd. The proposed 8-inch mains in the development have a minimum slope of 0.005 ft/ft. and will be directing flows to a sanitary sewer lift station. The two alternate options connecting to the existing facilities present adequate capacities for the additional demand produced by the site.

**APPENDIX A**



**VILLAGE PARKWAY  
HOMES  
VICINITY MAP**

N.T.S.

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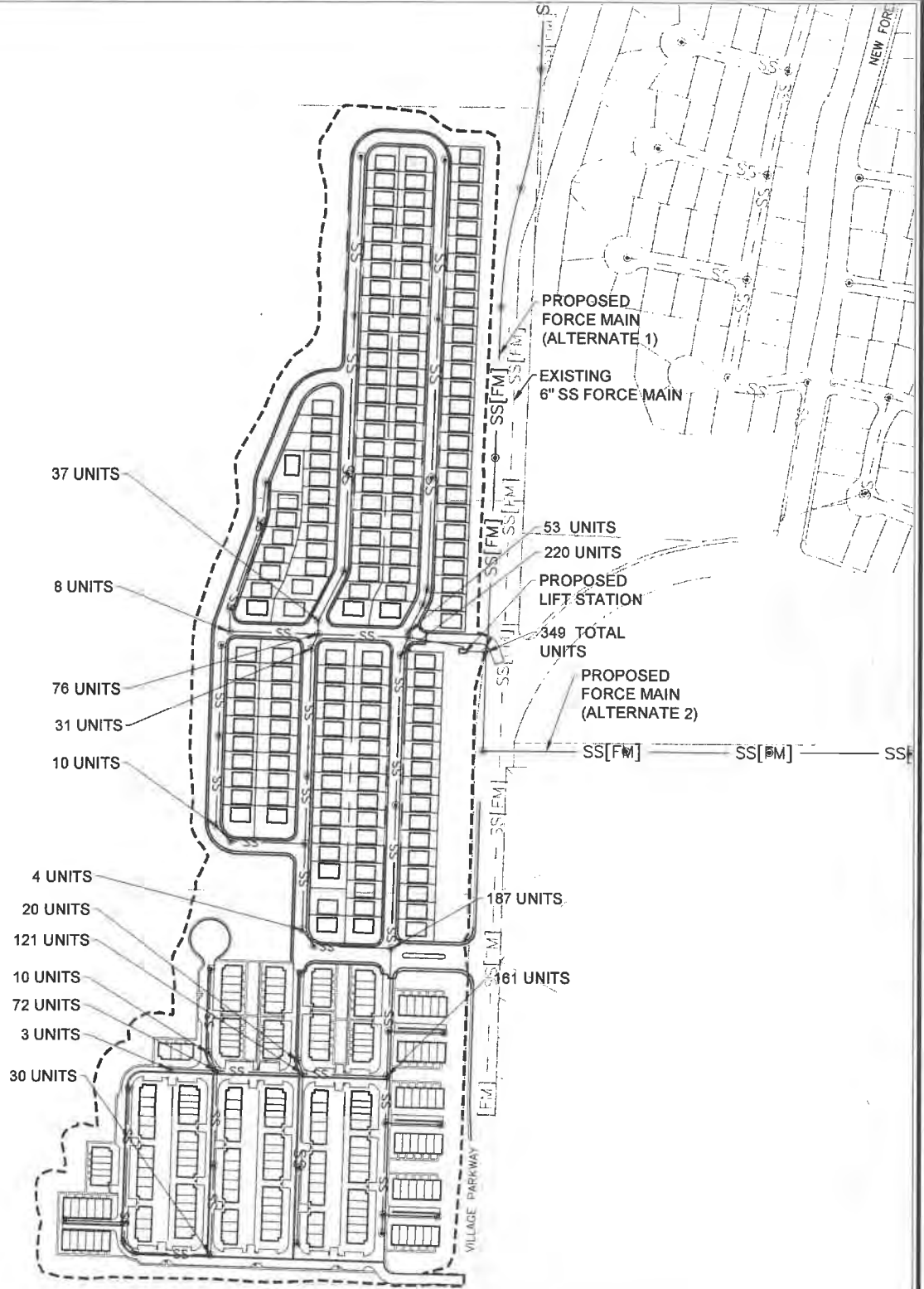
**SUMMIT** ENGINEERING CORPORATION  
5405 MAE ANNE AVENUE, RENO, NV, 89523  
PHONE: (775) 747-8550 FAX: (775) 747-8559

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VILLAGE PARKWAY  
HOMES  
ON-SITE SEWER DISPLAY

SCALE: 1" = 400'

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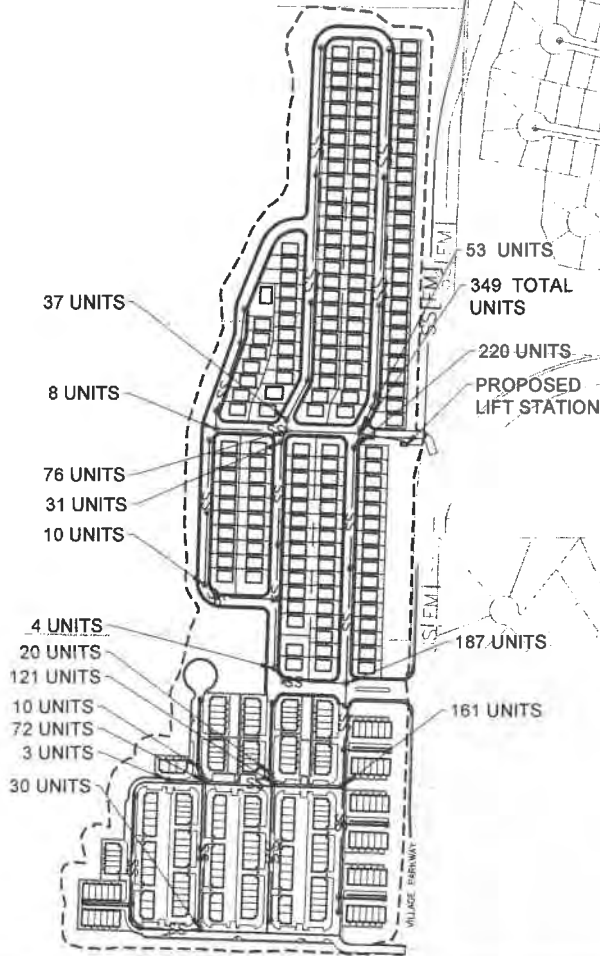
1323 LOTS (FROM LIFT STATION TO EX. FORCE MAIN)  
 EX. 10"SS @S=0.58%  
 1,469 LOT CAPACITY

EX. 12"SS @S=0.53%  
 2,191 LOT CAPACITY

1,916 LOTS

829 TOTAL LOTS  
 (349 UNITS FROM PROPOSED LIFT STATION, AND  
 480 LOTS FROM DIAMOND PEAK LIFT STATION)

1,087 LOTS (GRAVITY SYSTEM TO 15" MAIN)



VILLAGE PARKWAY  
 HOMES  
 ALTERNATE 1

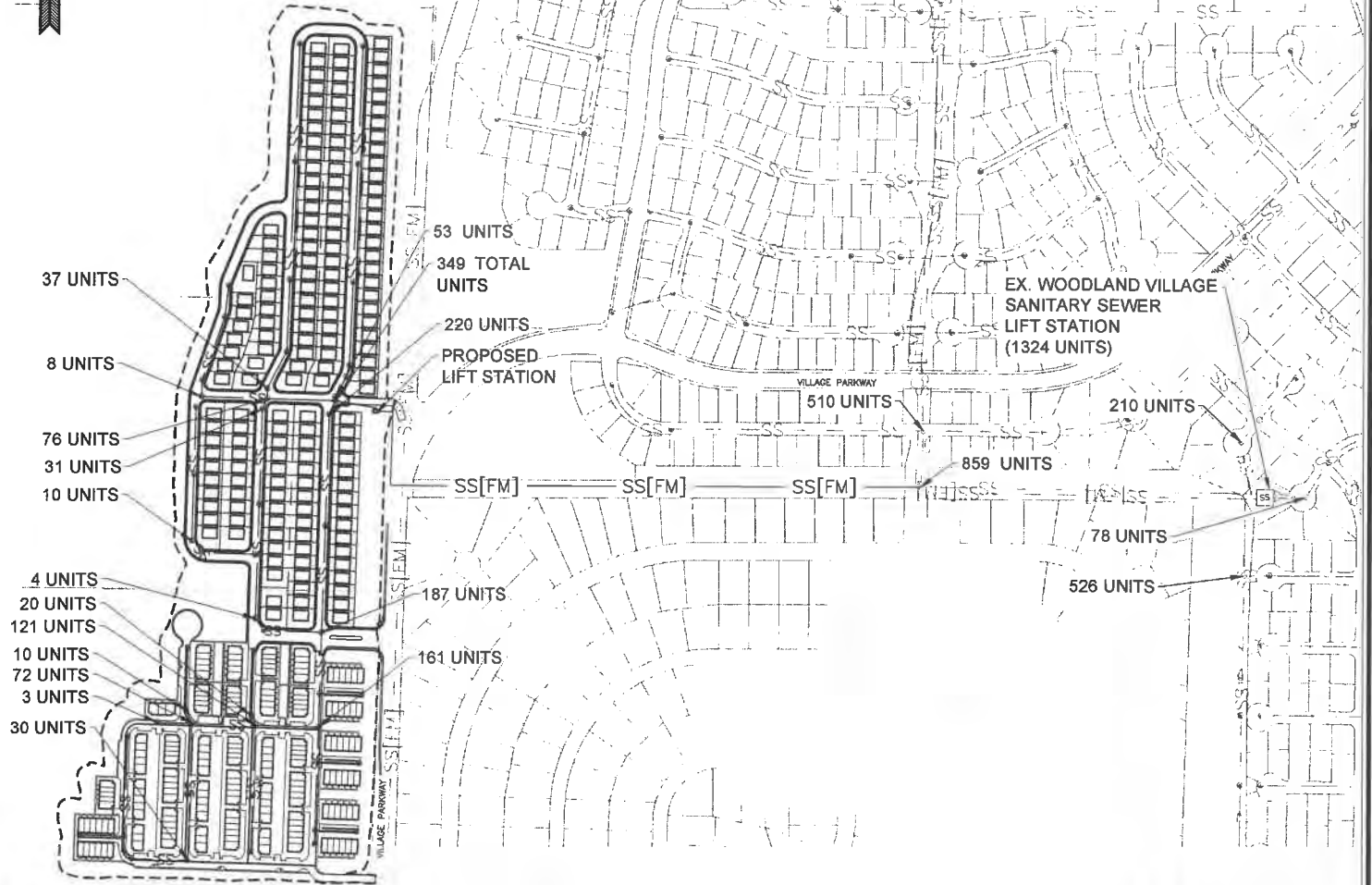
SCALE: 1" = 600'

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**N**



**VILLAGE PARKWAY  
HOMES  
ALTERNATE 2**

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OF  
**1**



**APPENDIX B**

## 8" MAIN 80% FULL CAPACITY @ S=0.5%

Project Description	
Friction Method	Manning Formula
Solve For	Discharge

---

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.005
Normal Depth	6.4
Diameter	8.0

---

Results	
Discharge	584,772
Flow Area	0.3
Wetted Perimeter	1.5
Hydraulic Radius	2.4
Top Width	0.53
Critical Depth	5.4
Percent Full	80.0
Critical Slope	0.007
Velocity	3.02
Velocity Head	0.14
Specific Energy	0.68
Froude Number	0.711
Maximum Discharge	643,543
Discharge Full	598,252
Slope Full	0.005
Flow Type	Subcritical

---

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

---

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	0.0
Downstream Velocity	0.00
Upstream Velocity	0.00
Normal Depth	6.4
Critical Depth	5.4
Channel Slope	0.005
Critical Slope	0.007

## 8" MAIN DEMAND @ S=0.50%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0050
Diameter	8.0
Discharge	282,690

Results	
Normal Depth	3.9
Flow Area	0.2
Wetted Perimeter	1.0
Hydraulic Radius	2.0
Top Width	0.67
Critical Depth	3.7
Percent Full	48.4
Critical Slope	0.0058
Velocity	2.62
Velocity Head	0.11
Specific Energy	0.43
Froude Number	0.920
Maximum Discharge	643,543
Discharge Full	598,252
Slope Full	0.0011
Flow Type	Subcritical

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	38.4
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	3.9
Critical Depth	3.7
Channel Slope	0.0050
Critical Slope	0.0058



## ALT. 1 EX.10" MAIN 80% FULL CAPACITY @ S=0.58%

Project Description	
Friction Method	Manning Formula
Solve For	Discharge

---

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0058
Normal Depth	8.0
Diameter	10.0

---

Results	
Discharge	1,141,937
Flow Area	0.5
Wetted Perimeter	1.8
Hydraulic Radius	3.0
Top Width	0.67
Critical Depth	7.2
Percent Full	80.0
Critical Slope	0.0075
Velocity	3.78
Velocity Head	0.22
Specific Energy	0.89
Froude Number	0.795
Maximum Discharge	1,256,705
Discharge Full	1,168,261
Slope Full	0.0055
Flow Type	Subcritical

---

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

---

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	80.0
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	8.0
Critical Depth	7.2
Channel Slope	0.0058
Critical Slope	0.0075

## ALT. 1 EX.10" MAIN DEMAND @ S=0.58%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

---

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0058
Diameter	10.0
Discharge	671,490

---

Results	
Normal Depth	5.4
Flow Area	0.3
Wetted Perimeter	1.4
Hydraulic Radius	2.6
Top Width	0.83
Critical Depth	5.4
Percent Full	54.4
Critical Slope	0.0058
Velocity	3.43
Velocity Head	0.18
Specific Energy	0.64
Froude Number	1.001
Maximum Discharge	1,256,705
Discharge Full	1,168,261
Slope Full	0.0019
Flow Type	Critical

---

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

---

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	55.8
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	5.4
Critical Depth	5.4
Channel Slope	0.0058
Critical Slope	0.0058

## ALT. 1 EX.12" MAIN DEMAND @ S=0.53%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0053
Diameter	12.0
Discharge	551,960

Results	
Normal Depth	4.5
Flow Area	0.3
Wetted Perimeter	1.3
Hydraulic Radius	2.5
Top Width	0.97
Critical Depth	4.6
Percent Full	37.8
Critical Slope	0.0049
Velocity	3.14
Velocity Head	0.15
Specific Energy	0.53
Froude Number	1.045
Maximum Discharge	1,953,473
Discharge Full	1,815,992
Slope Full	0.0005
Flow Type	Supercritical

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	37.8
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	4.5
Critical Depth	4.6
Channel Slope	0.0053
Critical Slope	0.0049



## ALT. 1 EX12" MAIN 80% FULL CAPACITY @ S=0.53%

Project Description	
Friction Method	Manning Formula
Solve For	Discharge
Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0053
Normal Depth	9.6
Diameter	12.0
Results	
Discharge	1,775,072
Flow Area	0.7
Wetted Perimeter	2.2
Hydraulic Radius	3.7
Top Width	0.80
Critical Depth	8.5
Percent Full	80.0
Critical Slope	0.0069
Velocity	4.08
Velocity Head	0.26
Specific Energy	1.06
Froude Number	0.783
Maximum Discharge	1,953,473
Discharge Full	1,815,992
Slope Full	0.0051
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	80.0
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	9.6
Critical Depth	8.5
Channel Slope	0.0053
Critical Slope	0.0069

## ALT. 2 EX.10" MAIN DEMAND @ S=0.30%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth

---

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0030
Diameter	10.0
Discharge	688,500

---

Results	
Normal Depth	6.9
Flow Area	0.4
Wetted Perimeter	1.6
Hydraulic Radius	2.9
Top Width	0.77
Critical Depth	5.5
Percent Full	68.8
Critical Slope	0.0058
Velocity	2.66
Velocity Head	0.11
Specific Energy	0.68
Froude Number	0.651
Maximum Discharge	903,816
Discharge Full	840,208
Slope Full	0.0020
Flow Type	Subcritical

---

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

---

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	55.8
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	6.9
Critical Depth	5.5
Channel Slope	0.0030
Critical Slope	0.0058

## ALT. 2 EX10" MAIN 80% FULL CAPACITY @ S=0.30%

Project Description	
Friction Method	Manning Formula
Solve For	Discharge

---

Input Data	
Roughness Coefficient	0.012
Channel Slope	0.0030
Normal Depth	8.0
Diameter	10.0

---

Results	
Discharge	821,275
Flow Area	0.5
Wetted Perimeter	1.8
Hydraulic Radius	3.0
Top Width	0.67
Critical Depth	6.0
Percent Full	80.0
Critical Slope	0.0062
Velocity	2.72
Velocity Head	0.11
Specific Energy	0.78
Froude Number	0.572
Maximum Discharge	903,816
Discharge Full	840,208
Slope Full	0.0029
Flow Type	Subcritical

---

GVF Input Data	
Downstream Depth	0.0
Length	0.0
Number Of Steps	0

---

GVF Output Data	
Upstream Depth	0.0
Profile Description	N/A
Profile Headloss	0.00
Average End Depth Over Rise	0.0
Normal Depth Over Rise	80.0
Downstream Velocity	Infinity
Upstream Velocity	Infinity
Normal Depth	8.0
Critical Depth	6.0
Channel Slope	0.0030
Critical Slope	0.0062

**PRELIMINARY HYDROLOGY REPORT FOR  
VILLAGE PARKWAY HOMES  
COLD SPRINGS VALLEY  
WASHOE COUNTY, NEVADA**

**Prepared for:**

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**Prepared by:**

**DEW Hydrology  
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**March 8, 2021**



*March 8, 2021*



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## **1.0 INTRODUCTION**

### **1.1 Introduction and Location**

This report documents a hydrology study for the proposed Village Parkway Homes (VPH) project in unincorporated Washoe County, Nevada. The project is located in Cold Springs Valley, just west of Woodland Village, about 10 miles north of Reno, NV (Figure 1). The area planned for development is in APNs 087-400-23, 087-400-24, and 087-400-11. It lies in Section 17, T 21 N, R 18 E, MDBM. The area of interest is shown on Flood Insurance Rate Map (FIRM) panels 32031C2805H and 32031C2825H (Figure 4) with an effective date of June 18, 2013. The project is in Flood Zone X (unshaded), an area of minimal flood hazard.

This study was conducted following procedures described in the Truckee Meadows Regional Drainage Manual (Manual).

### **1.2 Existing Site Conditions and Historic Drainage Patterns**

Cold Springs Valley is a closed drainage basin with its terminus in the Whites Lake playa. Historically, stormwater drained from the Peterson Mountain and other ranges south through Cold Springs Valley to Whites Lake. Cold Springs Valley slopes to the south at about 4 to 5%. Natural vegetation consists of sagebrush and grasses. The soils in the valley are highly permeable. The Village Parkway Homes project lies at the eastern base of Peterson Mountain and receives runoff from ephemeral channels flowing onto the project area. Permeable soils at the base of the mountain infiltrated appreciable quantities of the runoff. The remainder flowed into the valley then south to the White Lake Playa. Previous studies of the project area set the required flow limits at Mud Springs Road at **230 cfs** for 100-year, 24-hour event.

### **1.3 Project Description**

The proposed project consists of 181 individual residential homes on 3,600 (minimum) square foot lots and 37 townhome buildings with 191 units plus the required parking spaces. The project plans to mitigate the impacts of the project on flood rates through the construction of 3 retention/detention ponds.



## 2.0 PREVIOUS STUDIES

Previous studies that have a bearing on this application are summarized below.

In 1985, SEA Engineers/Planners completed Percolation Investigation Sweger Estate Cold Springs Valley. This was a percolation investigation of Section 9 and the west half of Section 15. The results showed very high percolation rates in Section 9 (<2 minutes per inch) and were slightly slower in Section 15 (5 minutes per inch).

Summit Engineers summarized another percolation study in a letter report in October, 1998. It stated that almost all of the Woodland Village project site was composed of permeable soils.

In February, 1999, Nimbus Engineers prepared Hydrology Report (Existing Conditions) Cold Springs 2,000 (updated March, 2000). This report divided the drainage basin into 15 sub-basins and prepared a hydrologic (HEC-HMS) model of the area. Village Parkway Homes lies within Watersheds L, P and Q in their report. This report estimated that the 100-year, 24 hour peak flow at Mud Springs Road would be 97 cfs.

In July, 1999, Nimbus prepared Flood Control Master Plan for Cold Springs 2,000, Inc. This was based on a proposed layout for Woodland Village and included the affect of the permeable soils on flow rates. This study used the HEC-1 model.

Request for Letter of Map Revision (LOMR) Cold Springs 2,000 was prepared by Nimbus Engineers in March, 2000. This report used the existing conditions HEC-HMS model with the affects of the permeable soils included to revise the flow rates in the Zone A portions of the project. Based on comments from FEMA, the impacts of the soils was modified and the 100-year, 24-hour flow rate at Mud Springs Road was set at 230 cfs.

In 2006, Nimbus Engineers updated the Master Plan based on revised development plans.

In 2013, Michael Baker Jr. prepared a Letter of Map Revision (LOMR) for the northern part of Cold Springs Valley (basically offsite watersheds A to J from the 1999 Nimbus report) to define the floodplain in those areas.

DEW Hydrology prepared the Updated Hydrology Master Plan For Woodland Village Subdivision Cold Springs Valley Washoe County, Nevada in 2016. It analyzed the impacts of developing Village 20 in Woodland Village and also updated the Master Plan for full build-out conditions through phase 23.

Drainage reports have been prepared by Summit Engineers for different villages (phases) of Woodland Village as they were completed. Also, Letter-Reports have been submitted by Nimbus and Quad Knopf to address various interim conditions.



## 3.0 HYDROLOGIC ANALYSIS

### 3.1 Methodology

The U.S Army Corps of Engineers HEC-1 (v. 4.1R) computer program was used in this analysis. This program incorporates watershed area, time of concentration, curve number and precipitation data to compute peak flow rates and runoff volumes. These parameters and the values used in the model are discussed below. Procedures described in the Truckee Meadows Regional Drainage Manual (TMRDM) were followed in this analysis. Because the area of the VPH project has been included in the Woodland Village models, the most recent (2016) Woodland Village model is being used as the starting point for this project. Models were developed for the 100-year and 5-year events for VPH.

### 3.2 Rainfall Depth and Distribution

The Woodland Village project has used a 100-year, 24-hour precipitation depth of 4.59 inches and a 5-year precipitation depth of 2.56 inches. A check on the NOAA website showed that rainfall depths had increased. The 100-year depth at VPH is 4.94 inches and Michael Baker Jr., used 5.01 inches for the 100-year precipitation value in their 2013 LOMR for areas further north and higher in elevation. Previously used rainfall depths are still within the confidence limits, so they were used in the model with a balanced storm distribution as was done in earlier studies.

### 3.3 Watershed Delineation

Figure 2 shows the watershed map used in the previous Woodland Village Master Plan update through Phase 20. The watershed boundaries affecting VPH (L1, L2, P, and Q) are based on topographic data from USGS topographic maps. The proposed offsite and onsite watershed boundaries (Figure 2B) are based on existing topography and planned grading.

### 3.4 Runoff Curve Number

To calculate the runoff curve number (CN), the soil types within each watershed were identified by hydrologic soil groups. Soils have been classified by the U.S. National Resource Conservation Service (NRCS) into 4 hydrologic soil groups: A, B, C, and D. Infiltration rates decrease from soil groups A through D. Group A soils have a rapid infiltration rate and include very porous soils such as sands. Groups B and C have intermediate infiltration rates. Group D soils have a very slow infiltration rate which results in a larger percentage of the rainfall contributing to runoff. The hydrologic soil groups were obtained from the NRCS web soil survey found at <http://websoilsurvey.nrcs.usda.gov/app>. This soils map (Figure 4) shows that soils in the mountainous areas west of the project are Group D, while the project area itself is mostly Group A with minor amounts of Group C.

Relative soil moisture content is described in the NRCS methodology by the term “antecedent moisture condition” or AMC. Three different relative conditions are describe by the NRCS, AMC I, II and III. AMC I is an extremely dry condition where soil moisture has been depleted and infiltration rates for the soil are near their maximum. AMC III is a saturated condition with limited infiltration and AMC II is an average condition. As prescribed in the “Truckee Meadows Regional Drainage Manual”, AMC II was used in this study.

Vegetation also is a factor in evaluating curve number. An investigation of the site showed that the vegetation type in the study area is sagebrush and cheatgrass in fair condition. The areas are developed with lot sizes from 0.25 to 0.3 acres. Curve numbers were based on the characteristics described above and Table 702 of the Regional Drainage manual. Curve number calculations are shown in Appendix B. In the area northwest of the development, the two I watersheds used the standard curve number input into the model with the 80% diversion rate used in previous models. The 2 O watersheds use a 4-inch initial abstraction and a constant loss rate of 0.1 inch/hour as was used in previous models for watershed O.

### **3.5 Overland Flow Infiltration**

As detailed in previous Woodland Village reports, the soils in the project area consist of highly permeable sands and gravels. Studies showed that using the curve number method resulted in flow rates that were too high. To correct this, a diversion feature in the HEC models was used to simulate infiltration and reduce the flow rates entering and passing through the Woodland Village area. These are included in the HEC-1 model used in this study. The only watershed directly draining to VPH with a diversion is Watershed P (Figures 2 and 2B) which had a diversion rate of 50%. Because the VPH development will cover the permeable soils at the base of Peterson Mountain, this diversion was removed from the model. Diversions from other areas of the Cold Springs Drainage Basin, typically 50% to 70% of the flow rate, were left in the model.

### **3.6 Watershed Lag Time**

Watershed time of concentration is the time it takes for water to reach the watershed outlet from the most hydraulic distant point in the watershed. The watershed lag time is used for the SCS methodology in the HEC-1 program. Using the SCS methodology, the lag time (TLAG) is equal to 0.6 times the time of concentration ( $T_c$ ), or  $TLAG = 0.6 \times T_c$ . Table 703 and Figure 701 from the Regional Drainage Manual were used to calculate time of concentration for most watersheds. Equation 710 in the Manual was used. For basins with an area exceeding 1 square mile or with a slope greater than 10%. Calculations are presented in Appendix B.



### 3.7 Hydrograph Routing

Channel and overland flow routing were performed with the Muskingum-Cunge method. This method takes into account channel characteristics such as shape, slope, length and roughness. The modified puls method was used for reservoir routing.

### 3.8 Summary of Watershed Parameters

The parameters for the new watersheds created or modified for VPH are shown in Table 1.

WATERSHED	AREA, AC	AREA, SQ MI	CURVE NO.	LAG, HR
L1	18.6	0.029	77	0.21
L3	7.44	0.018	77	0.2
P	19.84	0.031	77	0.1
Q	33.28	0.052	77	0.19
Q2	8.32	0.013	77	0.16
VPH-1	22.63	0.035	77	0.19
VPH-2	6.32	0.01	77	0.16
VPH-3	6.56	0.01	77	0.15
VPH-4	7.44	0.011	77	0.15
VPH-5	3.38	0.005	77	0.13

### 3.9 Results

The proposed VPH project was inserted into both the model evaluating the project on the Woodland Village Phase 20 and at full build out. As mentioned earlier, the control point used to regulate flows leaving Cold Springs Valley was Mud Springs Road (HEC-1 model node ABMSR). Because the Village Parkway Homes project is partially upstream and partially downstream of this point (Figure 2B) and diverts some flow from upstream to downstream of ABMSR, the proposed conditions flow rate at this point is not entirely reliable. Therefore, we compared the existing and proposed flow rates at Cold Springs Road, downstream of the project area, to measure the effectiveness of the detention/retention ponds (HEC-1 model nodes ABCDSR and BLCSRDP). Flow rates at those nodes from the Nimbus 2001 report were used for comparison. The results are shown in Table 2.

MODEL NODE	PHASE 20 MODEL	FULL BUILD-OUT	LIMIT
ABMSR	195	194	230
ABDCSP	284	284	337
BLCSRDP	291	291	342

Table 2 shows that the detention/retention ponds maintain the flow rates below the required limits at all 3 locations. Therefore, the project will not impact downstream property owners.

Using the Phase 20 model as a base, the proposed conditions 5-year flow rates were 66 cfs both Above and Below Cold Springs Road. Both of these flow rates are below the rates from the Woodland Village Phase 23 report of 71 cfs Above Cold Springs Road and 72 cfs Below Cold Springs Road. The proposed rate Above Mud Springs Road is 54 cfs which is below the previous rate of 65 cfs.

### 3.10 Detention/Retention Ponds

Three detention/retention ponds are proposed for the project. One, the west pond, (VPHRP) will intercept offsite flow from Peterson Mountain. It will collect this flow and route it to the southeast pond(Figure 2B). VPHRP has a 36-inch pipe outlet at elevation 5061.5 feet. This is 1.5 feet above the bottom of the pond so it will have 1.5 feet (18 inches) of retention volume. Infiltration tests showed an infiltration rate of 23 inches/hour (Appendix D). Hence, this water would infiltrate in less than an hour.

Because of the high infiltration rate, infiltration would likely occur in the pond during the storm event. This assumption has been made in other ponds in Cold Springs Valley. The rate of infiltration was calculated by first reducing the infiltration rate by 10% to 21 incher/hour. This rate was used over the pond area at the elevation of the outlet pipe’s invert, 0.57 acres at 5061.5 feet. The resulting rate of infiltration, 12 cfs was included in the proposed conditions models.

The northeast pond (NEPD) will collect runoff from offsite watershed L3 and onsite watershed VPH-1 (Figure 2B). This pond has an 18-inch outlet at elevation 5060 feet. It discharges to the channel on the east side of Village Parkway.

The southeast pond collects the water from the west pond and from onsite watersheds VPH-2, VPH-3, VPH-4 and VPH-5. It has a 30-inch pipe at elevation 5058.15 feet. It discharges to the channel on the east side of Village Parkway. The flow rates and water surface elevations for the ponds during the 100-year, 24-hour event are shown in Table 3.

<b>TABLE 3. DETENTION/RETENTION POND DATA FOR 100-YEAR EVENT</b>				
POND	Q in, cfs	Q out, cfs	Water Elev., ft	Freeboard, ft
West	131	44	5066.4	0.6
Northeast	71	19	5062.68	0.3
Southeast	81	44	5063.05	0.45



#### **4.0 SUMMARY AND FINDINGS**

Village Parkway Homes (VPH) will be constructed west of the Woodland Village subdivision. It will consist of single-family homes and townhomes. Three detention/retention basins will be constructed as part of the project. These ponds will mitigate the impacts of VPH on peak flow rates. Modeling results show that the project can be constructed without impacting adjacent or downstream properties. Flow rates remain within the allowed limit of 230 cfs at Mud Springs Road, 337 cfs above Cold Springs Road, and 342 cfs below Cold Springs Road for the 100-year 24-hour storm.

## 6.0 REFERENCES

DEW Hydrology, Updated Hydrology Master Plan for Woodland Village Subdivision Phase 23 Cold Springs Valley, Washoe County, NV, September 5, 2019.

Nimbus Engineers, Hydrology Report (Existing Conditions) Cold Springs 2,000, Revised March, 2000.

Nimbus Engineers, Request for Letter of Map Revision, (LOMR) Cold Springs 2,000, March 2000.

Nimbus Engineers, Cold Springs Updated Storm Drainage Report, May, 2001.

Nimbus Engineers, Updated Storm Drainage Report Woodland Village Cold Springs Valley, February, 2003.

HDR, Letter of Map Revision White Lake City of Reno, NV, July, 2009

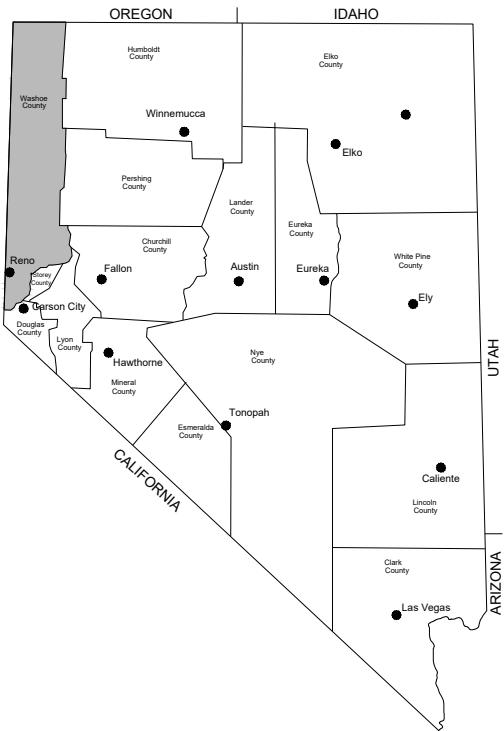
U.S. Army Corps of Engineers, Hydrologic Engineering, Computer Program 723-X6-L2010, (HEC-1) version 4.1R, updated by HEC-1.com, 2000. .

National Weather Service Website: [http://dipper.nws.noaa.gov/hdsc/pfds/sa/nv\\_pfds.html](http://dipper.nws.noaa.gov/hdsc/pfds/sa/nv_pfds.html)

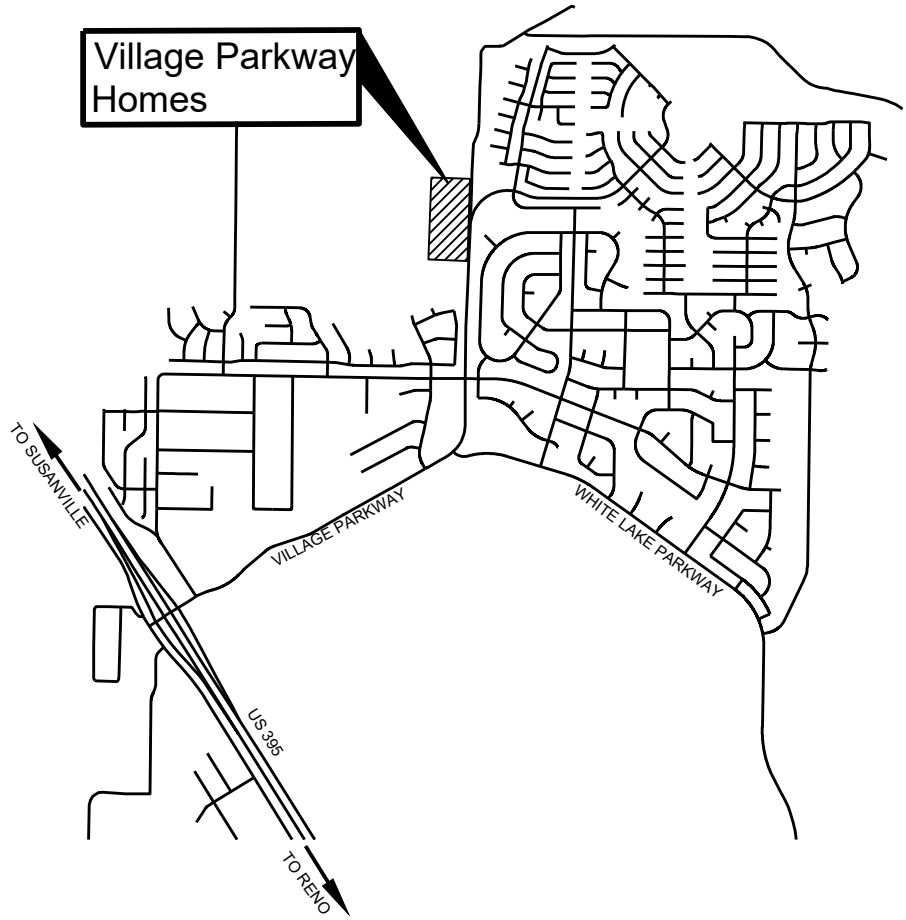
Natural Resource Conservation Service Website: <http://websoilsurvey.nrcs.usda.gov/app>

City of Reno, City of Sparks, and Washoe County, Truckee Meadows Regional Drainage Manual, April, 2009.

**APPENDIX A**  
**FIGURES**



State of Nevada



Vicinity Map

**FIGURE 1**  
 Vicinity Map  
 Village Parkway Homes  
 Reno, Nevada  
 February 4, 2021

**DEW Hydrology**  
 10180 Grizzly Hill Court  
 Reno, Nevada 89521  
 Phone: (775) 815-2293



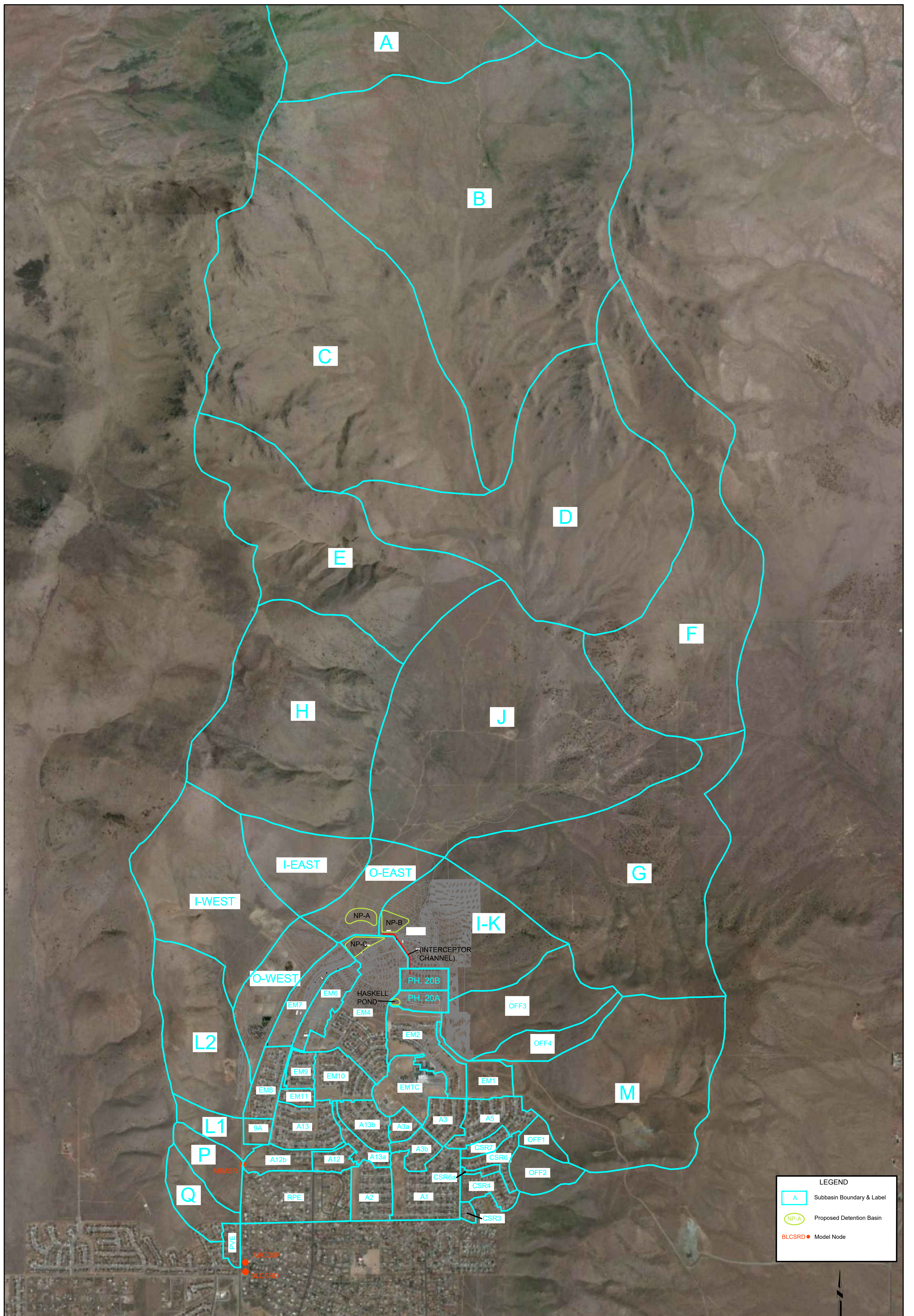


FIGURE 2  
Phase 20 Watershed Map  
Village Parkway Homes  
Reno, Nevada  
March 2, 2021



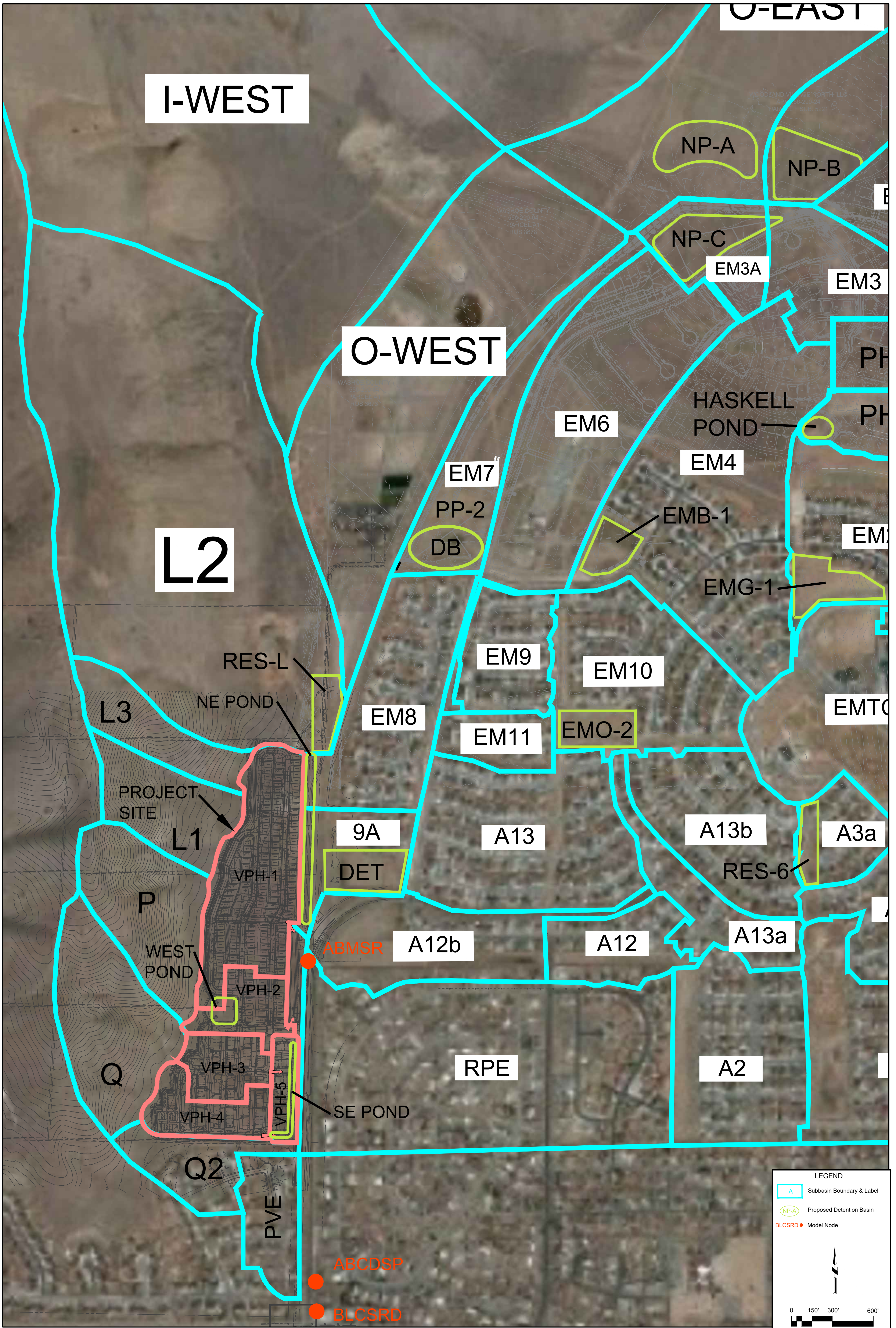
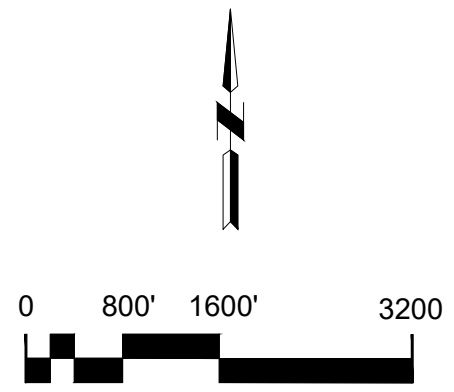
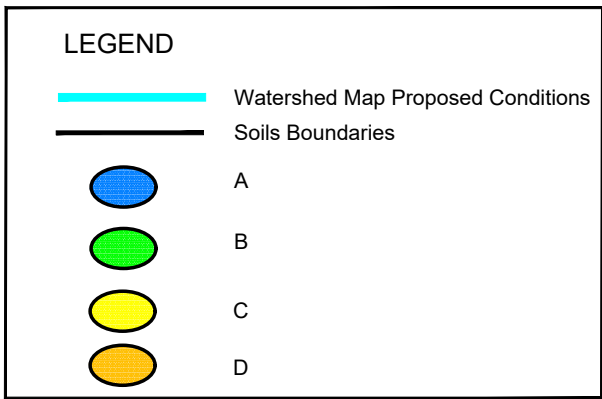
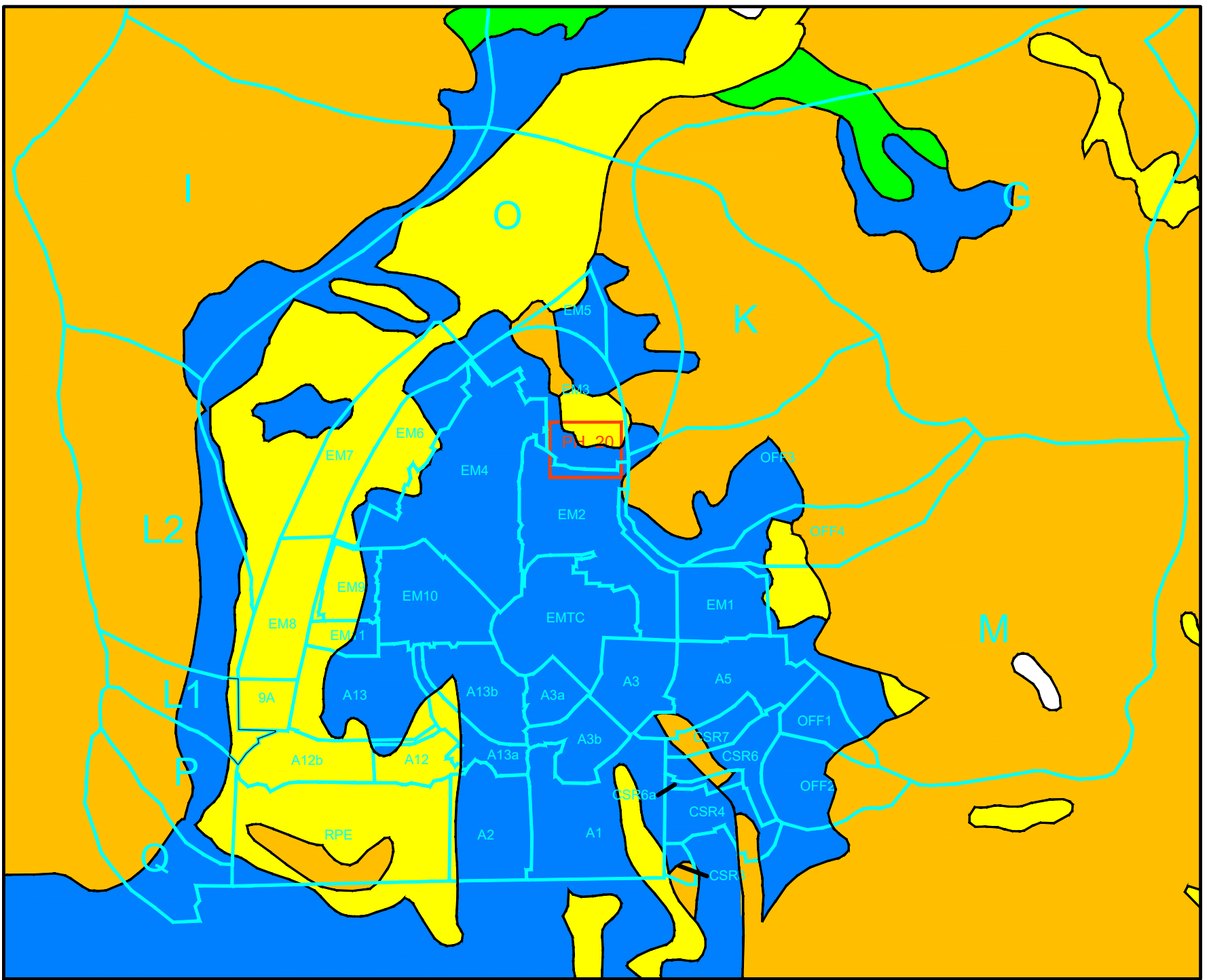


FIGURE 2B  
 Local Watershed Map - Proposed Conditions  
 Village Parkway Homes  
 Reno, Nevada  
 February 4, 2021





**FIGURE 3**  
 Soils Map  
 Village Parkway  
 Reno, Nevada  
 January 29, 2021

**DEW Hydrology**  
 10180 Grizzly Hill Court  
 Reno, Nevada 89521  
 Phone: (775) 815-2293

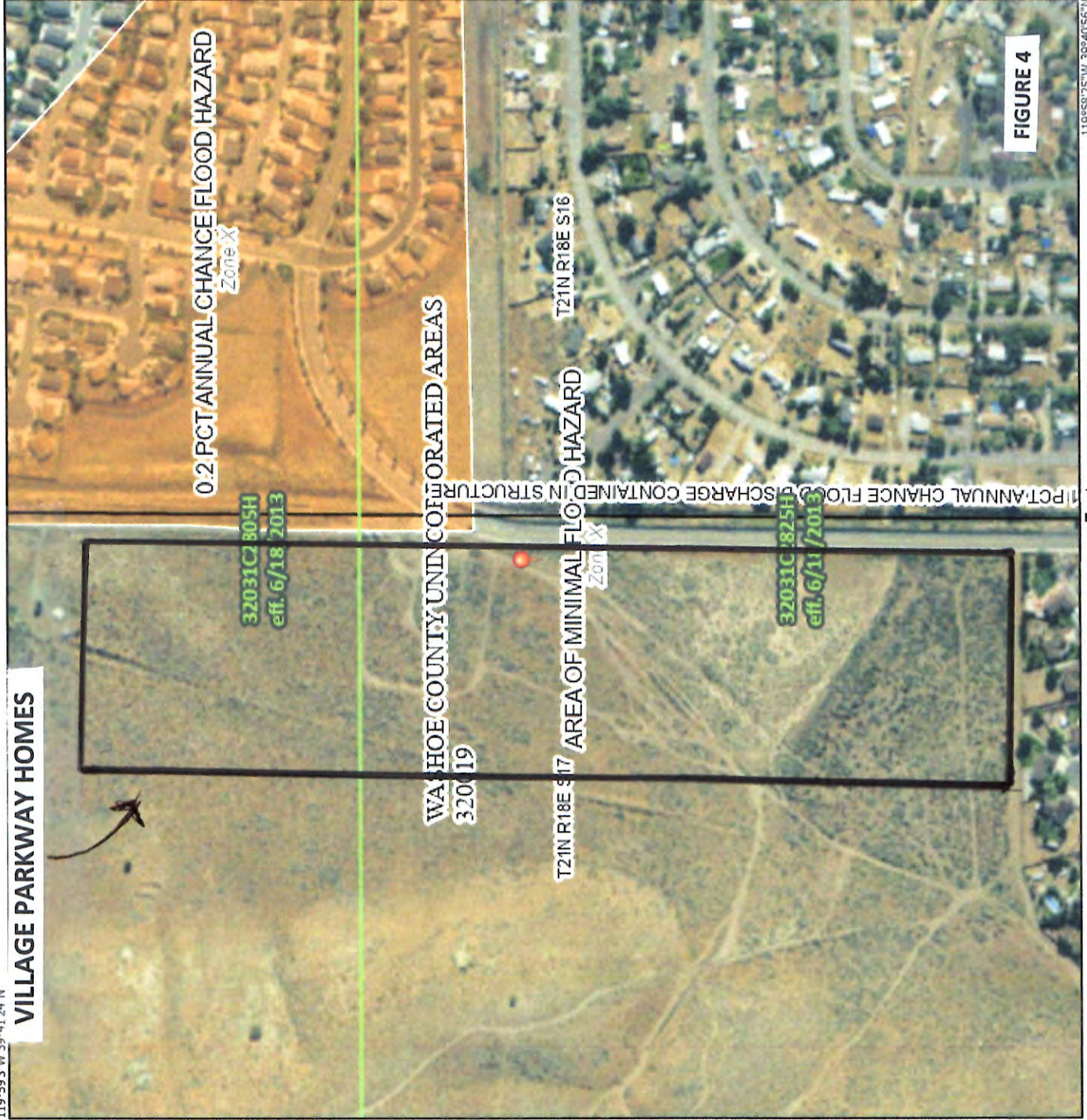


# National Flood Hazard Layer FIRMette



119°59'3"W 39°41'24"N

VILLAGE PARKWAY HOMES



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

**SPECIAL FLOOD HAZARD AREAS**

- Without Base Flood Elevation (BFE) Zone A, V, A99
- With BFE or Depth Zone AE, AO, AH, VE, AR
- Regulatory Floodway

**OTHER AREAS OF FLOOD HAZARD**

- 0.2% Annual Chance Flood Hazard. Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
- Future Conditions 1% Annual Chance Flood Hazard Zone X
- Area with Reduced Flood Risk due to Levee. See Notes. Zone X
- Area with Flood Risk due to Levee Zone D

**OTHER AREAS**

- NO SCREEN Area of Minimal Flood Hazard Zone X
- Effective LOMRS
- Area of Undetermined Flood Hazard Zone D

**GENERAL STRUCTURES**

- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

**OTHER FEATURES**

- Cross Sections with 1% Annual Chance Water Surface Elevation
  - 20.2
  - 17.5
- Coastal Transect
- Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

**MAP PANELS**

- Digital Data Available
- No Digital Data Available
- Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards. The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 3/7/2021 at 1:16 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

Feet 1:6,000

Basemap: USGS National Map; Orthoimagery: Data refreshed October, 2020



**APPENDIX B**  
**SUPPORTING CALCULATIONS**





NOAA Atlas 14, Volume 1, Version 5  
 Location name: Reno, Nevada, USA\*  
 Latitude: 39.6802°, Longitude: -119.9686°  
 Elevation: 5068.9 ft\*\*



\* source: ESRI Maps  
 \*\* source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin,  
 Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao,  
 Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

**PF tabular**

<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.114 (0.095-0.130)	0.141 (0.118-0.163)	0.187 (0.159-0.220)	0.232 (0.196-0.275)	0.310 (0.256-0.371)	0.384 (0.310-0.466)	0.473 (0.371-0.583)	0.583 (0.440-0.732)	0.766 (0.549-0.991)	0.938 (0.645-1.24)
10-min	0.173 (0.144-0.197)	0.214 (0.180-0.249)	0.285 (0.242-0.335)	0.354 (0.299-0.419)	0.471 (0.390-0.565)	0.584 (0.471-0.709)	0.720 (0.564-0.888)	0.888 (0.671-1.11)	1.17 (0.835-1.51)	1.43 (0.981-1.89)
15-min	0.214 (0.179-0.245)	0.265 (0.223-0.308)	0.353 (0.299-0.416)	0.438 (0.370-0.519)	0.584 (0.484-0.701)	0.723 (0.584-0.879)	0.892 (0.699-1.10)	1.10 (0.831-1.38)	1.45 (1.03-1.87)	1.77 (1.22-2.34)
30-min	0.288 (0.241-0.330)	0.357 (0.300-0.415)	0.474 (0.403-0.559)	0.590 (0.499-0.699)	0.786 (0.651-0.943)	0.975 (0.786-1.18)	1.20 (0.942-1.48)	1.48 (1.12-1.86)	1.95 (1.39-2.52)	2.38 (1.64-3.15)
60-min	0.356 (0.298-0.408)	0.442 (0.371-0.513)	0.587 (0.499-0.692)	0.730 (0.617-0.865)	0.974 (0.806-1.17)	1.21 (0.973-1.47)	1.49 (1.17-1.83)	1.83 (1.39-2.30)	2.41 (1.73-3.12)	2.95 (2.03-3.90)
2-hr	0.473 (0.420-0.541)	0.588 (0.523-0.674)	0.753 (0.663-0.863)	0.899 (0.783-1.03)	1.13 (0.960-1.30)	1.34 (1.11-1.55)	1.58 (1.29-1.86)	1.91 (1.51-2.33)	2.51 (1.90-3.15)	3.08 (2.26-3.94)
3-hr	0.581 (0.523-0.654)	0.720 (0.653-0.816)	0.898 (0.808-1.01)	1.05 (0.935-1.19)	1.26 (1.11-1.44)	1.46 (1.26-1.67)	1.69 (1.44-1.95)	2.02 (1.68-2.37)	2.60 (2.10-3.18)	3.15 (2.49-3.98)
6-hr	0.873 (0.791-0.971)	1.08 (0.984-1.21)	1.33 (1.20-1.49)	1.52 (1.37-1.71)	1.78 (1.58-2.00)	1.97 (1.73-2.22)	2.16 (1.88-2.46)	2.41 (2.07-2.77)	2.93 (2.48-3.42)	3.44 (2.87-4.05)
12-hr	1.24 (1.12-1.38)	1.55 (1.40-1.73)	1.94 (1.74-2.16)	2.25 (2.01-2.51)	2.66 (2.36-2.98)	2.98 (2.61-3.36)	3.30 (2.86-3.76)	3.63 (3.10-4.18)	4.07 (3.40-4.76)	4.44 (3.65-5.27)
24-hr	1.65 (1.48-1.86)	2.08 (1.87-2.34)	2.67 (2.39-3.00)	3.15 (2.80-3.54)	3.82 (3.36-4.32)	4.36 (3.79-4.96)	4.93 (4.24-5.66)	5.53 (4.69-6.40)	6.36 (5.29-7.47)	7.02 (5.74-8.36)
2-day	2.06 (1.82-2.35)	2.62 (2.31-2.99)	3.43 (3.02-3.92)	4.10 (3.59-4.70)	5.06 (4.37-5.84)	5.84 (4.99-6.79)	6.68 (5.62-7.85)	7.57 (6.28-9.00)	8.84 (7.16-10.7)	9.88 (7.85-12.2)
3-day	2.29 (2.01-2.62)	2.92 (2.57-3.35)	3.89 (3.41-4.47)	4.69 (4.09-5.40)	5.85 (5.03-6.78)	6.80 (5.77-7.95)	7.84 (6.55-9.24)	8.95 (7.36-10.7)	10.5 (8.46-12.8)	11.9 (9.33-14.7)
4-day	2.52 (2.20-2.90)	3.23 (2.82-3.72)	4.35 (3.80-5.02)	5.29 (4.58-6.11)	6.64 (5.69-7.73)	7.77 (6.56-9.11)	9.00 (7.48-10.6)	10.3 (8.43-12.3)	12.3 (9.75-14.9)	13.9 (10.8-17.1)
7-day	3.00 (2.60-3.51)	3.88 (3.35-4.53)	5.29 (4.56-6.19)	6.46 (5.54-7.56)	8.13 (6.88-9.59)	9.51 (7.95-11.3)	11.0 (9.07-13.2)	12.6 (10.2-15.3)	14.9 (11.8-18.5)	16.8 (13.1-21.1)
10-day	3.44 (2.99-4.00)	4.47 (3.88-5.19)	6.10 (5.28-7.09)	7.41 (6.39-8.63)	9.28 (7.90-10.9)	10.8 (9.08-12.7)	12.4 (10.3-14.8)	14.1 (11.5-17.0)	16.5 (13.2-20.3)	18.5 (14.5-23.0)
20-day	4.46 (3.89-5.16)	5.81 (5.06-6.72)	7.94 (6.90-9.17)	9.56 (8.28-11.0)	11.7 (10.1-13.6)	13.4 (11.4-15.6)	15.1 (12.7-17.8)	17.0 (14.2-20.3)	19.7 (16.1-23.9)	21.9 (17.5-26.9)
30-day	5.34 (4.66-6.18)	6.96 (6.07-8.05)	9.49 (8.26-11.0)	11.4 (9.90-13.1)	13.9 (12.0-16.1)	15.9 (13.6-18.4)	17.8 (15.1-20.9)	19.9 (16.6-23.5)	22.9 (18.9-27.5)	25.3 (20.6-30.8)
45-day	6.51 (5.68-7.40)	8.49 (7.41-9.65)	11.5 (10.0-13.1)	13.7 (11.9-15.6)	16.6 (14.3-18.9)	18.7 (16.1-21.4)	20.8 (17.8-24.0)	23.0 (19.4-26.7)	26.3 (21.9-30.9)	28.8 (23.7-34.3)
60-day	7.50 (6.52-8.55)	9.84 (8.55-11.2)	13.3 (11.6-15.2)	15.8 (13.7-17.9)	18.8 (16.3-21.5)	21.1 (18.1-24.1)	23.2 (19.8-26.7)	25.3 (21.4-29.4)	28.5 (23.7-33.3)	30.8 (25.4-36.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.



**CURVE NUMBER CALCULATION WORKSHEET**

**PROJECT:** Vil Pkwy **CALCULATED BY:** DEW  
**SUBBASIN:** L1  
**TOTAL AREA:** 18.6 ACRES

HSG	AREA, ACRES	FRACTION OF AREA	LAND USE & CONDITION	CN	WTD. CN	REMARKS
D	18.6	1.000	Shrub/brush fair	77	77.0	
	0	0.000	Sage/grass, fair	70	0.0	
		0.000			0.0	
		0.000			0.0	
	18.6	1.000				
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

**PROJECT:** Vil Pkwy **CALCULATED BY:** DEW  
**SUBBASIN:** P  
**TOTAL AREA:** 19.84 ACRES

HSG	AREA, ACRES	FRACTION OF AREA	LAND USE & CONDITION	CN	WTD. CN	REMARKS
D	19.84	1.000	Shrub/brush, fair	77	77.0	
	0	0.000	Sage/grass, fair	70	0.0	
		0.000			0.0	
	19.84	1.000				
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

**PROJECT:** Vil Pkwy **CALCULATED BY:** DEW  
**SUBBASIN:** Q Existing Conditions  
**TOTAL AREA:** 33.3 ACRES

HSG	AREA, ACRES	FRACTION OF AREA	LAND USE & CONDITION	CN	WTD. CN	REMARKS
D	33.3	1.000	Sage/grass, fair	77	77.0	
		0.000			0.0	
		0.000			0.0	
		0.000			0.0	
		0.000			0.0	
		0.000			0.0	
		0.000			0.0	
	33.3	1.000				
<b>FINAL CN VALUE:</b>					<b>77.0</b>	



**CURVE NUMBER CALCULATION WORKSHEET**

PROJECT: Vill Pkway

SUBBASIN: Q2

AREA, AC.: 8.32

CALCULATED BY: DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	.25 AC LOTS	8.32	1.000	77	77.0	
C		0.00	0.000	63	0.0	
D		0.00	0.000	84	0.0	
C		0.00	0.000	98	0.0	
		8.32	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)

**CURVE NUMBER CALCULATION WORKSHEET**

PROJECT: Vill Pkway

SUBBASIN: L3

AREA, AC.: 7.44

CALCULATED BY: DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	Shrub/brush fair	7.44	0.894	77	68.9	
C		0.00	0.000	63	0.0	
D		0.00	0.000	84	0.0	
C		0.00	0.000	98	0.0	
		7.44	0.894			
<b>FINAL CN VALUE:</b>					<b>68.9</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)

**CURVE NUMBER CALCULATION WORKSHEET**

**PROJECT:** Village Parkway Homes

**SUBBASIN:** VPH-1

**AREA, AC.:** 22.63

**CALCULATED BY:** DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	3,600 sq ft lots	22.63	1.000	77	77.0	
A		0.00	0.000	0	0.0	
C		0.00	0.000	0	0.0	
		22.63	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)

**PROJECT:** Village Parkway Homes

**SUBBASIN:** VPH-2

**AREA, AC.:** 6.32

**CALCULATED BY:** DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	3,600 sq ft lots	6.32	1.000	77	77.0	
A		0.00	0.000	0	0.0	
C		0.00	0.000	0	0.0	
		6.32	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)



**CURVE NUMBER CALCULATION WORKSHEET**

**PROJECT:** Vill Pkway  
**SUBBASIN:** VPH-3  
**AREA, AC.:** 6.56  
**CALCULATED BY:** DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	3,600 sq ft lots	6.56	1.000	77	77.0	
C		0.00	0.000	63	0.0	
D		0.00	0.000	84	0.0	
C		0.00	0.000	98	0.0	
		6.56	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)

**CURVE NUMBER CALCULATION WORKSHEET**

**PROJECT:** Vill Pkway  
**SUBBASIN:** VPH-4  
**AREA, AC.:** 7.44  
**CALCULATED BY:** DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	3,600 sq ft lots	7.44	1.000	77	77.0	
C		0.00	0.000	63	0.0	
D		0.00	0.000	84	0.0	
C		0.00	0.000	98	0.0	
		7.44	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)

**CURVE NUMBER CALCULATION WORKSHEET**

**PROJECT:** Vill Pkway  
**SUBBASIN:** VPH-5  
**AREA, AC.:** 3.38  
**CALCULATED BY:** DEW

HSG	LAND USE & CONDITION	AREA, ACRES	FRACTION OF AREA	CN*	WTD. CN	REMARKS
A	3,600 sq ft lots	3.38	1.000	77	77.0	
C		0.00	0.000	63	0.0	
D		0.00	0.000	84	0.0	
C		0.00	0.000	98	0.0	
		3.38	1.000			
<b>FINAL CN VALUE:</b>					<b>77.0</b>	

\*Curve number values based on Truckee Meadows Regional Drainage Manual (2009)



## TIME OF CONCENTRATION CALCULATIONS

**PROJECT:** VILLAGE PARKWAY HOMES  
SUB-BASIN DATA

Developed Watersheds

NAME	CN	R	INITIAL/OVERLAND TIME			TRAVEL TIME, $t_t$			URANIZED BASINS		FINAL		
			L, FT	S, %	$t_t$	L, ft	S, %	Vel, ft/sec	tt, min	$t_t$	$t_t$	$t_c$	
VPH-1	77	0.6264	100	1	8.52	1606	0.5	1.4	19.12	27.64	1706	19.48	19
VPH-2	77	0.6264	100	1	8.52	946	0.5	1.4	11.26	19.79	1046	15.81	16
VPH-3	77	0.6264	100	1	8.52	710	0.5	1.4	8.45	16.98	810	14.50	15
VPH-4	77	0.6264	100	1	8.52	821	0.5	1.4	9.77	18.30	921	15.12	15
VPH-5	77	0.6264	100	1	8.52	440	0.5	1.4	5.24	13.76	540	13.00	13
Q2	77	0.6264	100	1	8.52	1050	0.5	1.4	12.50	21.02	1150	16.39	16

**LAG TIMES FOR WATERSHEDS OVER 1 SQUARE MILE I OR WITH SLOPES GREATER THAN 10%**

PROJECT:	Village Parkway		Length to Centroid (L <sub>c</sub> ), miles	Upper Elev., ft	Lower Elev., ft	Elevation Change, ft	Average Slope (S), ft/mi	Roughness (Kn)	Lag Time (TLAG)hours
	Watershed*	Watercourse Length (L), miles							
	L1	0.35	0.17	5,600.0	5,100.0	500.0	1,428.57	0.08	0.21
	P	0.16	0.05	5,470.0	5,100.0	370.0	2,312.50	0.08	0.10
	Q	0.27	0.13	5,360.0	5,120.0	240.0	888.89	0.08	0.19
	L3	0.29	0.15	5350	5090	260.0	896.55	0.08	0.20

$$TLAG = 22.1(K_n)(L^*(L_c/S^5))^{.33}$$

Equation 710 in Truckee Meadows Regional Drainage Manual

**APPENDIX C**  
**HEC-1 MODELS**



**EXISTING CONDITIONS THROUGH WOODLAND VILLAGE PHASE 20**

VPH Existing Cond  
Woodland Village Ph.20

```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998 AND FEB 2010
* VERSION 4.1R
* RGMHEC2000 WWW.HEC-1.COM
* RUN DATE 07MAR21 TIME 18:38:31
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DDIAGRAM
1 ID 100 yr 24 hr event
2 ID VILLAGE PARKWAY HOMES
3 ID FILE NAME WV20-1RB.DA T THROUGH WV-20 ONLY
4 ID USING TYPE II STORM DISTRIBUTION
* DARF AREA (SQ. MI.)
* 1.00 0 - 2
* 0.99 2.1 - 8
* 0.98 8.1 - 16
* 0.97 16.1 - 29
* 0.96 29.1 - 43
* 0.95 43.1 - 63
* 0.94 63.1 - 98
5 IT 10 800
6 IO 5 0
7 JR PREC 1.0 .99 .98 .97 .96 .95
8 KK A
9 BA 0.72
10 PH 1 .68 1.24 2.06 2.32 2.52 2.94 3.76 4.59
11 LS 1.7 54
12 UD .62
13 KK B
14 BA 1.78
15 LS 1.63 55
16 UD 1.1
17 KK D@A&B
18 HC 2
19 KK D-A&B
20 DT D-AB
21 DI 0 10 50 100 500
22 DQ 0 5 25 50 250
23 KK RCH-1
24 KM ROUTE A&B TO J1@AB
25 RD 10200 .04 .12 TRAP 3 1
26 KK C
27 BA 1.26
28 LS 1.7 54
29 UD .82
30 KK J1@A&B
31 HC 2
32 KK RCH-2
33 RD 3500 .06 .12 TRAP 10 2.5
HEC-1 INPUT

```

1

PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
34 KK D

```

35	BA	1.0				
36	LS	1.57	50			
37	UD	.63				
38	KK	J2ABCD				
39	HC	2				
40	KK	DJ2				
41	KM	CHANGE DIVERSION FROM 50% TO 75%				
42	DT	J2				
43	DI	0	10	50	100	500
44	DQ	0	7.5	37.5	75	375
45	KK	E				
46	BA	.615				
47	LS	1.45	58			
48	UD	.68				
49	KK	D@E				
50	DT	DE				
51	DI	0	10	50	100	500
52	DQ	0	10	50	100	500
53	KK	F				
54	BA	0.815				
55	LS	1.51	57			
56	UD	1				
57	KK	D@F				
58	DT	DF				
59	DI	0	10	50	100	500
60	DQ	0	10	50	100	500
61	KK	J3-1				
62	HC	2				
63	KK	J				
64	BA	1.14				
65	LU	4	0.1			
66	UD	.67				
67	KK	J3-2				
68	HC	2				
69	KK	G				
70	BA	0.81				
71	LS	1.03	66			
72	UD	.93				

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

73	KK	D@G				
74	DT	DDG				
75	DI	0	10	50	100	500
76	DQ	0	10	50	100	500
77	KK	H				
78	BA	0.74				
79	LS	1.12	64			
80	UD	.63				
81	KK	D@H				
82	DT	DDH				
83	DI	0	10	50	100	500
84	DQ	0	10	50	100	500
85	KK	J3				
86	HC	4				
87	KK	RCH-3				
88	RD	8000	.04	.05	TRAP	10 1
89	KK	D@J3				
90	DT	D-J3				
91	DI	0	10	50	100	500
92	DQ	0	5	25	50	250
93	KK	IEAST				
94	BA	.18				
95	LS		64			
96	UD	.22				
97	KK	D@IE				
98	DT	DDG				
99	DI	0	10	50	100	500
100	DQ	0	8	40	80	400
101	KK	OEAST				
102	BA	.21				
103	LU	4	.1			
104	KK	CP2				



105 HC 2  
 106 KK CPO+J3  
 107 HC 2  
 108 KK D@NOA  
 109 DT DNA  
 110 DI 0 40 60 100 500 1000  
 111 DQ 0 0 40 40 40 40  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

112 KK RS-NOA NORTH RESERVOIR A  
 113 KM 36" OUTLET  
 114 RS 1 STOR 0  
 115 SA 0 .17 .91 2.24 3.55 4.94  
 116 SE 5101.5 5102 5103 5104 5105 5106  
 117 SQ 0 6 19 35 50 60  
 118 SE 5101.5 5102.5 5103.5 5104.5 5105.5 5106.5  
 119 KK I-KWATERSHED CONSISTING OF K+ EM-3+EM-5 APPROX.  
 120 BA .3741  
 121 LS 65  
 122 UD 0.61  
 123 KK DVI-K DIVERT FLOW FROM I-K SAME RATE AS FROM K  
 124 DT D- IK  
 125 DI 0 10 100 500  
 126 DQ 0 5 50 250  
 127 KK WV20-B PART OF WV-20 GOING NORTH  
 128 BA .017  
 129 LS 74  
 130 UD .16  
 131 KK CPEM5  
 132 HC 2  
 133 KK D@NOB  
 134 DT DNB  
 135 DI 0 40 60 100 500 1000  
 136 DQ 0 0 40 40 40 40

137 KK RS-NOB NORTH RESERVOIR B  
 138 KM 12" OUTLET  
 139 RS 1 STOR 0  
 140 SA 0 0.02 0.16 0.52 1.73 3.30 5.24 5.38 5.52  
 141 SE 5102.5 5103 5104 5104 5106 5107 5108 5109 5110  
 142 SQ 0 2.2 4.5 5.6 7 8 9 10 11  
 143 SE 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5 5109.5  
 144 KK NORTH  
 145 HC 2  
 146 KK M  
 147 BA 0.56  
 148 LS 1.17 63  
 149 UD 0.52  
 150 KK RES-M  
 151 RS 1 STOR 0  
 152 SA 2.5 2.56 2.66 2.79 1.95 3.15 3.4 3.72 4.12  
 153 SE 0 1.38 2.06 2.68 3.29 3.99 4.87 5.91 7.1  
 154 SQ 0 6 19 35 50 60 72 78 90  
 155 SE 0 1 2 3 4 5 6 7 8  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

156 KK OFF-4 OFFSITE 4  
 157 BA .06  
 158 LS 63  
 159 UD .42  
 160 KK M+OFF4 COMBINE OFF4 + POND M  
 161 HC 2  
 162 KK D@M  
 163 DT DDM  
 164 DI 0 10 50 100 500 1000  
 165 DQ 0 2 10 20 100 200  
 166 KK OFF-3  
 167 BA 0.191  
 168 LS 65  
 169 UD 0.52  
 170 KK OF3+4 COMBINE OFF3 & 0 FF4 & POND M  
 171 HC 2  
 172 KK EM-1

173 BA .046  
 174 LS 88  
 175 UD 0.25

176 KK JEM1+ COMBINE EM1, POND M, OFF3 & OFF4  
 177 KM SAME AS JM EM1 OFF3 OFF4 IN HEC-HMS  
 178 HC 2

179 KK TRI TRIANGULAR AREA EAST OF VILLAGE PKWY  
 180 BA .009  
 181 LS 64.5  
 182 UD 0.16

183 KK CPPP1 ADD TRIANGULAR AREA TO FLOW INTO PP-1  
 184 HC 2

185 KK PP-1  
 186 KM NOW WITH 30" OUTLET  
 187 RS 1 STOR 0  
 188 SA 0 .11 .34 .73 1.19 1.82 1.96 2.10 2.24  
 189 SA 2.52  
 190 SE 14.34 15 16 17 18 19 20 21 22  
 191 SE 24  
 192 SQ 0 5.5 16 28 38 45 50 57 62  
 193 SQ 70 75  
 194 SE 14.34 15.34 16.34 17.34 18.34 19.34 20.34 21.34 22.34  
 195 SE 24.34

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

196 KK RCHPP1  
 197 RD 2475 .007 .04 TRAP 3 3

198 KK D@NOC  
 199 DT DNC  
 200 DI 0 40 60 100 500 1000  
 201 DQ 0 0 40 40 40 40

202 KK RS-NOC NORTH RESERVOIR C  
 203 KM 30" OUTLET  
 204 RS 1 STOR 0  
 205 SA 0 .22 .82 2.4 3.85 4.54 5.03 5.31  
 206 SE 5094 5095 5096 5097 5098 5099 5100 5101  
 207 SQ 0 5.5 16 28 38 45 50 57  
 208 SE 5094 5095 5096 5097 5098 5099 5100 5101

209 KK CP-NOR COMBINE 3 NORTH DET BASINS  
 210 HC 2

211 KK IWEST  
 212 BA .35  
 213 LS 64  
 214 UD .37

215 KK D@IW  
 216 DT DDIW  
 217 DI 0 10 50 100 500  
 218 DQ 0 8 40 80 400

219 KK OWEST  
 220 BA .18  
 221 LU 4 .1

222 KK CP1  
 223 HC 2

224 KK NOR+I COMBINE FLOW FROM 3 DET BASINS & OFFSITE WATERSHED I  
 225 HC 2

226 KK EM4  
 227 BA .1193  
 228 LS 84  
 229 UD .25

230 KK EMB-1  
 231 RS 1 STOR 0  
 232 SA 1.5 1.54 1.6 1.68 1.79 1.95 2.15  
 233 SE 5078 5079.1 5079.69 5080.25 5080.95 5081.86 5082.96  
 234 SQ 0 8 26 40 52 60  
 235 SE 5078 5079 5080 5081 5082 5083

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

236 KK RHEMB1 REACH EMB-1  
 237 RD 759 .0066 .04 TRAP 3 3

238 KK EM-6  
 239 BA .0455  
 240 LS 1.5 84  
 241 UD .32

242	KK	EM-7								
243	BA	.061								
244	LS	.5	83							
245	UD	.3								
246	KK	CP-PP2								
247	HC	3								
248	KK	PP-2								
249	KM	OUTLET IS ONE 30" RCP								
250	RS	1	STOR	0						
251	SA	0	.02	.16	.52	1.73	3.30	5.24	5.38	5.52
252	SE	5171	5171.5	5172.5	5173.5	5174.5	5175.5	5176.5	5177.5	5178.5
253	SQ	0	5.7	13.5	18.6	22	25	29	31	32
254	SE	5171	5172	5173	5174	5175	5176	5177	5178	5178.5
255	KK	JCHAN2								
256	HC	2								
257	KK	CHAN-2								
258	RD	1130	.005	.04		TRAP	6	3		
259	KK	L2								
260	BA	.252								
261	LS	1.03	66							
262	UD	.33								
263	KK	D@L								
264	DT	D-L								
265	DI	0	10	50	100	500				
266	DQ	0	5	25	50	250				
267	KK	RES-L								
268	RS	1	STOR	0						
269	SA	0.6	0.64	0.69	0.76	0.86	1			
270	SE	0	1.69	2.25	2.95	3.86	4.96			
271	SQ	0	5.5	16	28	38	45			
272	SE	0	1	2	3	4	5			
273	KK	L1								
274	BA	.038								
275	LS	1.03	66							
276	UD	.28								

HEC-1 INPUT

PAGE 8

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

277	KK	JCHAN4								
278	HC	3								
279	KK	RECH4A								
280	RD	395	.001	.04		TRAP	8	3		
281	KK	RCH4B								
282	RD	665	.001	.04		TRAP	10	3		
283	KK	WV-20A								
284	BA	.013								
285	LS		61							
286	UD	.15								
287	KK	HASKEL								
288	RS	1	STOR	0						
289	SA	0	.47	.55	.60	.65				
290	SE	5194.5	5195	5196	5197	5198				
291	SQ	0	2.4	4.7	6	7.5				
292	SE	5194.5	5195.5	5196.5	5197.5	5198.5				
293	KK	EM-2								
294	BA	.0621								
295	LS		78							
296	UD	.32								
297	KK	20A+2								
298	KM	FLOW GOES INTO POND EMG-1								
299	HC	2								
300	KK	EMG-1								
301	RS	1	STOR	0						
302	SA	0.8	0.83	.87	.93	1.02	1.13	1.29		
303	SE	86	87.1	87.69	88.25	88.95	89.86	90.96		
304	SQ	0	8	26	40	52	60			
305	SE	86	87	88	89	90	91			
306	KK	EMG-1								
307	RD	1630	.01	.04		TRAP	3	3		
308	KK	EMTC								
309	BA	.053								
310	LS	1.5	79							
311	UD	.27								



312 KK EM-10  
 313 BA .053  
 314 LS 1.5 72  
 315 UD .32

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

316 KK JEMO2  
 317 HC 3

318 KK EMO-2  
 319 RS 1 STOR 0  
 320 SA 1.2 1.25 1.26 1.27 1.29 1.3 1.32 1.34 1.39  
 321 SE 67 68.49 68.91 69.31 69.72 70.21 70.69 71.31 72.8  
 322 SQ 0 11 32 56 76 90 100  
 323 SE 67 68 69 70 71 72 73

324 KK EMOc  
 325 RD 615 .003 .04 TRAP 0 3

326 KK EM-11  
 327 BA .012  
 328 LS 1.5 86  
 329 UD .13

330 KK EM-9  
 331 BA .021  
 332 LS 1.5 86  
 333 UD .13

334 KK JG2&B2  
 335 HC 3

336 KK EM-8  
 337 BA .046  
 338 LS 1.5 82  
 339 UD .22

340 KK EM-12  
 341 BA .015  
 342 LS 1.5 93  
 343 UD .12

344 KK TODET  
 345 HC 3

346 KK DETN  
 347 RS 1 STOR 0  
 348 SA 2.25 2.31 2.4 2.5 2.63 2.78 2.96 3.18 3.48  
 349 SE 0 1.49 1.91 2.31 2.72 3.21 3.69 4.31 5.8  
 350 SQ 0 5.5 16 28 38 45 50  
 351 SE 0 1 2 3 4 5 6

352 KK J4B  
 353 HC 2

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

354 KK RCH-4C  
 355 RD 300 .001 .04 TRAP 12 3

356 KK A3  
 357 BA .055  
 358 LS 80  
 359 UD .16

360 KK A3A  
 361 BA .007  
 362 LS 76  
 363 UD .13

364 KK COMBA3  
 365 HC 2

366 KK RES-6  
 367 RS 1 STOR 0  
 368 SA 0.24 0.5 0.54 0.61 0.67 0.69  
 369 SE 5074 5075 5076 5077 5078 5079  
 370 SQ 0 4.3 14 24 30 35

371 KK A3B  
 372 BA .026  
 373 LS 77  
 374 UD .17

375 KK D-PARK  
 376 DT PARK  
 377 DI 0 20 100 500 1000  
 378 DQ 0 5 25 125 250



447	KK	J-1							
448	HC	3							
449	KK	EXDET							
450	RS	1	STOR	0					
451	SA	0.27	0.28	0.37	0.47	0.52	0.52	0.52	
452	SE	5118	5119	5121	5125	5125.25	5125.5	5126	
453	SQ	0	0	9.8	23	99.5	238	631.1	
454	KK	DIV							
455	DT	D-DIV							
456	DI	0	10	100	1000				
457	DQ	0	5	50	500				
458	KK	REXDET							
459	RD	1787	.025	.013		TRAP	40	1	
460	KK	OFF-2							
461	BA	.0496							
462	LS		63						
463	UD	.27							
464	KK	R-19							
465	RD	1400	.02	.05		TRAP	15	1	
466	KK	CSR-6A							
467	BA	.005							
468	LS		73						
469	UD	.17							
470	KK	EXDT1A							
471	RS	1	STOR	0					
472	SA	0	.0046	.0169	.0553	.0703			
473	SE	5103	5104	5105	5109	5110			
474	SQ	0	1.65	4.75	8.43	9.15			

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

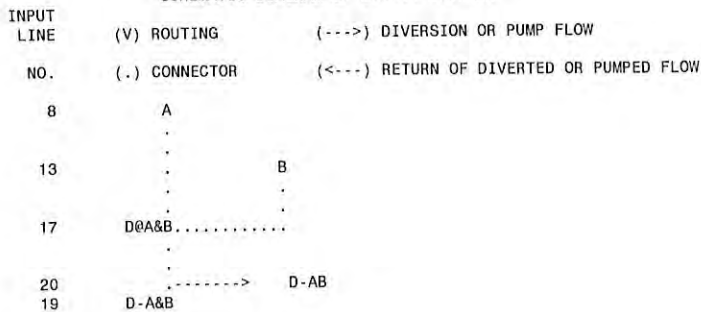
475	KK	J-6							
476	HC	2							
477	KK	CSR-6							
478	BA	.025							
479	LS		78						
480	UD	.18							
481	KK	CPXDT1							
482	HC	2							
483	KK	EXDT1							
484	RS	1	STOR	0					
485	SA	0.25	0.31	0.37	0.49				
486	SE	5101	5103	5105	5108				
487	SQ	0	9.5	17	22				
488	KK	A1							
489	BA	.09							
490	LS		78						
491	UD	.2							
492	KK	J8							
493	HC	2							
494	KK	R21							
495	RM	1	.107	.02					
496	KK	JRES2							
497	HC	2							
498	KK	RES2							
499	RS	1	STOR	0					
500	SA	0	.18	1.4	2.9	3.1	3.3	3.5	3.6
501	SA	3.9							
502	SE	5065.5	5066	5067	5068	5069	5070	5071	5071.34
503	SE	5072.34							
504	SQ	0	.9	5.5	9.1	11.6	13.6	15.4	16
505	SQ	77.5							
506	KK	R22							
507	RD	800	.02	.05		TRAP	15	1	
508	KK	CSR-4							
509	BA	.03							
510	LS		75						
511	UD	.13							
512	KK	EXDET2							
513	RS	1	STOR	0					
514	SA	0.13	0.16	0.19	0.22	0.26	0.3	0.34	0.39
515	SE	5091	5092	5093	5094	5095	5096	5097	5098
516	SQ	0	2.4	5	6.5	8	9.5	10	11



LINE	ID	1	2	3	4	5	6	7	8	9	10
517	KK	CSR-3									
518	BA	.0053									
519	LS		80								
520	UD	.12									
521	KK	J11									
522	HC	2									
523	KK	DITCH									
524	RD	3000	.01	.04		TRAP	6	1.5			
525	KK	A2									
526	BA	.05									
527	LS		76								
528	UD	.15									
529	KK	JRES15									
530	HC	3									
531	KK	RES15									
532	RS	1	STOR	0							
533	SA	3.55	3.71	3.85	4.04	4.36	4.69	4.94			
534	SE	5058.5	5059	5059.5	5060	5061	5062	5064			
535	SQ	0	0	0	.6	4.7	8.3	12.2			
536	KK	R23									
537	RD	2600	.02	.05		TRAP	5	1			
538	KK	RPE									
539	BA	0.12									
540	LS		72								
541	UD	.28									
542	KK	ACS-1									
543	HC	3									
544	KK	P									
545	BA	.069									
546	LS		71								
547	UD	.13									
548	KK	DIV-P									
549	DT	D-P									
550	DI	0	10	100	1000						
551	DQ	0	5	50	500						
552	KK	Q									
553	BA	.039									
554	LS		68								
555	UD	.27									

LINE	ID	1	2	3	4	5	6	7	8	9	10
556	KK	PVE-1									
557	BA	.0128									
558	LS		76								
559	UD	.13									
560	KK	ABCDSP									
561	HC	4									
562	KK	PVE-2									
563	BA	.011									
564	LS		76								
565	UD	.13									
566	KK	BLCSRD									
567	HC	2									
568	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK



```

      V
      V
23  RCH-1
      .
      .
26      .           C
      .           .
      .           .
30  J1@A&B .....
      V
      V
32  RCH-2
      .
      .
34      .           D
      .           .
      .           .
38  J2ABCD .....
      .
42  ----->      J2
40  DJ2
      .
      .
45      .           E
      .           .
      .           .
50      .           DE
49  D@E ----->
      .
      .
53      .           F
      .           .
      .           .
58      .           DF
57  D@F ----->
      .
      .
61  J3-1 .....
      .
      .
63      .           J
      .           .
      .           .
67  J3-2 .....
      .
      .
69      .           G
      .           .
      .           .
74      .           DDG
73  D@G ----->
      .
      .
77      .           H
      .           .
      .           .
82      .           DDH
81  D@H ----->
      .
      .
85  J3 .....
      V
      V
87  RCH-3
      .
      .
90  ----->      D-J3
89  D@J3
      .
      .
93      .           IEAST
      .           .
      .           .
98      .           DDG
97  D@IE ----->
      .
      .
101      .           OEAST
      .           .
      .           .
104      .           CP2 .....
      .
      .
106  CPO+J3 .....
      .
      .
109  ----->      DNA
108  D@NOA
      V
      V
112  RS-NOA
      .
      .

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```

119 . . . . . I-K
. . . . . |
124 . . . . . |-----> D-IK
123 . . . . . DVI-K
. . . . . |
127 . . . . . |         WV20-B
. . . . . |
131 . . . . . CPEM5
. . . . . |
134 . . . . . |-----> DNB
133 . . . . . D@NOB
. . . . . |
. . . . . | V
137 . . . . . | V
. . . . . | RS-NOB
. . . . . |
144 NORTH.....
. . . . . |
146 . . . . . |         M
. . . . . |         V
. . . . . |         V
150 . . . . . RES-M
. . . . . |
156 . . . . . |         OFF-4
. . . . . |
160 . . . . . M+OFF4
. . . . . |
163 . . . . . |-----> DDM
162 . . . . . D@M
. . . . . |
166 . . . . . |         OFF-3
. . . . . |
170 . . . . . OF3+4
. . . . . |
172 . . . . . |         EM-1
. . . . . |
176 . . . . . JEM1+
. . . . . |
179 . . . . . |         TRI
. . . . . |
183 . . . . . CPPP1
. . . . . |
. . . . . | V
185 . . . . . | V
. . . . . | PP-1
. . . . . | V
196 . . . . . RCHPP1
. . . . . |
199 . . . . . |-----> DNC
198 . . . . . D@NOC
. . . . . |
. . . . . | V
202 . . . . . RS-NOC
. . . . . |
209 CP-NOR.....
. . . . . |
211 . . . . . IWEST
. . . . . |
216 . . . . . |-----> DDIW
215 . . . . . D@IW
. . . . . |
219 . . . . . |         OWEST
. . . . . |
222 . . . . . CP1
. . . . . |
224 NOR+I.....
. . . . . |
226 . . . . . |         EM4
. . . . . |         V
. . . . . |         V
230 . . . . . |         EMB-1
. . . . . |         V

```



236	.	V		
	.	RHEMB1		
238	.	.	EM-6	
242	.	.	.	EM-7
246	.	CP-PP2	.....	
	.	V		
	.	V		
248	.	PP-2		
255	JCHAN2	.....		
	.	V		
	.	V		
257	CHAN-2			
259	.	L2		
264	.	----->	D-L	
263	.	D@L		
	.	V		
	.	V		
267	.	RES-L		
273	.	.	L1	
277	JCHAN4	.....		
	.	V		
	.	V		
279	RECH4A			
	.	V		
	.	V		
281	RCH4B			
283	.	WV-20A		
	.	V		
	.	V		
287	.	HASKEL		
293	.	.	EM-2	
297	.	20A+2	.....	
	.	V		
	.	V		
300	.	EMG-1		
	.	V		
	.	V		
306	.	EMG-1		
308	.	.	EMTC	
312	.	.	.	EM-10
316	.	JEMO2	.....	
	.	V		
	.	V		
318	.	EMO-2		
	.	V		
	.	V		
324	.	EMOc		
326	.	.	EM-11	
330	.	.	.	EM-9
334	.	JG2&B2	.....	
336	.	.	EM-8	
340	.	.	.	EM-12
344	.	TODETN	.....	
	.	V		

```

346 . . . V
      . . . DETN
      . . .
352 J4B .....
      V
      V
354 RCH-4C
      .
356 . . . A3
      .
360 . . . A3A
      .
364 . . . COMBA3 .....
      V
      V
366 . . . RES-6
      .
371 . . . A3B
      .
376 . . . D-PARK -----> PARK
375 . . . V
      . . . V
379 . . . RES-5
      . . . V
384 . . . R-9
      .
386 . . . A13A
      .
390 . . . A13B
      .
394 . . . COMA13 .....
      .
396 . . . A12A
      .
400 . . . A12
      .
404 . . . COMA12 .....
      .
406 . . . JRES3 .....
      . . . V
408 . . . RES-3
      .
413 . . . A13
      .
417 . . . A12B
      .
421 . . . JRES1 .....
      . . . V
423 . . . RES-1
      .
431 ABMSR .....
      .
433 . . . OFF-1
      . . . V
437 . . . R8
      .
439 . . . A5
      .
443 . . . CSR-7
      .
447 . . . J-1 .....
      . . . V
449 . . . EXDET
      .
455 . . . D-DIV
454 . . . DIV ----->

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      V
      V
458  . . . . . REXDET
      .
      .
460  . . . . . OFF-2
      . . . . . V
      . . . . . V
464  . . . . . R-19
      . . . . .
      . . . . .
466  . . . . . CSR-6A
      . . . . . V
      . . . . . V
470  . . . . . EXDT1A
      . . . . .
      . . . . .
475  . . . . . J-6.....
      . . . . .
      . . . . .
477  . . . . . CSR-6
      . . . . .
      . . . . .
481  . . . . . CPXDT1.....
      . . . . . V
      . . . . . V
483  . . . . . EXDT1
      . . . . .
      . . . . .
488  . . . . . A1
      . . . . .
      . . . . .
492  . . . . . J8.....
      . . . . . V
      . . . . . V
494  . . . . . R21
      . . . . .
      . . . . .
496  . . . . . JRES2.....
      . . . . . V
      . . . . . V
498  . . . . . RES2
      . . . . . V
      . . . . . V
506  . . . . . R22
      . . . . .
      . . . . .
508  . . . . . CSR-4
      . . . . . V
      . . . . . V
512  . . . . . EXDET2
      . . . . .
      . . . . .
517  . . . . . CSR-3
      . . . . .
      . . . . .
521  . . . . . J11.....
      . . . . . V
      . . . . . V
523  . . . . . DITCH
      . . . . .
      . . . . .
525  . . . . . A2
      . . . . .
      . . . . .
529  . . . . . JRES15.....
      . . . . . V
      . . . . . V
531  . . . . . RES15
      . . . . . V
      . . . . . V
536  . . . . . R23
      . . . . .
      . . . . .
538  . . . . . RPE
      . . . . .
      . . . . .
542  . . . . . ACS-1.....
      . . . . .
      . . . . .
544  . . . . . P
      . . . . .
      . . . . .
549  . . . . . -----> D-P
548  . . . . . DIV-P
      . . . . .
      . . . . .
552  . . . . . Q
      . . . . .
      . . . . .
556  . . . . . PVE-1
      . . . . .
      . . . . .
560  . . . . . ABCDSP.....

```





HYDROGRAPH AT +	C	1.260	1	FLOW TIME	173.70 13.00	167.28 13.00	160.97 13.00	154.75 13.00	148.63 13.00	142.70 13.17
2 COMBINED AT +	J1@A&B	3.760	1	FLOW TIME	292.49 13.33	277.67 13.33	264.27 13.50	253.43 13.50	243.81 13.50	234.54 13.50
ROUTED TO +	RCH-2	3.760	1	FLOW TIME	289.48 13.50	275.52 13.50	261.29 13.67	250.68 13.67	240.82 13.67	232.01 13.67
HYDROGRAPH AT +	D	1.000	1	FLOW TIME	166.69 12.83	160.98 12.83	155.35 12.83	149.80 12.83	144.33 12.83	138.95 12.83
2 COMBINED AT +	J2ABCD	4.760	1	FLOW TIME	375.21 13.50	358.74 13.50	340.56 13.50	321.28 13.50	307.53 13.50	293.48 13.67
DIVERSION TO +	J2	4.760	1	FLOW TIME	281.41 13.50	269.06 13.50	255.42 13.50	240.96 13.50	230.64 13.50	220.11 13.67
HYDROGRAPH AT +	DJ2	4.760	1	FLOW TIME	93.80 13.50	89.69 13.50	85.14 13.50	80.32 13.50	76.88 13.50	73.37 13.67
HYDROGRAPH AT +	E	.615	1	FLOW TIME	142.56 12.83	138.11 12.83	133.71 12.83	129.35 12.83	125.05 12.83	120.80 12.83
DIVERSION TO +	DE	.615	1	FLOW TIME	142.56 12.83	138.11 12.83	133.71 12.83	129.35 12.83	125.05 12.83	120.80 12.83
HYDROGRAPH AT +	D@E	.615	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
HYDROGRAPH AT +	F	.815	1	FLOW TIME	130.32 13.17	126.11 13.17	121.96 13.17	117.95 13.33	114.02 13.33	110.14 13.33
DIVERSION TO +	DF	.815	1	FLOW TIME	130.32 13.17	126.11 13.17	121.96 13.17	117.95 13.33	114.02 13.33	110.14 13.33
HYDROGRAPH AT +	D@F	.815	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
2 COMBINED AT +	J3-1	1.430	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
HYDROGRAPH AT +	J	1.140	1	FLOW TIME	13.79 17.83	10.25 18.17	6.53 18.33	2.83 18.50	.00 .00	.00 .00
2 COMBINED AT +	J3-2	2.570	1	FLOW TIME	13.79 17.83	10.25 18.17	6.53 18.33	2.83 18.50	.00 .00	.00 .00
HYDROGRAPH AT +	G	.810	1	FLOW TIME	263.54 13.17	257.51 13.17	251.51 13.17	245.56 13.17	239.63 13.17	233.74 13.17
DIVERSION TO +	DDG	.810	1	FLOW TIME	263.54 13.17	257.51 13.17	251.51 13.17	245.56 13.17	239.63 13.17	233.74 13.17
HYDROGRAPH AT +	D@G	.810	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
HYDROGRAPH AT +	H	.740	1	FLOW TIME	282.19 12.83	275.35 12.83	268.54 12.83	261.78 12.83	255.07 12.83	248.40 12.83
DIVERSION TO +	DDH	.740	1	FLOW TIME	282.19 12.83	275.35 12.83	268.54 12.83	261.78 12.83	255.07 12.83	248.40 12.83
HYDROGRAPH AT +	D@H	.740	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
4 COMBINED AT +	J3	8.880	1	FLOW TIME	93.80 13.50	89.69 13.50	85.14 13.50	80.32 13.50	76.88 13.50	73.37 13.67
ROUTED TO +	RCH-3	8.880	1	FLOW	93.81	88.64	84.28	79.68	76.05	73.02

				TIME	13.67	13.67	13.67	13.83	13.83	13.83
DIVERSION TO										
+	D-J3	8.880	1	FLOW TIME	46.91 13.67	44.32 13.67	42.14 13.67	39.84 13.83	38.02 13.83	36.51 13.83
HYDROGRAPH AT										
+	D@J3	8.880	1	FLOW TIME	46.91 13.67	44.32 13.67	42.14 13.67	39.84 13.83	38.02 13.83	36.51 13.83
HYDROGRAPH AT										
+	IEAST	.180	1	FLOW TIME	126.16 12.33	123.09 12.33	120.03 12.33	117.00 12.33	113.98 12.33	110.98 12.33
DIVERSION TO										
+	DDG	.180	1	FLOW TIME	100.93 12.33	98.47 12.33	96.03 12.33	93.60 12.33	91.18 12.33	88.78 12.33
HYDROGRAPH AT										
+	D@IE	.180	1	FLOW TIME	25.23 12.33	24.62 12.33	24.01 12.33	23.40 12.33	22.80 12.33	22.20 12.33
HYDROGRAPH AT										
+	OEAST	.210	1	FLOW TIME	2.86 17.17	2.21 17.50	1.59 17.83	.98 18.00	.11 18.17	.00 18.17
2 COMBINED AT										
+	CP2	.390	1	FLOW TIME	25.23 12.33	24.62 12.33	24.01 12.33	23.40 12.33	22.80 12.33	22.20 12.33
2 COMBINED AT										
+	CPO+J3	9.270	1	FLOW TIME	49.23 13.67	46.60 13.67	44.38 13.67	41.92 13.83	40.06 13.83	38.50 13.83
DIVERSION TO										
+	DNA	9.270	1	FLOW TIME	18.45 13.67	13.19 13.67	8.75 13.67	3.83 13.83	.12 13.83	.00 13.83
HYDROGRAPH AT										
+	D@NOA	9.270	1	FLOW TIME	39.89 13.17	39.99 14.17	39.75 13.50	39.62 14.00	39.94 13.83	38.50 13.83
ROUTED TO										
+	RS-NOA	9.270	1	FLOW TIME	28.95 14.83	29.08 14.83	29.02 14.67	28.77 14.67	28.35 14.67	27.63 14.67
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5104.12 14.83	5104.13 14.83	5104.13 14.67	5104.11 14.67	5104.08 14.67	5104.04 14.67
HYDROGRAPH AT										
+	I-K	.374	1	FLOW TIME	153.89 12.83	150.30 12.83	146.72 12.83	143.17 12.83	139.64 12.83	136.13 12.83
DIVERSION TO										
+	D-IK	.374	1	FLOW TIME	76.94 12.83	75.15 12.83	73.36 12.83	71.58 12.83	69.82 12.83	68.06 12.83
HYDROGRAPH AT										
+	DVI-K	.374	1	FLOW TIME	76.94 12.83	75.15 12.83	73.36 12.83	71.58 12.83	69.82 12.83	68.06 12.83
HYDROGRAPH AT										
+	WV20-B	.017	1	FLOW TIME	20.35 12.33	19.99 12.33	19.63 12.33	19.28 12.33	18.92 12.33	18.57 12.33
2 COMBINED AT										
+	CPEMS	.391	1	FLOW TIME	82.12 12.67	80.18 12.67	78.24 12.67	76.32 12.67	74.41 12.67	72.51 12.67
DIVERSION TO										
+	DNB	.391	1	FLOW TIME	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50
HYDROGRAPH AT										
+	D@NOB	.391	1	FLOW TIME	42.12 12.67	40.18 12.67	38.97 13.33	39.87 13.33	39.23 13.33	38.34 13.33
ROUTED TO										
+	RS-NOB	.391	1	FLOW TIME	7.73 18.83	7.69 18.67	7.65 18.67	7.61 18.67	7.57 18.67	7.52 18.50
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5107.23 18.83	5107.19 18.83	5107.15 18.83	5107.11 18.83	5107.07 18.67	5107.02 18.67
2 COMBINED AT										
+	NORTH	9.661	1	FLOW TIME	36.44 14.83	36.53 14.83	36.44 14.83	36.13 14.67	35.67 14.67	34.90 14.67
HYDROGRAPH AT										
+	M	.560	1	FLOW TIME	229.45 12.67	223.62 12.67	217.83 12.67	212.08 12.67	206.37 12.67	200.70 12.67



ROUTED TO											
+	RES-M	.560	1	FLOW TIME	59.65 13.67	58.59 13.67	57.49 13.67	56.41 13.67	55.37 13.67	54.34 13.67	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	4.96 13.67	4.86 13.67	4.75 13.67	4.64 13.67	4.54 13.67	4.44 13.67	
HYDROGRAPH AT											
+	OFF-4	.060	1	FLOW TIME	27.36 12.50	26.64 12.50	25.94 12.50	25.24 12.50	24.54 12.50	23.85 12.50	
2 COMBINED AT											
+	M+OFF4	.620	1	FLOW TIME	67.04 13.00	65.81 13.00	64.59 13.00	63.22 13.00	61.91 13.17	60.76 13.17	
DIVERSION TO											
+	DDM	.620	1	FLOW TIME	13.41 13.00	13.16 13.00	12.92 13.00	12.64 13.00	12.38 13.17	12.15 13.17	
HYDROGRAPH AT											
+	D@M	.620	1	FLOW TIME	53.63 13.00	52.65 13.00	51.67 13.00	50.58 13.00	49.53 13.17	48.61 13.17	
HYDROGRAPH AT											
+	OFF-3	.191	1	FLOW TIME	88.81 12.67	86.71 12.67	84.62 12.67	82.55 12.67	80.48 12.67	78.43 12.67	
2 COMBINED AT											
+	OF3+4	.811	1	FLOW TIME	131.95 12.83	128.56 12.83	125.18 12.83	121.76 12.83	118.25 12.83	114.76 12.83	
HYDROGRAPH AT											
+	EM-1	.046	1	FLOW TIME	80.73 12.33	79.70 12.33	78.67 12.33	77.65 12.33	76.62 12.33	75.59 12.33	
2 COMBINED AT											
+	JEM1+	.857	1	FLOW TIME	175.19 12.50	171.35 12.50	167.54 12.50	163.74 12.50	159.97 12.50	156.22 12.50	
HYDROGRAPH AT											
+	TRI	.009	1	FLOW TIME	6.87 12.33	6.71 12.33	6.55 12.33	6.39 12.33	6.24 12.33	6.08 12.33	
2 COMBINED AT											
+	CPPP1	.866	1	FLOW TIME	179.42 12.50	175.49 12.50	171.58 12.50	167.70 12.50	163.84 12.50	160.00 12.50	
ROUTED TO											
+	PP-1	.866	1	FLOW TIME	63.48 14.50	63.43 14.33	63.37 14.33	63.32 14.33	63.27 14.17	62.83 14.17	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	22.07 14.50	22.05 14.50	22.04 14.33	22.02 14.33	22.00 14.17	21.85 14.17	
ROUTED TO											
+	RCHPP1	.866	1	FLOW TIME	63.97 13.17	63.58 13.50	63.37 14.50	63.33 14.00	63.28 14.33	62.83 14.33	
DIVERSION TO											
+	DNC	.866	1	FLOW TIME	40.00 13.17	40.00 13.17	40.00 13.17	40.00 13.17	40.00 13.17	40.00 13.17	
HYDROGRAPH AT											
+	D@NOC	.866	1	FLOW TIME	39.97 21.50	39.59 21.33	39.83 21.00	39.89 20.83	39.66 20.67	39.67 20.33	
ROUTED TO											
+	RS-NOC	.866	1	FLOW TIME	31.83 22.67	31.89 22.33	31.98 22.17	32.06 22.00	32.14 21.67	32.22 21.50	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	5097.38 22.67	5097.39 22.33	5097.40 22.17	5097.41 22.00	5097.41 21.67	5097.42 21.50	
2 COMBINED AT											
+	CP-NOR	10.527	1	FLOW TIME	58.69 15.00	58.69 14.83	58.57 14.83	58.19 14.83	57.61 14.83	56.58 14.83	
HYDROGRAPH AT											
+	IWEST	.350	1	FLOW TIME	187.08 12.50	182.50 12.50	177.95 12.50	173.43 12.50	168.93 12.50	164.47 12.50	
DIVERSION TO											
+	DDIW	.350	1	FLOW TIME	149.67 12.50	146.00 12.50	142.36 12.50	138.74 12.50	135.14 12.50	131.57 12.50	
HYDROGRAPH AT											
+	D@IW	.350	1	FLOW TIME	37.42 12.50	36.50 12.50	35.59 12.50	34.69 12.50	33.79 12.50	32.89 12.50	
HYDROGRAPH AT											
+	OWEST	.180	1	FLOW	5.07	3.90	2.79	1.52	.15	.00	

			TIME	17.50	17.67	18.00	18.17	18.33	.00
2 COMBINED AT									
+	CP1	.530	1 FLOW TIME	37.42 12.50	36.50 12.50	35.59 12.50	34.69 12.50	33.79 12.50	32.89 12.50
2 COMBINED AT									
+	NOR+I	11.057	1 FLOW TIME	68.36 12.67	67.23 12.67	66.13 12.67	64.94 12.67	63.81 12.67	62.69 12.67
HYDROGRAPH AT									
+	EM4	.119	1 FLOW TIME	186.95 12.33	184.32 12.33	181.68 12.33	179.05 12.33	176.43 12.33	173.80 12.33
ROUTED TO									
+	EMB-1	.119	1 FLOW TIME	54.03 12.83	53.59 12.83	53.15 12.83	52.72 12.83	52.29 12.83	51.78 12.83
			** PEAK STAGES IN FEET **						
			1 STAGE TIME	5082.25 12.83	5082.20 12.83	5082.14 12.83	5082.09 12.83	5082.04 12.83	5081.98 12.83
ROUTED TO									
+	RHEMB1	.119	1 FLOW TIME	53.68 12.83	53.26 12.83	52.82 12.83	52.34 12.83	51.86 12.83	51.30 12.83
HYDROGRAPH AT									
+	EM-6	.045	1 FLOW TIME	39.35 12.50	38.33 12.50	37.30 12.50	36.28 12.50	35.27 12.50	34.25 12.50
HYDROGRAPH AT									
+	EM-7	.061	1 FLOW TIME	80.64 12.33	79.43 12.33	78.21 12.33	77.00 12.33	75.79 12.33	74.58 12.33
3 COMBINED AT									
+	CP-PP2	.226	1 FLOW TIME	159.60 12.50	156.91 12.50	154.18 12.50	151.52 12.50	148.76 12.50	146.12 12.50
ROUTED TO									
+	PP-2	.226	1 FLOW TIME	29.33 15.17	29.23 15.17	29.13 15.17	29.03 15.00	28.86 15.00	28.67 15.00
			** PEAK STAGES IN FEET **						
			1 STAGE TIME	5177.16 15.17	5177.11 15.17	5177.06 15.17	5177.01 15.00	5176.97 15.00	5176.92 15.00
2 COMBINED AT									
+	JCHAN2	11.283	1 FLOW TIME	93.03 12.67	91.81 12.67	90.80 14.83	90.28 14.67	89.49 14.67	88.25 14.67
ROUTED TO									
+	CHAN-2	11.283	1 FLOW TIME	92.89 12.67	91.03 14.83	90.79 14.83	90.28 14.83	89.46 14.83	88.21 14.83
HYDROGRAPH AT									
+	L2	.252	1 FLOW TIME	159.85 12.50	156.27 12.50	152.70 12.50	149.16 12.50	145.63 12.50	142.13 12.50
DIVERSION TO									
+	D-L	.252	1 FLOW TIME	79.92 12.50	78.13 12.50	76.35 12.50	74.58 12.50	72.82 12.50	71.06 12.50
HYDROGRAPH AT									
+	DØL	.252	1 FLOW TIME	79.92 12.50	78.13 12.50	76.35 12.50	74.58 12.50	72.82 12.50	71.06 12.50
ROUTED TO									
+	RES-L	.252	1 FLOW TIME	36.12 12.83	35.36 12.83	34.60 12.83	33.85 12.83	33.10 12.83	32.36 12.83
			** PEAK STAGES IN FEET **						
			1 STAGE TIME	3.81 12.83	3.74 12.83	3.66 12.83	3.58 12.83	3.51 12.83	3.44 12.83
HYDROGRAPH AT									
+	L1	.038	1 FLOW TIME	25.58 12.33	24.98 12.33	24.38 12.33	23.79 12.33	23.20 12.33	22.62 12.33
3 COMBINED AT									
+	JCHAN4	11.573	1 FLOW TIME	143.03 12.67	140.02 12.67	138.18 12.67	135.72 12.67	132.82 12.67	131.13 12.67
ROUTED TO									
+	RECH4A	11.573	1 FLOW TIME	138.46 12.67	135.90 12.67	133.96 12.67	131.05 12.67	128.74 12.67	127.13 12.67
ROUTED TO									
+	RCH4B	11.573	1 FLOW TIME	135.18 12.83	132.85 12.83	130.60 12.83	128.16 12.83	125.52 12.83	124.37 12.83
HYDROGRAPH AT									
+	WV-20A	.013	1 FLOW TIME	7.92 12.33	7.72 12.33	7.51 12.33	7.31 12.33	7.11 12.33	6.90 12.33

ROUTED TO										
+	HASKEL	.013	1	FLOW TIME	2.00 12.83	1.96 12.83	1.92 12.83	1.89 12.83	1.85 12.83	1.82 12.83
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5195.33 12.83	5195.32 12.83	5195.30 12.83	5195.29 12.83	5195.27 12.83	5195.26 12.83
HYDROGRAPH AT										
+	EM-2	.062	1	FLOW TIME	67.41 12.50	66.33 12.50	65.25 12.50	64.17 12.50	63.09 12.50	62.02 12.50
2 COMBINED AT										
+	20A+2	.075	1	FLOW TIME	69.27 12.50	68.15 12.50	67.04 12.50	65.93 12.50	64.82 12.50	63.71 12.50
ROUTED TO										
+	EMG-1	.075	1	FLOW TIME	35.65 12.83	35.09 12.83	34.54 12.83	33.98 12.83	33.43 12.83	32.88 12.83
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	88.69 12.83	88.65 12.83	88.61 12.83	88.57 12.83	88.53 12.83	88.49 12.83
ROUTED TO										
+	EMG-1	.075	1	FLOW TIME	35.08 13.00	34.82 13.00	33.90 13.00	33.70 13.00	32.80 13.00	32.58 13.00
HYDROGRAPH AT										
+	EMTC	.053	1	FLOW TIME	39.62 12.33	38.41 12.33	37.32 12.50	36.28 12.50	35.25 12.50	34.22 12.50
HYDROGRAPH AT										
+	EM-10	.053	1	FLOW TIME	29.86 12.50	28.98 12.50	28.11 12.50	27.24 12.50	26.38 12.50	25.52 12.50
3 COMBINED AT										
+	JEM02	.181	1	FLOW TIME	88.46 12.50	86.58 12.50	83.74 12.50	81.44 12.50	79.12 12.50	76.46 12.50
ROUTED TO										
+	EMO-2	.181	1	FLOW TIME	49.68 13.17	48.52 13.17	47.22 13.17	45.95 13.17	44.73 13.17	43.41 13.17
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	69.74 13.17	69.69 13.17	69.63 13.17	69.58 13.17	69.53 13.17	69.48 13.17
ROUTED TO										
+	EMOc	.181	1	FLOW TIME	49.30 13.17	48.14 13.17	46.77 13.33	45.57 13.33	44.42 13.33	43.18 13.33
HYDROGRAPH AT										
+	EM-11	.012	1	FLOW TIME	15.44 12.17	14.99 12.17	14.54 12.17	14.10 12.17	13.65 12.17	13.21 12.17
HYDROGRAPH AT										
+	EM-9	.021	1	FLOW TIME	27.01 12.17	26.23 12.17	25.45 12.17	24.67 12.17	23.89 12.17	23.12 12.17
3 COMBINED AT										
+	JG2&B2	.214	1	FLOW TIME	53.33 13.17	52.11 13.17	50.67 13.17	49.31 13.17	48.02 13.17	46.60 13.33
HYDROGRAPH AT										
+	EM-8	.046	1	FLOW TIME	45.35 12.33	44.08 12.33	42.81 12.33	41.54 12.33	40.29 12.33	39.03 12.33
HYDROGRAPH AT										
+	EM-12	.015	1	FLOW TIME	28.78 12.17	28.10 12.17	27.41 12.17	26.72 12.17	26.03 12.17	25.33 12.17
3 COMBINED AT										
+	TODETN	.275	1	FLOW TIME	112.78 12.33	109.94 12.33	107.10 12.33	104.27 12.33	101.45 12.33	98.64 12.33
ROUTED TO										
+	DETN	.275	1	FLOW TIME	33.01 14.67	32.32 14.67	31.61 14.67	30.91 14.67	30.23 14.67	29.51 14.83
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	3.50 14.67	3.43 14.67	3.36 14.67	3.29 14.67	3.22 14.67	3.15 14.83
2 COMBINED AT										
+	J4B	11.848	1	FLOW TIME	153.97 12.83	150.95 12.83	147.97 12.83	144.93 13.00	141.96 13.00	139.73 12.83
ROUTED TO										
+	RCH-4C	11.848	1	FLOW TIME	152.84 13.00	149.97 13.00	147.31 13.00	144.37 13.00	141.40 13.00	139.19 13.00
HYDROGRAPH AT										
+	A3	.055	1	FLOW	81.57	80.33	79.10	77.86	76.63	75.40





				** PEAK STAGES IN FEET **							
		1	STAGE	5060.30	5060.26	5060.22	5060.19	5060.15	5060.11		
			TIME	14.33	14.33	14.33	14.33	14.33	14.33		
3 COMBINED AT											
+	ABMSR	12.097	1 FLOW TIME	198.14 13.00	194.73 13.00	191.46 13.00	187.84 13.00	184.09 13.00	181.11 13.00		
HYDROGRAPH AT											
+	OFF-1	.023	1 FLOW TIME	14.87 12.33	14.50 12.33	14.12 12.33	13.75 12.33	13.38 12.33	13.02 12.33		
ROUTED TO											
+	R8	.023	1 FLOW TIME	14.17 12.50	13.83 12.50	13.49 12.50	12.98 12.50	12.65 12.50	12.31 12.50		
HYDROGRAPH AT											
+	A5	.060	1 FLOW TIME	101.37 12.33	99.97 12.33	98.58 12.33	97.18 12.33	95.78 12.33	94.39 12.33		
HYDROGRAPH AT											
+	CSR-7	.014	1 FLOW TIME	17.56 12.33	17.26 12.33	16.96 12.33	16.66 12.33	16.36 12.33	16.06 12.33		
3 COMBINED AT											
+	J-1	.097	1 FLOW TIME	129.54 12.33	127.49 12.33	125.44 12.33	123.40 12.33	121.38 12.33	119.37 12.33		
ROUTED TO											
+	EXDET	.097	1 FLOW TIME	118.99 12.50	120.21 12.50	121.42 12.50	122.46 12.50	123.54 12.50	124.59 12.50		
				** PEAK STAGES IN FEET **							
				1	STAGE	5125.29	5125.29	5125.29	5125.29	5125.29	5125.30
					TIME	12.50	12.50	12.50	12.50	12.50	12.50
DIVERSION TO											
+	D-DIV	.097	1 FLOW TIME	59.50 12.50	60.10 12.50	60.71 12.50	61.23 12.50	61.77 12.50	62.30 12.50		
HYDROGRAPH AT											
+	DIV	.097	1 FLOW TIME	59.50 12.50	60.10 12.50	60.71 12.50	61.23 12.50	61.77 12.50	62.30 12.50		
ROUTED TO											
+	REXDET	.097	1 FLOW TIME	54.37 12.50	54.01 12.50	53.90 12.50	52.96 12.50	52.05 12.50	52.34 12.50		
HYDROGRAPH AT											
+	OFF-2	.050	1 FLOW TIME	28.29 12.33	27.55 12.33	26.82 12.33	26.09 12.33	25.36 12.33	24.64 12.33		
ROUTED TO											
+	R-19	.050	1 FLOW TIME	28.11 12.50	27.41 12.50	26.72 12.50	26.39 12.50	25.69 12.50	24.99 12.50		
HYDROGRAPH AT											
+	CSR-6A	.005	1 FLOW TIME	5.79 12.33	5.68 12.33	5.58 12.33	5.47 12.33	5.37 12.33	5.27 12.33		
ROUTED TO											
+	EXDT1A	.005	1 FLOW TIME	5.02 12.33	5.00 12.33	4.97 12.33	4.95 12.33	4.92 12.33	4.89 12.33		
				** PEAK STAGES IN FEET **							
				1	STAGE	5105.30	5105.27	5105.24	5105.21	5105.19	5105.16
					TIME	12.33	12.33	12.33	12.33	12.33	12.33
2 COMBINED AT											
+	J-6	.055	1 FLOW TIME	33.01 12.50	32.27 12.50	31.53 12.50	31.16 12.50	30.35 12.50	29.47 12.50		
HYDROGRAPH AT											
+	CSR-6	.025	1 FLOW TIME	35.04 12.33	34.47 12.33	33.91 12.33	33.36 12.33	32.80 12.33	32.24 12.33		
2 COMBINED AT											
+	CPXDT1	.080	1 FLOW TIME	59.86 12.33	58.63 12.33	57.41 12.33	55.94 12.33	54.72 12.33	53.52 12.33		
ROUTED TO											
+	EXDT1	.080	1 FLOW TIME	20.24 12.83	20.03 12.83	19.82 12.83	19.61 12.83	19.40 12.83	19.20 12.83		
				** PEAK STAGES IN FEET **							
				1	STAGE	5106.94	5106.82	5106.69	5106.56	5106.44	5106.32
					TIME	12.83	12.83	12.83	12.83	12.83	12.83
HYDROGRAPH AT											
+	A1	.090	1 FLOW TIME	124.95 12.33	122.93 12.33	120.92 12.33	118.92 12.33	116.92 12.33	114.92 12.33		
2 COMBINED AT											
+	J8	.170	1 FLOW	139.01	136.74	134.49	132.17	129.93	127.69		







**PROPOSED CONDITIONS THROUGH PHASE 20**

VPH Proposed Conditions  
 Base model: Woodland  
 Village Through Ph 20

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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998 AND FEB 2010
* VERSION 4.1R
* RGMHEC2000 WWW.HEC-1.COM
* RUN DATE 07MAR21 TIME 18:18:59
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
  
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DDIAGRAM
1 ID 100 yr 24 hr event
2 ID VILLAGE PARKWAY HOMES
3 ID FILE NAME VPH-DIV2.DA T
4 ID USING TYPE II STORM DISTRIBUTION
5 ID BASE MODEL FROM WOODLAND VILLAGE PH 20
* DARF AREA (SQ. MI.)
* 1.00 0 - 2
* 0.99 2.1 - 8
* 0.98 8.1 - 16
* 0.97 16.1 - 29
* 0.96 29.1 - 43
* 0.95 43.1 - 63
* 0.94 63.1 - 98
6 IT 10 800
7 IO 5 0
8 JR PREC 1.0 .99 .98 .97 .96 .95
9 KK A
10 BA 0.72
11 PH 1 .68 1.24 2.06 2.32 2.52 2.94 3.76 4.59
12 LS 1.7 54
13 UD .62
14 KK B
15 BA 1.78
16 LS 1.63 55
17 UD 1.1
18 KK D@A&B
19 HC 2
20 KK D-A&B
21 DT D-AB
22 DI 0 10 50 100 500
23 DQ 0 5 25 50 250
24 KK RCH-1
25 KM ROUTE A&B TO J1@AB
26 RD 10200 .04 .12 TRAP 3 1
27 KK C
28 BA 1.26
29 LS 1.7 54
30 UD .82
31 KK J1@A&B
32 HC 2
33 KK RCH-2
34 RD 3500 .06 .12 TRAP 10 2.5
  
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HEC-1 INPUT

PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
  
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35	KK	D							
36	BA	1.0							
37	LS	1.57	50						
38	UD	.63							
39	KK	J2ABCD							
40	HC	2							
41	KK	DJ2							
42	KM	CHANGE DIVERSION FROM 50% TO 75%							
43	DT	J2							
44	DI	0	10	50	100	500			
45	DQ	0	7.5	37.5	75	375			
46	KK	E							
47	BA	.615							
48	LS	1.45	58						
49	UD	.68							
50	KK	D@E							
51	DT	DE							
52	DI	0	10	50	100	500			
53	DQ	0	10	50	100	500			
54	KK	F							
55	BA	0.815							
56	LS	1.51	57						
57	UD	1							
58	KK	D@F							
59	DT	DF							
60	DI	0	10	50	100	500			
61	DQ	0	10	50	100	500			
62	KK	J3-1							
63	HC	2							
64	KK	J							
65	BA	1.14							
66	LU	4	0.1						
67	UD	.67							
68	KK	J3-2							
69	HC	2							
70	KK	G							
71	BA	0.81							
72	LS	1.03	66						
73	UD	.93							

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HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

74	KK	D@G							
75	DT	DDG							
76	DI	0	10	50	100	500			
77	DQ	0	10	50	100	500			
78	KK	H							
79	BA	0.74							
80	LS	1.12	64						
81	UD	.63							
82	KK	D@H							
83	DT	DDH							
84	DI	0	10	50	100	500			
85	DQ	0	10	50	100	500			
86	KK	J3							
87	HC	4							
88	KK	RCH-3							
89	RD	8000	.04	.05	TRAP	10	1		
90	KK	D@J3							
91	DT	D-J3							
92	DI	0	10	50	100	500			
93	DQ	0	5	25	50	250			
94	KK	IEAST							
95	BA	.18							
96	LS		64						
97	UD	.22							
98	KK	D@IE							
99	DT	DDG							
100	DI	0	10	50	100	500			
101	DQ	0	8	40	80	400			
102	KK	OEAST							
103	BA	.21							
104	LU	4	.1						

105 KK CP2  
 106 HC 2  
 107 KK CPO+J3  
 108 HC 2  
 109 KK D@NOA  
 110 DT DNA  
 111 DI 0 40 60 100 500 1000  
 112 DQ 0 0 40 40 40 40  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

113 KK RS-NOA NORTH RESERVOIR A  
 114 KM 36" OUTLET  
 115 RS 1 STOR 0  
 116 SA 0 .17 .91 2.24 3.55 4.94  
 117 SE 5101.5 5102 5103 5104 5105 5106  
 118 SQ 0 6 19 35 50 60  
 119 SE 5101.5 5102.5 5103.5 5104.5 5105.5 5106.5  
 120 KK I-KWATERSHED CONSISTING OF K+ EM-3+EM-5 APPROX.  
 121 BA .3741  
 122 LS 65  
 123 UD 0.61

124 KK DVI-K DIVERT FLOW FROM I-K SAME RATE AS FROM K  
 125 DT D-1K  
 126 DI 0 10 100 500  
 127 DQ 0 5 50 250

128 KK WV20-B PART OF WV-20 GOING NORTH  
 129 BA .017  
 130 LS 74  
 131 UD .16

132 KK CPEM5  
 133 HC 2

134 KK D@NOB  
 135 DT DNB  
 136 DI 0 40 60 100 500 1000  
 137 DQ 0 0 40 40 40 40

138 KK RS-NOB NORTH RESERVOIR B  
 139 KM 12" OUTLET  
 140 RS 1 STOR 0  
 141 SA 0 0.02 0.16 0.52 1.73 3.30 5.24 5.38 5.52  
 142 SE 5102.5 5103 5104 5104 5106 5107 5108 5109 5110  
 143 SQ 0 2.2 4.5 5.6 7 8 9 10 11  
 144 SE 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5 5109.5

145 KK NORTH  
 146 HC 2

147 KK M  
 148 BA 0.56  
 149 LS 1.17 63  
 150 UD 0.52

151 KK RES-M  
 152 RS 1 STOR 0  
 153 SA 2.5 2.56 2.66 2.79 1.95 3.15 3.4 3.72 4.12  
 154 SE 0 1.38 2.06 2.68 3.29 3.99 4.87 5.91 7.1  
 155 SQ 0 6 19 35 50 60 72 78 90  
 156 SE 0 1 2 3 4 5 6 7 8  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

157 KK OFF-4 OFFSITE 4  
 158 BA .06  
 159 LS 63  
 160 UD .42

161 KK M+OFF4 COMBINE OFF4 + POND M  
 162 HC 2

163 KK D@M  
 164 DT DDM  
 165 DI 0 10 50 100 500 1000  
 166 DQ 0 2 10 20 100 200

167 KK OFF-3  
 168 BA 0.191  
 169 LS 65  
 170 UD 0.52

171 KK OF3+4 COMBINE OFF3 & 0 FF4 & POND M  
 172 HC 2

173 KK EM-1  
 174 BA .046  
 175 LS 88  
 176 UD 0.25

177 KK JEM1+ COMBINE EM1, POND M, OFF3 & OFF4  
 178 KM SAME AS JM EM1 OFF3 OFF4 IN HEC-HMS  
 179 HC 2

180 KK TRI TRIANGULAR AREA EAST OF VILLAGE PKWY  
 181 BA .009  
 182 LS 64.5  
 183 UD 0.16

184 KK CPPP1 ADD TRIANGULAR AREA TO FLOW INTO PP-1  
 185 HC 2

186 KK PP-1  
 187 KM NOW WITH 30" OUTLET  
 188 RS 1 STOR 0  
 189 SA 0 .11 .34 .73 1.19 1.82 1.96 2.10 2.24  
 190 SA 2.52  
 191 SE 14.34 15 16 17 18 19 20 21 22  
 192 SE 24  
 193 SQ 0 5.5 16 28 38 45 50 57 62  
 194 SQ 70 75  
 195 SE 14.34 15.34 16.34 17.34 18.34 19.34 20.34 21.34 22.34  
 196 SE 24.34

HEC-1 INPUT

1  
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

197 KK RCHPP1  
 198 RD 2475 .007 .04 TRAP 3 3

199 KK D@NOC  
 200 DT DNC  
 201 DI 0 40 60 100 500 1000  
 202 DQ 0 0 40 40 40 40

203 KK RS-NOC NORTH RESERVOIR C  
 204 KM 30" OUTLET  
 205 RS 1 STOR 0  
 206 SA 0 .22 .82 2.4 3.85 4.54 5.03 5.31  
 207 SE 5094 5095 5096 5097 5098 5099 5100 5101  
 208 SQ 0 5.5 16 28 38 45 50 57  
 209 SE 5094 5095 5096 5097 5098 5099 5100 5101

210 KK CP-NOR COMBINE 3 NORTH DET BASINS  
 211 HC 2

212 KK IWEST  
 213 BA .35  
 214 LS 64  
 215 UD .37

216 KK D@IW  
 217 DT DDIW  
 218 DI 0 10 50 100 500  
 219 DQ 0 8 40 80 400

220 KK OWEST  
 221 BA .18  
 222 LU 4 .1

223 KK CP1  
 224 HC 2

225 KK NOR+I COMBINE FLOW FROM 3 DET BASINS & OFFSITE WATERSHED I  
 226 HC 2

227 KK EM4  
 228 BA .1193  
 229 LS 84  
 230 UD .25

231 KK EMB-1  
 232 RS 1 STOR 0  
 233 SA 1.5 1.54 1.6 1.68 1.79 1.95 2.15  
 234 SE 5078 5079.1 5079.69 5080.25 5080.95 5081.86 5082.96  
 235 SQ 0 8 26 40 52 60  
 236 SE 5078 5079 5080 5081 5082 5083

HEC-1 INPUT

1  
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

237 KK RHEMB1 REACH EMB-1  
 238 RD 759 .0066 .04 TRAP 3 3

239 KK EM-6  
 240 BA .0455  
 241 LS 1.5 84



242	UD	.32								
243	KK	EM-7								
244	BA	.061								
245	LS	.5	83							
246	UD	.3								
247	KK	CP-PP2								
248	HC	3								
249	KK	PP-2	NORTH OF BRIAR ROAD							
250	KM	OUTLET IS ONE 30" RCP								
251	RS	1	STOR	0						
252	SA	0	.02	.16	.52	1.73	3.30	5.24	5.38	5.52
253	SE	5171	5171.5	5172.5	5173.5	5174.5	5175.5	5176.5	5177.5	5178.5
254	SQ	0	5.7	13.5	18.6	22	25	29	31	32
255	SE	5171	5172	5173	5174	5175	5176	5177	5178	5178.5
256	KK	JCHAN2								
257	HC	2								
258	KK	CHAN-2								
259	RD	1130	.005	.04		TRAP	6	3		
260	KK	L2								
261	BA	.234								
262	LS	1.03	66							
263	UD	.33								
264	KK	D@L								
265	DT	D-L								
266	DI	0	10	50	100	500				
267	DQ	0	5	25	50	250				
268	KK	RES-L								
269	RS	1	STOR	0						
270	SA	0.6	0.64	0.69	0.76	0.86	1			
271	SE	0	1.69	2.25	2.95	3.86	4.96			
272	SQ	0	5.5	16	28	38	45			
273	SE	0	1	2	3	4	5			
274	KK	L3	PART OF L2 DRAINING TO VILLAGE PARKWAY HOMES							
275	BA	.018								
276	LS		77							
277	UD	0.2								

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

278	KK	VPH-1	VILL. PKWY HOMES NORTH PORTION							
279	BA	0.035								
280	LS		77							
281	UD	.19								
282	KK	VPCP-1								
283	HC	2								
284	KK	L1								
285	BA	.029								
286	LS		77							
287	UD	.21								
288	KK	P								
289	BA	.031								
290	LS		77							
291	UD	0.1								
292	KK	VPCP2								
293	HC	2								
294	KK	Q								
295	BA	.052								
296	LS		77							
297	UD	.19								
298	KK	VPCP2A	FLOW ENTERING RETENTION/DETENTION POND							
299	HC	2								
300	KK	D@VPH	INFILTRATION @ VP RETENTION POND							
301	DT	VPH								
302	DI	0	10	25	50	100	140	150	155	200
303	DQ	0	0	12	12	12	12	12	12	12
304	KK	VPHRPRETENTION/DETENTION POND @ VILLAGE PKWY HOMES								
305	KM	30-IN RCP OUTLET@ 61.5 FT								
306	RS	1	STOR	0						
307	SA	.278	.607	.848	.972	1.013				
308	SE	5060	5062	5064	5066	5067				
309	SQ	0	0	4.5	16	29	35	40	50	
310	SE	5060	5061.5	5062.5	5063.5	5064.5	5065.5	5066.	5067	
311	KK	D-SOU								
312	DT	SOUTH								

313 DI 0 10 50 100 500  
 314 DQ 0 10 50 100 500  
 315 KK VPCP3 COMBINE FLOWS GOING TO RET PONDS  
 316 HC 2

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

317 KK VPNEPD RETENTION/DETENTION POND  
 318 KM 18-IN RCP OUTLET@ 60 FT  
 319 KM 2 FT OF GRAVEL AT BOTTOM OF POND  
 320 RS 1 STOR 0  
 321 SA .14 .14 .34 .73 .94 1.13  
 322 SE 56 57.9 58 62 64 66  
 323 SQ 0 0 0 4 13  
 324 SE 56 57.9 58 60 61 62 63 64 65 66

325 KK VPCP1A COMBINE OUTFLOW FROM PVH NE POND WITH MAIN CHANNEL  
 326 HC 3

327 KK RECH4A  
 328 RD 395 .001 .04 TRAP 8 3

329 KK RCH4B  
 330 RD 665 .001 .04 TRAP 10 3

331 KK WV-20A PART OF WV-20 GOING SOUTH  
 332 BA .013  
 333 LS 61  
 334 UD .15

335 KK HASKEL 12" RCP OUTLET  
 336 RS 1 STOR 0  
 337 SA 0 .47 .55 .60 .65  
 338 SE 5194.5 5195 5196 5197 5198  
 339 SQ 0 2.4 4.7 6 7.5  
 340 SE 5194.5 5195.5 5196.5 5197.5 5198.5

341 KK EM-2  
 342 BA .0621  
 343 LS 78  
 344 UD .32

345 KK 20A+2 COMBINE W VILLAGE 20A POND WITH EM-2  
 346 KM FLOW GOES INTO POND EMG-1  
 347 HC 2

348 KK EMG-1 DETENTION POND EMG-1  
 349 RS 1 STOR 0  
 350 SA 0.8 0.83 .87 .93 1.02 1.13 1.29  
 351 SE 86 87.1 87.69 88.25 88.95 89.86 90.96  
 352 SQ 0 8 26 40 52 60  
 353 SE 86 87 88 89 90 91

354 KK EMG-1  
 355 RD 1630 .01 .04 TRAP 3 3

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

356 KK EMTc  
 357 BA .053  
 358 LS 1.5 79  
 359 UD .27

360 KK EM-10  
 361 BA .053  
 362 LS 1.5 72  
 363 UD .32

364 KK JEM02  
 365 HC 3

366 KK EMO-2  
 367 RS 1 STOR 0  
 368 SA 1.2 1.25 1.26 1.27 1.29 1.3 1.32 1.34 1.39  
 369 SE 67 68.49 68.91 69.31 69.72 70.21 70.69 71.31 72.8  
 370 SQ 0 11 32 56 76 90 100  
 371 SE 67 68 69 70 71 72 73

372 KK EMOc  
 373 RD 615 .003 .04 TRAP 0 3

374 KK EM-11  
 375 BA .012  
 376 LS 1.5 86  
 377 UD .13

378 KK EM-9  
 379 BA .021  
 380 LS 1.5 86

381 UD .13  
 382 KK JG2&B2  
 383 HC 3  
 384 KK EM-8  
 385 BA .046  
 386 LS 1.5 82  
 387 UD .22  
 388 KK EM-12  
 389 BA .015  
 390 LS 1.5 93  
 391 UD .12  
 392 KK TODETN  
 393 HC 3

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

394 KK DETN  
 395 RS 1 STOR 0  
 396 SA 2.25 2.31 2.4 2.5 2.63 2.78 2.96 3.18 3.48  
 397 SE 0 1.49 1.91 2.31 2.72 3.21 3.69 4.31 5.8  
 398 SQ 0 5.5 16 28 38 45 50  
 399 SE 0 1 2 3 4 5 6

400 KK J4B  
 401 HC 2  
 402 KK RCH-4C  
 403 RD 300 .001 .04 TRAP 12 3

404 KK A3  
 405 BA .055  
 406 LS 80  
 407 UD .16

408 KK A3A  
 409 BA .007  
 410 LS 76  
 411 UD .13

412 KK COMBA3  
 413 HC 2

414 KK RES-6  
 415 RS 1 STOR 0  
 416 SA 0.24 0.5 0.54 0.61 0.67 0.69  
 417 SE 5074 5075 5076 5077 5078 5079  
 418 SQ 0 4.3 14 24 30 35

419 KK A3B  
 420 BA .026  
 421 LS 77  
 422 UD .17

423 KK D-PARK  
 424 DT PARK  
 425 DI 0 20 100 500 1000  
 426 DQ 0 5 25 125 250

427 KK RES-5  
 428 RS 1 STOR 0  
 429 SA 0.25 0.28 0.32 0.35 0.39 0.43 0.46 0.5 0.59  
 430 SE 5069 5070 5071 5072 5073 5074 5075 5076 5077  
 431 SQ 0 4.3 14 24 30 35.4 40 44 44

432 KK R-9 ROUTING  
 433 RD 1000 .02 .05 TRAP 15 1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

434 KK A13A  
 435 BA .006  
 436 LS 72  
 437 UD .17

438 KK A13B  
 439 BA .04  
 440 LS 73  
 441 UD .18

442 KK COMA13  
 443 HC 2

444 KK A12A  
 445 BA .015  
 446 LS 75  
 447 UD .15







584	KK	R23								
585	RD	2600	.02	.05	TRAP	5	1			
586	KK	RPE								
587	BA	0.12								
588	LS		72							
589	UD	.28								
590	KK	ACS-1								
591	HC	2								
592	KK	VPH2								
593	BA	0.01								
594	LS		77							
595	UD	0.16								

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

596	KK	VPH-3								
597	BA	.01								
598	LS		77							
599	UD	0.15								
600	KK	VPCP2								
601	HC	2								
602	KK	VPH-4								
603	BA	.011								
604	LS		77							
605	UD	0.15								
606	KK	VPH-5								
607	BA	.005								
608	LS		77							
609	UD	.13								
610	KK	RCLDP								
611	DR	SOUTH								
612	KK	VPCP-4			COMBINE VPH3, 4, AND 5					
613	HC	4								
614	KK	VPDICH			VILLAGE PKWY HOMES DETENTION DITCH					
615	KM	OUTLETIS 30" RCP @ ELEV 5058.15								
616	RS	1 STOR	0							
617	SA	.0001	0.13	0.42	0.74	1				
618	SE	5058.1	5059.5	5060	5062	5063.5				
619	SQ	0	5	16	29	35	44	46		
620	SE	5058.1	5059.1	5060.1	5061.1	5062.1	5063.1	5063.5		
621	KK	Q2								
622	BA	.013								
623	LS		77							
624	UD	.16								
625	KK	VPCP6COMBINED FLOW IN MUD SPRINGS CHANNEL								
626	HC	4								
627	KK	PVE-1								
628	BA	.0128								
629	LS		76							
630	UD	.13								
631	KK	ABCDSP			ABOVE COLD SPRINGS ROAD					
632	HC	2								
633	KK	PVE-2								
634	BA	.011								
635	LS		76							
636	UD	.13								

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

637	KK	BLCSRD			BELOW COLD SPRINGS ROAD					
638	HC	2								
639	ZZ									

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

9 A  
 .  
 14 . B  
 .  
 .  
 18 D@A&B.....



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21 .-----> D-AB
20 D-A&B
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24 RCH-1
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27 .
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31 J1@A&B
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33 RCH-2
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35 .
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39 J2ABCD
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43 .-----> J2
41 DJ2
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46 .
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51 .-----> DE
50 D@E
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54 .
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.
59 .-----> DF
58 D@F
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62 J3-1
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.
.
64 .
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68 J3-2
.
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70 .
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.
75 .-----> DDG
74 D@G
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78 .
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83 .-----> DDH
82 D@H
.
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86 J3
.
.
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88 RCH-3
.
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91 .-----> D-J3
90 D@J3
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94 IEAST
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99 .-----> DDG
98 D@IE
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102 OEAST
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105 CP2
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107 CPO+J3
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110 .-----> DNA
109 D@NOA
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113	RS-NOA	V	
120	.	.	I-K
125	.	.	
124	DVI-K	----->	D-IK
128	.	.	WV20-B
132	CPEMS	.....	
135	.	.	
134	D@NOB	----->	DNB
138	RS-NOB	V	
145	NORTH	.....	
147	.	.	M
151	RES-M	V	
157	.	.	OFF-4
161	M+OFF4	.....	
164	.	.	
163	D@M	----->	DDM
167	.	.	OFF-3
171	OF3+4	.....	
173	.	.	EM-1
177	JEM1+	.....	
180	.	.	TRI
184	CPPP1	.....	
186	PP-1	V	
197	RCHPP1	V	
200	.	.	
199	D@NOC	----->	DNC
203	RS-NOC	V	
210	CP-NOR	.....	
212	IWEST	.	
217	.	.	
216	D@IW	----->	DDIW
220	.	.	OWEST
223	CP1	.....	
225	NOR+I	.....	
227	EM4	.	



345	.	20A+2	.....		
	.	V			
	.	V			
348	.	EMG-1			
	.	V			
	.	V			
354	.	EMG-1			
	.				
356	.		EMTC		
	.				
360	.			EM-10	
	.				
364	.	JEMO2	.....		
	.	V			
	.	V			
366	.	EMO-2			
	.	V			
	.	V			
372	.	EMOc			
	.				
374	.		EM-11		
	.				
378	.			EM-9	
	.				
382	.	JG2&B2	.....		
	.				
384	.		EM-8		
	.				
388	.			EM-12	
	.				
392	.	TODETN	.....		
	.	V			
	.	V			
394	.	DETN			
	.				
400	.	J4B	.....		
	.	V			
	.	V			
402	.	RCH-4C			
	.				
404	.	A3			
	.				
408	.		A3A		
	.				
412	.	COMBA3	.....		
	.	V			
	.	V			
414	.	RES-6			
	.				
419	.		A3B		
	.				
424	.			PARK	
423	.	D-PARK	----->		
	.	V			
	.	V			
427	.	RES-5			
	.	V			
	.	V			
432	.	R-9			
	.				
434	.		A13A		
	.				
438	.			A13B	
	.				
442	.		COMA13	.....	
	.				
444	.			A12A	
	.				
448	.			A12	
	.				
452	.			COMA12	.....



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454 . . . . . JRES3 .....
      . . . . . V
      . . . . . V
456 . . . . . RES-3
      . . . . .
461 . . . . . A13
      . . . . .
465 . . . . . A12B
      . . . . .
469 . . . . . JRES1 .....
      . . . . . V
      . . . . . V
471 . . . . . RES-1
      . . . . .
479 . . . . . ABMSR .....
      . . . . .
481 . . . . . OFF-1
      . . . . . V
      . . . . . V
485 . . . . . R8
      . . . . .
487 . . . . . A5
      . . . . .
491 . . . . . CSR-7
      . . . . .
495 . . . . . J-1 .....
      . . . . . V
      . . . . . V
497 . . . . . EXDET
      . . . . .
503 . . . . . -----> D-DIV
502 . . . . . DIV
      . . . . . V
      . . . . . V
506 . . . . . REXDET
      . . . . .
508 . . . . . OFF-2
      . . . . . V
      . . . . . V
512 . . . . . R-19
      . . . . .
514 . . . . . CSR-6A
      . . . . . V
      . . . . . V
518 . . . . . EXDT1A
      . . . . .
523 . . . . . J-6 .....
      . . . . .
525 . . . . . CSR-6
      . . . . .
529 . . . . . CPXDT1 .....
      . . . . . V
      . . . . . V
531 . . . . . EXDT1
      . . . . .
536 . . . . . A1
      . . . . .
540 . . . . . J8 .....
      . . . . . V
      . . . . . V
542 . . . . . R21
      . . . . .
544 . . . . . JRES2 .....
      . . . . . V
      . . . . . V
546 . . . . . RES2
      . . . . . V
      . . . . . V
554 . . . . . R22
      . . . . .
556 . . . . . CSR-4
      . . . . . V
      . . . . . V
560 . . . . . EXDET2
      . . . . .

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565 . . . . . CSR-3
. . . . .
569 . . . . . J11.....
. . . . . V
. . . . . V
571 . . . . . DITCH
. . . . .
573 . . . . . A2
. . . . .
577 . . . . . JRES15.....
. . . . . V
. . . . . V
579 . . . . . RES15
. . . . . V
. . . . . V
584 . . . . . R23
. . . . .
586 . . . . . RPE
. . . . .
590 . . . . . ACS-1.....
. . . . .
592 . . . . . VPH2
. . . . .
596 . . . . . VPH-3
. . . . .
600 . . . . . VPCP2.....
. . . . .
602 . . . . . VPH-4
. . . . .
606 . . . . . VPH-5
. . . . .
611 . . . . .
610 . . . . . RCLDP <----- SOUTH
. . . . .
612 . . . . . VPCP-4.....
. . . . . V
. . . . . V
614 . . . . . VPDICH
. . . . .
621 . . . . . Q2
. . . . .
625 . . . . . VPCP6.....
. . . . .
627 . . . . . PVE-1
. . . . .
631 . . . . . ABCDSP.....
. . . . .
633 . . . . . PVE-2
. . . . .
637 . . . . . BLCSRD.....

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(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 AND FEB 2010 *
* VERSION 4.1R *
* RGMHEC2000 WWW.HEC-1.COM *
* RUN DATE 07MAR21 TIME 18:18:59 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

100 yr 24 hr event  
VILLAGE PARKWAY HOMES  
FILE NAME VPH-DIV2.DA T  
USING TYPE II STORM DISTRIBUTION  
BASE MODEL FROM WOODLAND VILLAGE PH 20

7 IO            OUTPUT CONTROL VARIABLES  
                 IPRNT            5    PRINT CONTROL  
                 IPLOT            0    PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 10 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 800 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 6 0 ENDING DATE  
 NDTIME 1310 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .17 HOURS  
 TOTAL TIME BASE 133.17 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 1.00 .99 .98 .97 .96 .95

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION					
					RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
					1.00	.99	.98	.97	.96	.95
HYDROGRAPH AT +	A	.720	1	FLOW TIME	121.51 12.83	117.04 12.83	112.64 12.83	108.31 12.83	104.04 12.83	99.83 12.83
HYDROGRAPH AT +	B	1.780	1	FLOW TIME	220.78 13.33	213.16 13.33	205.63 13.33	198.22 13.33	190.92 13.33	183.72 13.33
2 COMBINED AT +	D0A&B	2.500	1	FLOW TIME	305.45 13.17	294.83 13.17	284.36 13.17	274.03 13.17	263.86 13.17	253.84 13.17
DIVERSION TO +	D-AB	2.500	1	FLOW TIME	152.72 13.17	147.41 13.17	142.18 13.17	137.02 13.17	131.93 13.17	126.92 13.17
HYDROGRAPH AT +	D-A&B	2.500	1	FLOW TIME	152.72 13.17	147.41 13.17	142.18 13.17	137.02 13.17	131.93 13.17	126.92 13.17
ROUTED TO +	RCH-1	2.500	1	FLOW TIME	154.00 13.67	148.35 13.67	142.60 13.67	134.73 13.67	129.09 13.67	124.07 13.83
HYDROGRAPH AT +	C	1.260	1	FLOW TIME	173.70 13.00	167.28 13.00	160.97 13.00	154.75 13.00	148.63 13.00	142.70 13.17
2 COMBINED AT +	J10A&B	3.760	1	FLOW TIME	292.49 13.33	277.67 13.33	264.27 13.50	253.43 13.50	243.81 13.50	234.54 13.50
ROUTED TO +	RCH-2	3.760	1	FLOW TIME	289.48 13.50	275.52 13.50	261.29 13.67	250.68 13.67	240.82 13.67	232.01 13.67
HYDROGRAPH AT +	D	1.000	1	FLOW TIME	166.69 12.83	160.98 12.83	155.35 12.83	149.80 12.83	144.33 12.83	138.95 12.83
2 COMBINED AT +	J2ABCD	4.760	1	FLOW TIME	375.21 13.50	358.74 13.50	340.56 13.50	321.28 13.50	307.53 13.50	293.48 13.67
DIVERSION TO +	J2	4.760	1	FLOW TIME	281.41 13.50	269.06 13.50	255.42 13.50	240.96 13.50	230.64 13.50	220.11 13.67
HYDROGRAPH AT +	DJ2	4.760	1	FLOW TIME	93.80 13.50	89.69 13.50	85.14 13.50	80.32 13.50	76.88 13.50	73.37 13.67
HYDROGRAPH AT +	E	.615	1	FLOW	142.56	138.11	133.71	129.35	125.05	120.80





2 COMBINED AT											
+	CPO+J3	9.270	1	FLOW TIME	49.23 13.67	46.60 13.67	44.38 13.67	41.92 13.83	40.06 13.83	38.50 13.83	
DIVERSION TO											
+	DNA	9.270	1	FLOW TIME	18.45 13.67	13.19 13.67	8.75 13.67	3.83 13.83	.12 13.83	.00 .00	
HYDROGRAPH AT											
+	D@NOA	9.270	1	FLOW TIME	39.89 13.17	39.99 14.17	39.75 13.50	39.62 14.00	39.94 13.83	38.50 13.83	
ROUTED TO											
+	RS-NOA	9.270	1	FLOW TIME	28.95 14.83	29.08 14.83	29.02 14.67	28.77 14.67	28.35 14.67	27.63 14.67	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5104.12 14.83	5104.13 14.83	5104.13 14.67	5104.11 14.67	5104.08 14.67	5104.04 14.67	
HYDROGRAPH AT											
+	I-K	.374	1	FLOW TIME	153.89 12.83	150.30 12.83	146.72 12.83	143.17 12.83	139.64 12.83	136.13 12.83	
DIVERSION TO											
+	D-IK	.374	1	FLOW TIME	76.94 12.83	75.15 12.83	73.36 12.83	71.58 12.83	69.82 12.83	68.06 12.83	
HYDROGRAPH AT											
+	DVI-K	.374	1	FLOW TIME	76.94 12.83	75.15 12.83	73.36 12.83	71.58 12.83	69.82 12.83	68.06 12.83	
HYDROGRAPH AT											
+	WV20-B	.017	1	FLOW TIME	20.35 12.33	19.99 12.33	19.63 12.33	19.28 12.33	18.92 12.33	18.57 12.33	
2 COMBINED AT											
+	CPEM5	.391	1	FLOW TIME	82.12 12.67	80.18 12.67	78.24 12.67	76.32 12.67	74.41 12.67	72.51 12.67	
DIVERSION TO											
+	DNB	.391	1	FLOW TIME	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50	
HYDROGRAPH AT											
+	D@NOB	.391	1	FLOW TIME	42.12 12.67	40.18 12.67	38.97 13.33	39.87 13.33	39.23 13.33	38.34 13.33	
ROUTED TO											
+	RS-NOB	.391	1	FLOW TIME	7.73 18.83	7.69 18.67	7.65 18.67	7.61 18.67	7.57 18.67	7.52 18.50	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5107.23 18.83	5107.19 18.83	5107.15 18.83	5107.11 18.83	5107.07 18.67	5107.02 18.67	
2 COMBINED AT											
+	NORTH	9.661	1	FLOW TIME	36.44 14.83	36.53 14.83	36.44 14.83	36.13 14.67	35.67 14.67	34.90 14.67	
HYDROGRAPH AT											
+	M	.560	1	FLOW TIME	229.45 12.67	223.62 12.67	217.83 12.67	212.08 12.67	206.37 12.67	200.70 12.67	
ROUTED TO											
+	RES-M	.560	1	FLOW TIME	59.65 13.67	58.59 13.67	57.49 13.67	56.41 13.67	55.37 13.67	54.34 13.67	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	4.96 13.67	4.86 13.67	4.75 13.67	4.64 13.67	4.54 13.67	4.44 13.67	
HYDROGRAPH AT											
+	OFF-4	.060	1	FLOW TIME	27.36 12.50	26.64 12.50	25.94 12.50	25.24 12.50	24.54 12.50	23.85 12.50	
2 COMBINED AT											
+	M+OFF4	.620	1	FLOW TIME	67.04 13.00	65.81 13.00	64.59 13.00	63.22 13.00	61.91 13.17	60.76 13.17	
DIVERSION TO											
+	DDM	.620	1	FLOW TIME	13.41 13.00	13.16 13.00	12.92 13.00	12.64 13.00	12.38 13.17	12.15 13.17	
HYDROGRAPH AT											
+	D@M	.620	1	FLOW TIME	53.63 13.00	52.65 13.00	51.67 13.00	50.58 13.00	49.53 13.17	48.61 13.17	
HYDROGRAPH AT											
+	OFF-3	.191	1	FLOW TIME	88.81 12.67	86.71 12.67	84.62 12.67	82.55 12.67	80.48 12.67	78.43 12.67	
2 COMBINED AT											
+	OF3+4	.811	1	FLOW	131.95	128.56	125.18	121.76	118.25	114.76	



HYDROGRAPH AT											
+	EM-7	.061	1	FLOW TIME	80.64 12.33	79.43 12.33	78.21 12.33	77.00 12.33	75.79 12.33	74.58 12.33	
3 COMBINED AT											
+	CP-PP2	.226	1	FLOW TIME	159.60 12.50	156.91 12.50	154.18 12.50	151.52 12.50	148.76 12.50	146.12 12.50	
ROUTED TO											
+	PP-2	.226	1	FLOW TIME	29.33 15.17	29.23 15.17	29.13 15.17	29.03 15.00	28.86 15.00	28.67 15.00	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5177.16 15.17	5177.11 15.17	5177.06 15.17	5177.01 15.00	5176.97 15.00	5176.92 15.00	
2 COMBINED AT											
+	JCHAN2	11.283	1	FLOW TIME	93.03 12.67	91.81 12.67	90.80 14.83	90.28 14.67	89.49 14.67	88.25 14.67	
ROUTED TO											
+	CHAN-2	11.283	1	FLOW TIME	92.89 12.67	91.03 14.83	90.79 14.83	90.28 14.83	89.46 14.83	88.21 14.83	
HYDROGRAPH AT											
+	L2	.234	1	FLOW TIME	148.45 12.50	145.13 12.50	141.82 12.50	138.53 12.50	135.25 12.50	132.00 12.50	
DIVERSION TO											
+	D-L	.234	1	FLOW TIME	74.23 12.50	72.56 12.50	70.91 12.50	69.26 12.50	67.63 12.50	66.00 12.50	
HYDROGRAPH AT											
+	D@L	.234	1	FLOW TIME	74.23 12.50	72.56 12.50	70.91 12.50	69.26 12.50	67.63 12.50	66.00 12.50	
ROUTED TO											
+	RES-L	.234	1	FLOW TIME	33.83 12.83	33.12 12.83	32.41 12.83	31.71 12.83	31.02 12.83	30.33 12.83	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	3.58 12.83	3.51 12.83	3.44 12.83	3.37 12.83	3.30 12.83	3.23 12.83	
HYDROGRAPH AT											
+	L3	.018	1	FLOW TIME	24.11 12.33	23.71 12.33	23.32 12.33	22.92 12.33	22.52 12.33	22.13 12.33	
HYDROGRAPH AT											
+	VPH-1	.035	1	FLOW TIME	47.18 12.33	46.41 12.33	45.63 12.33	44.86 12.33	44.08 12.33	43.31 12.33	
2 COMBINED AT											
+	VPCP-1	.053	1	FLOW TIME	71.29 12.33	70.12 12.33	68.95 12.33	67.77 12.33	66.61 12.33	65.44 12.33	
HYDROGRAPH AT											
+	L1	.029	1	FLOW TIME	38.51 12.33	37.88 12.33	37.24 12.33	36.60 12.33	35.97 12.33	35.34 12.33	
HYDROGRAPH AT											
+	P	.031	1	FLOW TIME	55.48 12.17	54.55 12.17	53.62 12.17	52.70 12.17	51.78 12.17	50.86 12.17	
2 COMBINED AT											
+	VPCP2	.060	1	FLOW TIME	83.57 12.17	82.15 12.17	80.73 12.17	79.32 12.17	77.91 12.17	76.50 12.17	
HYDROGRAPH AT											
+	Q	.052	1	FLOW TIME	70.09 12.33	68.94 12.33	67.78 12.33	66.63 12.33	65.49 12.33	64.34 12.33	
2 COMBINED AT											
+	VPCP2A	.112	1	FLOW TIME	142.83 12.33	140.49 12.33	138.16 12.33	135.84 12.33	133.52 12.33	131.20 12.33	
DIVERSION TO											
+	VPH	.112	1	FLOW TIME	12.00 12.00	12.00 12.00	12.00 12.00	12.00 12.00	12.00 12.00	12.00 12.00	
HYDROGRAPH AT											
+	D@VPH	.112	1	FLOW TIME	130.83 12.33	128.49 12.33	126.16 12.33	123.84 12.33	121.52 12.33	119.20 12.33	
ROUTED TO											
+	VPHRP	.112	1	FLOW TIME	44.34 12.67	43.47 12.67	42.60 12.67	41.73 12.67	40.86 12.67	39.99 12.67	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5066.43 12.67	5066.35 12.67	5066.26 12.67	5066.17 12.67	5066.09 12.67	5066.00 12.67	
DIVERSION TO											
+	SOUTH	.112	1	FLOW	44.34	43.47	42.60	41.73	40.86	39.99	





3 COMBINED AT											
+	JG2&B2	.214	1	FLOW TIME	53.33 13.17	52.11 13.17	50.67 13.17	49.31 13.17	48.02 13.17	46.60 13.33	
HYDROGRAPH AT											
+	EM-8	.046	1	FLOW TIME	45.35 12.33	44.08 12.33	42.81 12.33	41.54 12.33	40.29 12.33	39.03 12.33	
HYDROGRAPH AT											
+	EM-12	.015	1	FLOW TIME	28.78 12.17	28.10 12.17	27.41 12.17	26.72 12.17	26.03 12.17	25.33 12.17	
3 COMBINED AT											
+	TODETN	.275	1	FLOW TIME	112.78 12.33	109.94 12.33	107.10 12.33	104.27 12.33	101.45 12.33	98.64 12.33	
ROUTED TO											
+	DETN	.275	1	FLOW TIME	33.01 14.67	32.32 14.67	31.61 14.67	30.91 14.67	30.23 14.67	29.51 14.83	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	3.50 14.67	3.43 14.67	3.36 14.67	3.29 14.67	3.22 14.67	3.15 14.83	
2 COMBINED AT											
+	J4B	11.957	1	FLOW TIME	157.90 13.00	154.86 13.00	152.30 13.00	149.32 13.00	146.17 13.00	143.79 13.17	
ROUTED TO											
+	RCH-4C	11.957	1	FLOW TIME	157.21 13.17	154.46 13.17	151.75 13.17	148.81 13.17	145.86 13.17	143.49 13.17	
HYDROGRAPH AT											
+	A3	.055	1	FLOW TIME	81.57 12.33	80.33 12.33	79.10 12.33	77.86 12.33	76.63 12.33	75.40 12.33	
HYDROGRAPH AT											
+	A3A	.007	1	FLOW TIME	10.21 12.17	10.03 12.17	9.85 12.17	9.68 12.17	9.50 12.17	9.32 12.17	
2 COMBINED AT											
+	COMBA3	.062	1	FLOW TIME	90.04 12.33	88.67 12.33	87.29 12.33	85.92 12.33	84.55 12.33	83.18 12.33	
ROUTED TO											
+	RES-6	.062	1	FLOW TIME	34.25 12.67	33.89 12.67	33.54 12.67	33.19 12.67	32.83 12.67	32.48 12.67	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5078.85 12.67	5078.78 12.67	5078.71 12.67	5078.64 12.67	5078.57 12.67	5078.50 12.67	
HYDROGRAPH AT											
+	A3B	.026	1	FLOW TIME	35.10 12.33	34.53 12.33	33.95 12.33	33.38 12.33	32.81 12.33	32.24 12.33	
DIVERSION TO											
+	PARK	.026	1	FLOW TIME	8.78 12.33	8.63 12.33	8.49 12.33	8.35 12.33	8.20 12.33	8.06 12.33	
HYDROGRAPH AT											
+	D-PARK	.026	1	FLOW TIME	26.33 12.33	25.89 12.33	25.46 12.33	25.04 12.33	24.61 12.33	24.18 12.33	
ROUTED TO											
+	RES-5	.026	1	FLOW TIME	15.37 12.50	15.10 12.50	14.83 12.50	14.57 12.50	14.30 12.50	14.02 12.50	
				** PEAK STAGES IN FEET **							
			1	STAGE TIME	5071.14 12.50	5071.11 12.50	5071.08 12.50	5071.06 12.50	5071.03 12.50	5071.00 12.50	
ROUTED TO											
+	R-9	.026	1	FLOW TIME	14.98 12.67	14.51 12.67	14.32 12.67	14.18 12.67	13.92 12.67	13.63 12.67	
HYDROGRAPH AT											
+	A13A	.006	1	FLOW TIME	6.66 12.33	6.53 12.33	6.41 12.33	6.29 12.33	6.17 12.33	6.04 12.33	
HYDROGRAPH AT											
+	A13B	.040	1	FLOW TIME	46.30 12.33	45.46 12.33	44.62 12.33	43.78 12.33	42.95 12.33	42.12 12.33	
2 COMBINED AT											
+	COMA13	.046	1	FLOW TIME	52.96 12.33	51.99 12.33	51.03 12.33	50.07 12.33	49.11 12.33	48.16 12.33	
HYDROGRAPH AT											
+	A12A	.015	1	FLOW TIME	18.64 12.17	18.30 12.17	17.97 12.17	17.63 12.17	17.30 12.17	16.97 12.17	
HYDROGRAPH AT											
+	A12	.020	1	FLOW	27.30	26.79	26.28	25.77	25.26	24.76	



ROUTED TO											
+	EXDT1A	.005	1	FLOW TIME	5.02 12.33	5.00 12.33	4.97 12.33	4.95 12.33	4.92 12.33	4.89 12.33	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	5105.30 12.33	5105.27 12.33	5105.24 12.33	5105.21 12.33	5105.19 12.33	5105.16 12.33	
2 COMBINED AT											
+	J-6	.055	1	FLOW TIME	33.01 12.50	32.27 12.50	31.59 12.50	31.16 12.50	30.35 12.50	29.47 12.50	
HYDROGRAPH AT											
+	CSR-6	.025	1	FLOW TIME	35.04 12.33	34.47 12.33	33.91 12.33	33.36 12.33	32.80 12.33	32.24 12.33	
2 COMBINED AT											
+	CPXD1	.080	1	FLOW TIME	59.86 12.33	58.63 12.33	57.41 12.33	55.94 12.33	54.72 12.33	53.52 12.33	
ROUTED TO											
+	EXDT1	.080	1	FLOW TIME	20.24 12.83	20.03 12.83	19.82 12.83	19.61 12.83	19.40 12.83	19.20 12.83	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	5106.94 12.83	5106.82 12.83	5106.69 12.83	5106.56 12.83	5106.44 12.83	5106.32 12.83	
HYDROGRAPH AT											
+	A1	.090	1	FLOW TIME	124.95 12.33	122.93 12.33	120.92 12.33	118.92 12.33	116.92 12.33	114.92 12.33	
2 COMBINED AT											
+	J8	.170	1	FLOW TIME	139.01 12.33	136.74 12.33	134.49 12.33	132.17 12.33	129.93 12.33	127.69 12.33	
ROUTED TO											
+	R21	.170	1	FLOW TIME	119.58 12.50	117.72 12.50	115.86 12.50	113.97 12.50	112.12 12.50	110.28 12.50	
2 COMBINED AT											
+	JRES2	.266	1	FLOW TIME	173.95 12.50	171.73 12.50	169.76 12.50	166.93 12.50	164.17 12.50	162.62 12.50	
ROUTED TO											
+	RES2	.266	1	FLOW TIME	15.37 16.83	15.23 16.67	15.09 16.67	14.95 16.67	14.81 16.67	14.67 16.50	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	5070.98 16.83	5070.90 16.83	5070.83 16.83	5070.75 16.67	5070.67 16.67	5070.60 16.67	
ROUTED TO											
+	R22	.266	1	FLOW TIME	15.37 16.83	15.23 16.83	15.09 16.83	14.95 16.67	14.81 16.67	14.67 16.67	
HYDROGRAPH AT											
+	CSR-4	.030	1	FLOW TIME	41.96 12.17	41.21 12.17	40.47 12.17	39.72 12.17	38.98 12.17	38.24 12.17	
ROUTED TO											
+	EXDET2	.030	1	FLOW TIME	9.79 12.67	9.75 12.67	9.71 12.67	9.67 12.67	9.63 12.67	9.59 12.67	
					** PEAK STAGES IN FEET **						
			1	STAGE TIME	5096.59 12.67	5096.51 12.67	5096.42 12.67	5096.34 12.67	5096.26 12.67	5096.18 12.67	
HYDROGRAPH AT											
+	CSR-3	.005	1	FLOW TIME	9.54 12.17	9.39 12.17	9.24 12.17	9.10 12.17	8.95 12.17	8.80 12.17	
2 COMBINED AT											
+	J11	.035	1	FLOW TIME	15.89 12.33	15.68 12.33	15.48 12.33	15.28 12.33	15.07 12.33	14.87 12.33	
ROUTED TO											
+	DITCH	.035	1	FLOW TIME	17.59 12.50	17.34 12.50	17.08 12.50	16.82 12.50	16.57 12.50	16.31 12.50	
HYDROGRAPH AT											
+	A2	.050	1	FLOW TIME	64.81 12.17	63.67 12.17	62.53 12.17	61.40 12.17	60.27 12.17	59.15 12.17	
3 COMBINED AT											
+	JRES15	.352	1	FLOW TIME	80.64 12.33	79.25 12.33	77.87 12.33	76.51 12.33	75.12 12.33	73.77 12.33	
ROUTED TO											
+	RES15	.352	1	FLOW TIME	10.22 29.33	10.12 29.17	10.02 29.17	9.92 29.00	9.82 29.00	9.72 28.83	
					** PEAK STAGES IN FEET **						
			1	STAGE	5062.98	5062.93	5062.88	5062.83	5062.78	5062.73	





**PROPOSED CONDITIONS THROUGH FULL BUILD OUT OF WOODLAND VILLAGE**

VPH Proposed  
 100 Year event  
 Base Model Woodland Village  
 Full build out

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 AND FEB 2010 *
* VERSION 4.1R *
* RGMHEC2000 WWW.HEC-1.COM *
* RUN DATE 07MAR21 TIME 17:57:35 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

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HEC-1 INPUT
PAGE 1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DDIAGRAM
1 ID 100 yr 24 hr event
2 ID WOODLANDVILLAGE PHASE 23 MODEL
3 ID FILE NAME VPH-FBO.DAT
4 ID USING BALANCED STORM
5 ID FULL BUILD OUT USES 3 BASINS IN NORTH
*
* DARF AREA (SQ. MI.)
* 1.00 0 - 2
* 0.99 2.1 - 8
* 0.98 8.1 - 16
* 0.97 16.1 - 29
* 0.96 29.1 - 43
* 0.95 43.1 - 63
* 0.94 63.1 - 98
6 IT 10 800
7 IO 5 0
8 JR PREC 1.0 .99 .98 .97
9 KK A
10 BA 0.72
11 PH 1
12 LS 1.7 54 .68 1.24 2.06 2.32 2.52 2.94 3.76 4.59
13 UD .62
14 KK B
15 BA 1.78
16 LS 1.63 55
17 UD 1.1
18 KK D@A&B
19 HC 2
20 KK D-A&B
21 DT D-AB
22 DI 0 10 50 100 500
23 DQ 0 5 25 50 250
24 KK RCH-1
25 KM ROUTE A&B TO J1@AB
26 RD 10200 .04 .12 TRAP 3 1
27 KK C
28 BA 1.26
29 LS 1.7 54
30 UD .82
31 KK J1@A&B
32 HC 2
  
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HEC-1 INPUT
PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

33 KK RCH-2
34 RD 3500 .06 .12 TRAP 10 2.5
  
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35	KK	D					
36	BA	1.0					
37	LS	1.57	50				
38	UD	.63					
39	KK	J2ABCD					
40	HC	2					
41	KK	DJ2					
42	DT	J2					
43	DI	0	10	50	100	500	
44	DQ	0	5	25	50	250	
45	KK	E					
46	BA	.615					
47	LS	1.45	58				
48	UD	.68					
49	KK	D@E					
50	DT	DE					
51	DI	0	10	50	100	500	
52	DQ	0	8	40	80	400	
53	KK	F					
54	BA	0.815					
55	LS	1.51	57				
56	UD	1					
57	KK	D@F					
58	DT	DF					
59	DI	0	10	50	100	500	
60	DQ	0	8	40	80	400	
61	KK	J3-1					
62	HC	2					
63	KK	J					
64	BA	1.14					
65	LU	4	0.1				
66	UD	.67					
67	KK	J3-2					
68	HC	2					
69	KK	G					
70	BA	0.81					
71	LS	1.03	66				
72	UD	.93					

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

73	KK	D@G					
74	DT	DDG					
75	DI	0	10	50	100	500	
76	DQ	0	8	40	80	400	
77	KK	H					
78	BA	0.74					
79	LS	1.12	64				
80	UD	.63					
81	KK	D@H					
82	DT	DDH					
83	DI	0	10	50	100	500	
84	DQ	0	8	40	80	400	
85	KK	J3					
86	HC	4					
87	KK	RCH-3					
88	RD	4000	.04	.05	TRAP	10	1
89	KK	D@J3					
90	DT	D-J3					
91	DI	0	10	50	100	250	500
92	DQ	0	5	25	50	125	250
93	KK	IEAST					
94	BA	.18					
95	LS		64				
96	UD	.22					
97	KK	D@IE					
98	DT	DDG					
99	DI	0	10	50	100	500	
100	DQ	0	8	40	80	400	
101	KK	OEAST					
102	BA	.21					
103	LU	4	.1				

104 KK CP2  
 105 HC 2

106 KK CPO+J3  
 107 HC 2

108 KK D@NOA  
 109 DT DNA  
 110 DI 0 40 60 100 500 1000  
 111 DQ 0 0 40 40 40 40

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

112 KK NP-A NORTH RESERVOIR A  
 113 KM 36" OUTLET  
 114 RS 1 STOR 0  
 115 SA 0 .17 .91 2.24 3.55 4.94 5.09 5.24  
 116 SE 5101.5 5102 5103 5104 5105 5106 5107 5108  
 117 SQ 0 6 19 35 50 60 72 78  
 118 SE 5101.5 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5

119 KK K-1  
 120 BA .077  
 121 LS 70  
 122 UD .31

123 KK D@K1  
 124 DT DDK1  
 125 DI 0 10 50 100 500  
 126 DQ 0 5 25 50 250

127 KK K-2  
 128 BA .105  
 129 LS 70  
 130 UD .30

131 KK D@K2  
 132 DT DDK2  
 133 DI 0 10 50 100 500  
 134 DQ 0 5 25 50 250

135 KK K-3  
 136 BA .033  
 137 LS 70  
 138 UD .22

139 KK D@K3  
 140 DT DDK3  
 141 DI 0 10 50 100 500  
 142 DQ 0 5 25 50 250

143 KK CP-K  
 144 HC 3

145 KK EM-5  
 146 BA .03  
 147 LS 88  
 148 UD .19

149 KK DP-EM5 POND TO MITAGATE EM-5 DEVELOPMENT  
 150 RS 1 STOR 0  
 151 SA .47 .74  
 152 SE 23.17 28.17  
 153 SQ 0 4.1 12.5 20 26 29  
 154 SE 23.17 24.17 25.17 26.17 27.17 28.17

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

155 KK CPEM5  
 156 HC 2

157 KK D@NOB  
 158 DT DNB  
 159 DI 0 40 60 100 500 1000  
 160 DQ 0 0 40 40 40 40

161 KK NP-B NORTH RESERVOIR B  
 162 KM 12" OUTLET  
 163 RS 1 STOR 0  
 164 SA 0 0.02 0.16 0.52 1.73 3.30 5.24 5.38 5.52  
 165 SE 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5 5109.5  
 166 SQ 0 2.2 4.5 5.6 7 8 9 10  
 167 SE 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5 5109.5 11

168 KK NORTH  
 169 HC 2

170 KK M  
 171 BA 0.56  
 172 LS 1.17 63





241	SA	0	.22	.82	2.4	3.85	4.54	5.03	5.31		
242	SE	5094	5095	5096	5097	5098	5099	5100	5101		
243	SQ	0	5.5	16	28	38	45	50	57	62	68
244	SE	5094	5095	5096	5097	5098	5099	5100	5101		

245 KK CP-NOR COMBINE 3 NORTH DET BASINS  
 246 HC 2

247	KK	IWEST									
248	BA	.35									
249	LS		64								
250	UD	.37									

251	KK	D@IW									
252	DT	DDIW									
253	DI	0	10	50	100	500					
254	DQ	0	8	40	80	400					

255	KK	OWEST									
256	BA	.18									
257	LU	4	.1								

258 KK CP1  
 259 HC 2

260 KK NOR+I COMBINE FLOW FROM 3 DET BASINS & OFFSITE WATERSHED I  
 261 HC 2

262	KK	EM-3A									
263	BA	.01									
264	LS		89								
265	UD	.13									

266	KK	EM-4									
267	BA	.1									
268	LS		84								
269	UD	.25									

270 KK CEMB1  
 271 HC 2

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

272	KK	EMB-1									
273	RS	1	STOR	0							
274	SA	1.5	1.54	1.6	1.68	1.79	1.95	2.15			
275	SE	5078	5079.1	5079.69	5080.25	5080.95	5081.86	5082.96			
276	SQ	0	8	26	40	52	60				
277	SE	5078	5079	5080	5081	5082	5083				

278	KK	RHEMB1	REACH	EMB-1							
279	RD	759	.0066	.04	TRAP	3	3				

280	KK	EM-6									
281	BA	.078									
282	LS		84								
283	UD	.25									

284 KK EM-7  
 285 KM WILL NOT BE DEVELOPED,  
 286 BA .034  
 287 LS 61  
 288 UD .21

289 KK CP-PP2 NORTH OF BRIAR ROAD  
 290 HC 3

291	KK	PP-2									
292	KM	OUTLET (1) 12"									
293	RS	1	STOR	0							
294	SA	0	.22	.82	2.4	3.85	4.54	5.03	5.31		
295	SE	5094	5095	5096	5097	5098	5099	5100	5101		
296	SQ	0	2.2	4.5	5.6	7	8	9	10	11	
297	SE	5094	5095	5096	5097	5098	5099	5100	5101	5101.5	

298 KK JCHAN2  
 299 HC 2

300	KK	CHAN-2									
301	RD	1130	.005	.04	TRAP	6	3				

302	KK	L2									
303	BA	.234									
304	LS	1.03	66								
305	UD	.33									

306	KK	D@L									
307	DT	D-L									
308	DI	0	10	50	100	500					
309	DQ	0	5	25	50	250					

310 KK RES-L

311	RS	1	STOR	0										
312	SA	0.6	0.64	0.69	0.76	0.86	1							
313	SE	0	1.69	2.25	2.95	3.86	4.96							
314	SQ	0	5.5	16	28	38	45							
315	SE	0	1	2	3	4	5							

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

316	KK	L3	PART OF L2 DRAINING TO VILLAGE PARKWAY HOMES											
317	BA	.018												
318	LS		77											
319	UD	0.2												
320	KK	VPH-1	VILL. PKWY HOMES NORTH PORTION											
321	BA	0.035												
322	LS		77											
323	UD	.19												
324	KK	VPCP-1												
325	HC	2												
326	KK	VPNEPD	RETENTION/DETENTION POND											
327	KM	18-IN RCP	OUTLET@ 60 FT											
328	RS	1	STOR	0										
329	SA	.34	.73	.94	1.13									
330	SE	58	62	64	66									
331	SQ	0	0	4	13	20	26	30	35					
332	SE	58	60	61	62	63	64	65	66					
333	KK	VPCP1A	COMBINE OUTFLOW FROM PVH NE POND WITH MAIN CHANNEL											
334	HC	3												
335	KK	RECH4A												
336	RD	395	.001	.04		TRAP	8	3						
337	KK	RCH4B												
338	RD	665	.001	.04		TRAP	10	3						
339	KK	WV-20A	PART OF WV-20 GOING SOUTH											
340	BA	.013												
341	LS		61											
342	UD	.15												
343	KK	HASKEL	12" RCP OUTLET											
344	RS	1	STOR	0										
345	SA	0	.47	.55	.60	.65								
346	SE	5194.5	5195	5196	5197	5198								
347	SQ	0	2.4	4.7	6	7.5								
348	SE	5194.5	5195.5	5196.5	5197.5	5198.5								
349	KK	EM-2												
350	BA	.0621												
351	LS		78											
352	UD	.32												
353	KK	20A+2	COMBINE W VILLAGE 20A POND WITH EM-2											
354	KM	FLOW GOES	INTO POND EMG-1											
355	HC	2												

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

356	KK	EMG-1	DETENTION POND EMG-1											
357	RS	1	STOR	0										
358	SA	0.8	0.83	.87	.93	1.02	1.13	1.29						
359	SE	86	87.1	87.69	88.25	88.95	89.86	90.96						
360	SQ	0	8	26	40	52	60							
361	SE	86	87	88	89	90	91							
362	KK	EMG-1												
363	RD	1630	.01	.04		TRAP	3	3						
364	KK	EMTC												
365	BA	.053												
366	LS	1.5	79											
367	UD	.27												
368	KK	EM-10												
369	BA	.053												
370	LS	1.5	72											
371	UD	.32												
372	KK	JEM02												
373	HC	3												
374	KK	EMO-2												
375	RS	1	STOR	0										
376	SA	1.2	1.25	1.26	1.27	1.29	1.3	1.32	1.34	1.39				
377	SE	67	68.49	68.91	69.31	69.72	70.21	70.69	71.31	72.8				
378	SQ	0	11	32	56	76	90	100						
379	SE	67	68	69	70	71	72	73						

380	KK	EMOc								
381	RD	615	.003	.04		TRAP	0	3		
382	KK	EM-11								
383	BA	.012								
384	LS	1.5	86							
385	UD	.13								
386	KK	EM-9								
387	BA	.021								
388	LS	1.5	86							
389	UD	.13								
390	KK	JG2&B2								
391	HC	3								
392	KK	EM-8								
393	BA	.046								
394	LS	1.5	82							
395	UD	.22								

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

396	KK	EM-12								
397	BA	.015								
398	LS	1.5	93							
399	UD	.12								
400	KK	TODETN								
401	HC	3								
402	KK	DETN								
403	RS	1	STOR	0						
404	SA	2.25	2.31	2.4	2.5	2.63	2.78	2.96	3.18	3.48
405	SE	0	1.49	1.91	2.31	2.72	3.21	3.69	4.31	5.8
406	SQ	0	5.5	16	28	38	45	50		
407	SE	0	1	2	3	4	5	6		
408	KK	J4B								
409	HC	2								
410	KK	RCH-4C								
411	RD	300	.001	.04		TRAP	12	3		
412	KK	A3								
413	BA	.055								
414	LS		80							
415	UD	.16								
416	KK	A3A								
417	BA	.007								
418	LS		76							
419	UD	.13								
420	KK	COMBA3								
421	HC	2								
422	KK	RES-6								
423	RS	1	STOR	0						
424	SA	0.24	0.5	0.54	0.61	0.67	0.69			
425	SE	5074	5075	5076	5077	5078	5079			
426	SQ	0	4.3	14	24	30	35			
427	KK	A3B								
428	BA	.026								
429	LS		77							
430	UD	.17								
431	KK	D-PARK								
432	DT	PARK								
433	DI	0	20	100	500	1000				
434	DQ	0	5	25	125	250				

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

435	KK	RES-5								
436	RS	1	STOR	0						
437	SA	0.25	0.28	0.32	0.35	0.39	0.43	0.46	0.5	0.59
438	SE	5069	5070	5071	5072	5073	5074	5075	5076	5077
439	SQ	0	4.3	14	24	30	35.4	40	44	44
440	KK	R-9	ROUTING							
441	RD	1000	.02	.05		TRAP	15	1		
442	KK	A13A								
443	BA	.006								
444	LS		72							
445	UD	.17								



446	KK	A13B							
447	BA	.04							
448	LS		73						
449	UD	.18							
450	KK	COMA13							
451	HC	2							
452	KK	A12A							
453	BA	.015							
454	LS		75						
455	UD	.15							
456	KK	A12							
457	BA	.02							
458	LS		73						
459	UD	.12							
460	KK	COMA12							
461	HC	2							
462	KK	JRES3							
463	HC	3							
464	KK	RES-3							
465	RS	1	STOR	0					
466	SA	1	1.2	1.35	1.55	1.8			
467	SE	5059	5060	5061	5062	5063			
468	SQ	0	0	7.3	53.15	116.35			
469	KK	A13							
470	BA	.05							
471	LS		74						
472	UD	.17							

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

473	KK	A12B																	
474	BA	.03																	
475	LS		88																
476	UD	.12																	
477	KK	JRES1																	
478	HC	3																	
479	KK	RES-1																	
480	RS	1	STOR	0															
481	SA	.0006	.0812	.2929	.6341	1.0634	1.5306	2.0022	2.4899	3.0079	3.5568								
482	SA	4.1272	5.1068	5.5454	5.8719														
483	SE	5057	5057.2	5057.4	5057.6	5057.8	5058	5058.2	5058.4	5058.6	5058.8								
484	SE	5059	5060	5061	5062														
485	SQ	0	0	0	0	0	0	0	1.2	2.4	3.6								
486	SQ	4.8	14	20	20														
487	KK	ABMSR																	
488	HC	3																	
489	KK	OFF-1																	
490	BA	.0226																	
491	LS		63																
492	UD	.22																	
493	KK	R8																	
494	RD	2000	.054	.05		TRAP	15	1											
495	KK	A5																	
496	BA	.06																	
497	LS		84																
498	UD	.17																	
499	KK	CSR-7																	
500	BA	.014																	
501	LS		75																
502	UD	.18																	
503	KK	J-1																	
504	HC	3																	
505	KK	EXDET																	
506	RS	1	STOR	0															
507	SA	0.27	0.28	0.37	0.47	0.52	0.52	0.52											
508	SE	5118	5119	5121	5125	5125.25	5125.5	5126											
509	SQ	0	0	9.8	23	99.5	238	631.1											
510	KK	DIV																	
511	DT	D-DIV																	
512	DI	0	10	100	1000														
513	DQ	0	5	50	500														

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10



583	LS		76						
584	UD	.15							
585	KK	JRES15							
586	HC	3							
587	KK	RES15							
588	RS	1	STOR	0					
589	SA	3.55	3.71	3.85	4.04	4.36	4.69	4.94	
590	SE	5058.5	5059	5059.5	5060	5061	5062	5064	
591	SQ	0	0	0	.6	4.7	8.3	12.2	

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

592	KK	R23							
593	RD	2600	.02	.05		TRAP	5	1	
594	KK	RPE							
595	BA	0.12							
596	LS		72						
597	UD	.28							
598	KK	ACS-1							
599	HC	2							
600	KK	VPCP3							
601	HC	2							
602	KK	L1							
603	BA	.029							
604	LS		77						
605	UD	.21							
606	KK	P							
607	BA	.031							
608	LS		77						
609	UD	0.1							
610	KK	VPCP2							
611	HC	2							
612	KK	Q							
613	BA	.052							
614	LS		77						
615	UD	.19							
616	KK	VPCP2A							
617	HC	2							
FLOW ENTERING RETENTION/DETENTION POND									
618	KK	D@VPH							
619	DT	VPH							
620	DI	0	10	25	50	100	140	150	155
621	DQ	0	0	12	12	12	12	12	12
INFILTRATION @ VP RETENTION POND									
622	KK	VPHRPRETENTION/DETENTION POND @ VILLAGE PKWY HOMES							
623	KM	30-IN RCP OUTLET@ 61.5 FT							
624	RS	1	STOR	0					
625	SA	.278	.607	.848	.972	1.013			
626	SE	5060	5062	5064	5066	5067			
627	SQ	0	0	4.5	16	29	35	40	50
628	SE	5060	5061.5	5062.5	5063.5	5064.5	5065.5	5066.	5067
629	KK	VPH2							
630	BA	0.01							
631	LS		77						
632	UD	0.15							

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

633	KK	VPCP3							
634	HC	2							
COMBINE FLOWS GOING TO RET POND									
635	KK	VPH-3							
636	BA	.01							
637	LS		77						
638	UD	0.15							
639	KK	VPH-4							
640	BA	.011							
641	LS		77						
642	UD	0.15							
643	KK	VPH-5							
644	BA	.005							
645	LS		77						
646	UD	.13							
647	KK	VPCP-4							
648	HC	4							
COMBINE VPH3, 4, AND 5									

649	KK	VPDICH	VILLAGE PKWY HOMES DETENTION DITCH					
650	KM	OUTLETIS 30"	RCP @ ELEV 5058.15					
651	RS	1	STOR	0				
652	SA	.0001	0.13	0.42	0.74	1		
653	SE	5058.1	5059.5	5060	5062	5063.5		
654	SQ	0	5	16	29	35	44	
655	SE	5058.1	5059.1	5060.1	5061.1	5062.1	5063.1 5063.5	

656	KK	VP5CP5TOTAL FLOW LEAVING VILLAGE PKWY HOMES
657	HC	2

658	KK	Q2
659	BA	.013
660	LS	77
661	UD	.16

662	KK	VP6CP6COMBINED FLOW IN MUD SPRINGS CHANNEL
663	HC	2

664	KK	PVE-1
665	BA	.0128
666	LS	76
667	UD	.13

668	KK	ABCDSPP ABOVE COLD SPRINGS ROAD
669	HC	2

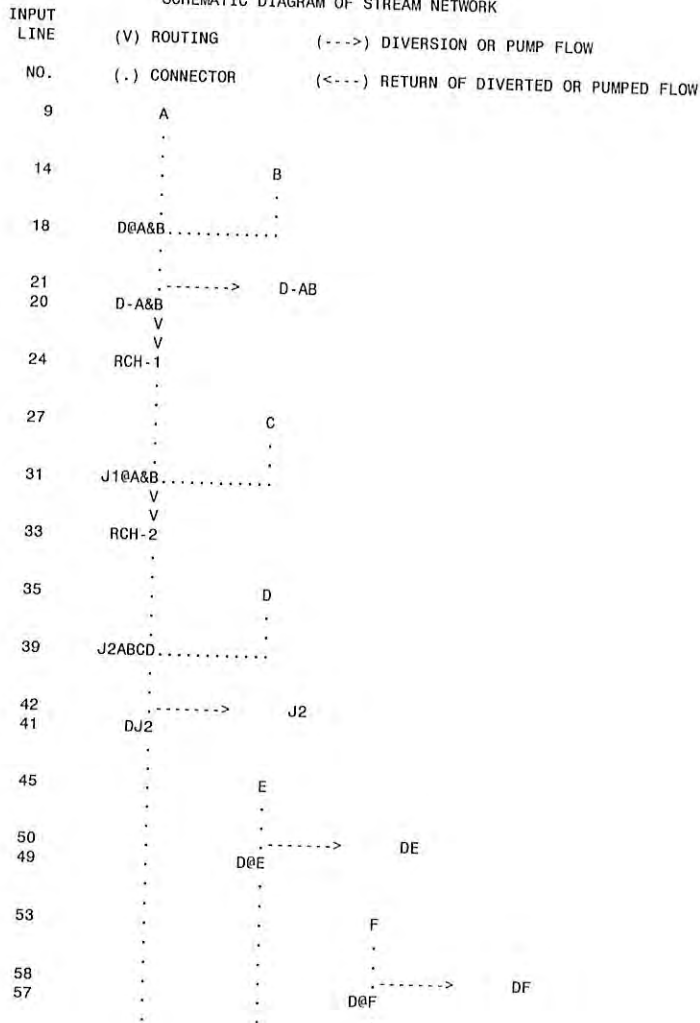
670	KK	PVE-2
671	BA	.011
672	LS	76
673	UD	.13

HEC-1 INPUT

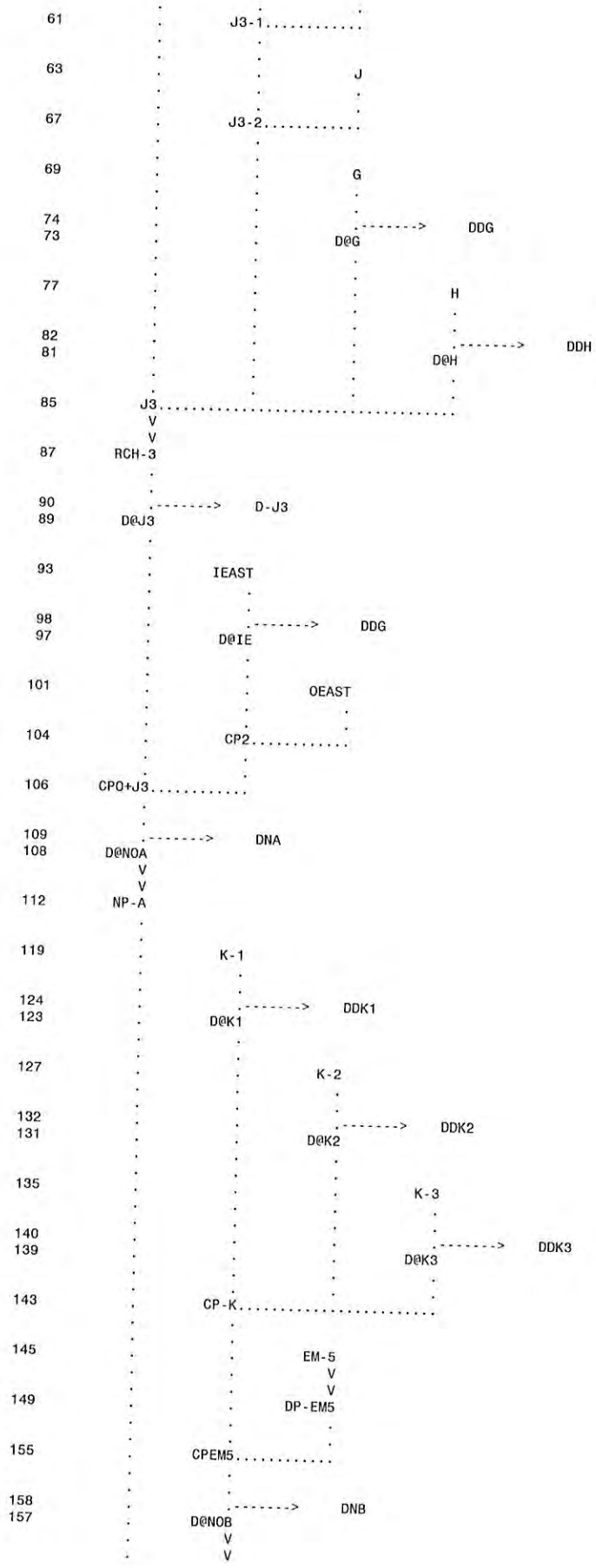
1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

674	KK	BLCSRD	BELOW COLD SPRINGS ROAD
675	HC	2	
676	ZZ		

SCHEMATIC DIAGRAM OF STREAM NETWORK





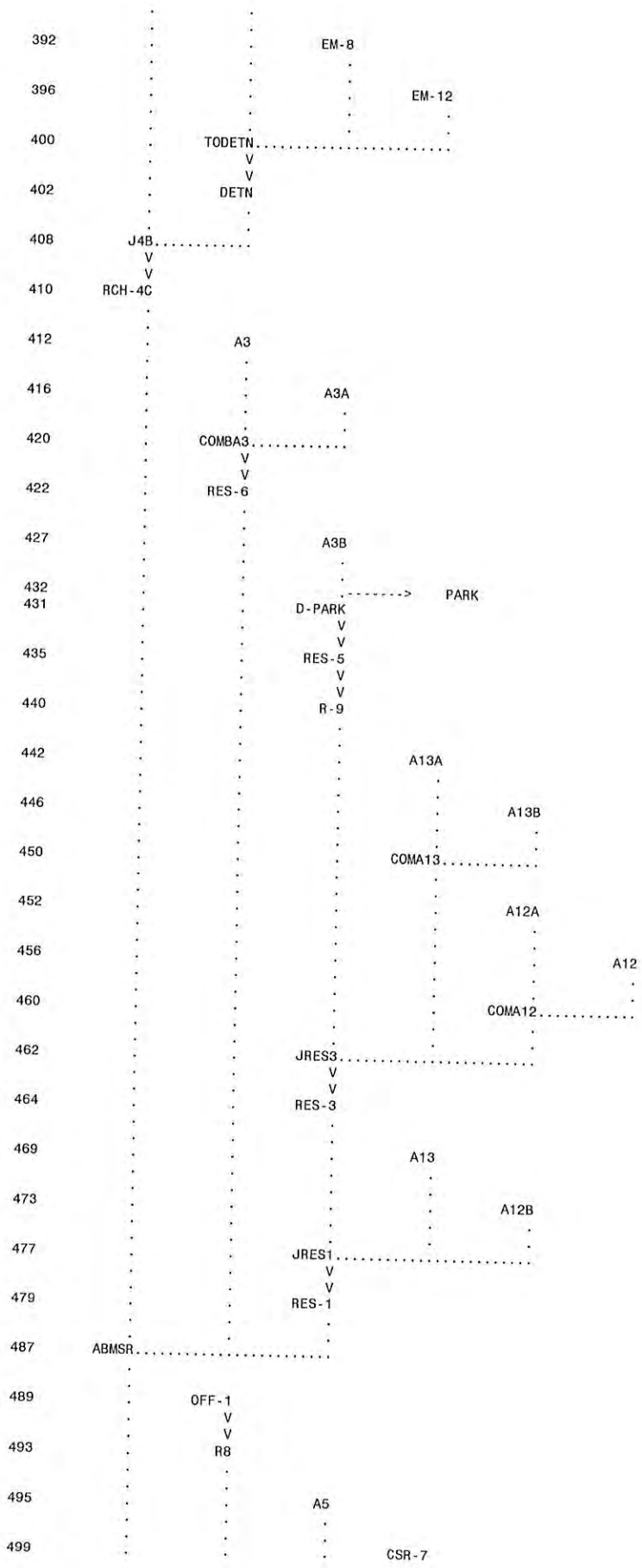


161	.	NP-B	.
168	NORTH	.....	.
170	.	M	.
	.	V	.
	.	V	.
174	.	RES-M	.
180	.	.	OFF-4
184	.	M+OFF4	.....
187	.	.	-----> DDM
186	.	D@M	.
190	.	.	OFF-3
194	.	OF3+4	.....
196	.	.	EM-1
200	.	JEM1+	.....
203	.	.	TRI
207	.	GPPP1	.....
	.	V	.
	.	V	.
209	.	PP-1	.
	.	V	.
	.	V	.
220	.	RCHPP1	.
222	.	.	EM-3
226	.	JCH1	.....
228	.	.	WV20-B
232	.	JCH2	.....
235	.	.	-----> DNC
234	.	D@NOC	.
	.	V	.
	.	V	.
238	.	NP-C	.
245	CP-NOR	.....	.
247	.	IWEST	.
252	.	.	-----> DDIW
251	.	D@IW	.
255	.	.	OWEST
258	.	CP1	.....
260	NOR+I	.....	.
262	.	EM-3A	.
266	.	.	EM-4
270	.	CEMB1	.....
	.	V	.
	.	V	.
272	.	EMB-1	.

```

      V
      V
278  RHEMB1
      V
280  EM-6
      V
284  EM-7
      V
289  CP-PP2 .....
      V
291  PP-2
      V
298  JCHAN2 .....
      V
300  CHAN-2
      V
302  L2
      V
307  D-L
306  D=L ----->
      V
310  RES-L
      V
316  L3
      V
320  VPH-1
      V
324  VPCP-1 .....
      V
326  VPNEPD
      V
333  VPCP1A .....
      V
335  RECH4A
      V
337  RCH4B
      V
339  WV-20A
      V
343  HASKEL
      V
349  EM-2
      V
353  20A+2 .....
      V
356  EMG-1
      V
362  EMG-1
      V
364  EMTC
      V
368  EM-10
      V
372  JEMO2 .....
      V
374  EMO-2
      V
380  EMOc
      V
382  EM-11
      V
386  EM-9
      V
390  JG2&B2 .....

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503      . . . . . J-1 .....
      . . . . . V
      . . . . . V
505      . . . . . EXDET
      . . . . .
511      . . . . . -----> D-DIV
510      . . . . . DIV
      . . . . . V
      . . . . . V
514      . . . . . REXDET
      . . . . .
516      . . . . . OFF-2
      . . . . . V
      . . . . . V
520      . . . . . R-19
      . . . . .
522      . . . . . CSR-6A
      . . . . . V
      . . . . . V
526      . . . . . EXDT1A
      . . . . .
531      . . . . . J-6 .....
      . . . . .
533      . . . . . CSR-6
      . . . . .
537      . . . . . CPXDT1 .....
      . . . . . V
      . . . . . V
539      . . . . . EXDT1
      . . . . .
544      . . . . . A1
      . . . . .
548      . . . . . J8 .....
      . . . . . V
      . . . . . V
550      . . . . . R21
      . . . . .
552      . . . . . JRES2 .....
      . . . . . V
      . . . . . V
554      . . . . . RES2
      . . . . . V
      . . . . . V
562      . . . . . R22
      . . . . .
564      . . . . . CSR-4
      . . . . . V
      . . . . . V
568      . . . . . EXDET2
      . . . . .
573      . . . . . CSR-3
      . . . . .
577      . . . . . J11 .....
      . . . . . V
      . . . . . V
579      . . . . . DITCH
      . . . . .
581      . . . . . A2
      . . . . .
585      . . . . . JRES15 .....
      . . . . . V
      . . . . . V
587      . . . . . RES15
      . . . . . V
      . . . . . V
592      . . . . . R23
      . . . . .
594      . . . . . RPE
      . . . . .
598      . . . . . ACS-1 .....
      . . . . .
600      . . . . . VPCP3 .....
      . . . . .
602      . . . . . L1

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606 . . . . . P
610 . . . . . VPCP2.....
612 . . . . . Q
616 . . . . . VPCP2A.....
619 . . . . . -----> VPH
618 . . . . . D@VPH
        . . . . . V
        . . . . . V
622 . . . . . VPHRP
629 . . . . . VPH2
633 . . . . . VPCP3.....
635 . . . . . VPH-3
639 . . . . . VPH-4
643 . . . . . VPH-5
647 . . . . . VPCP-4.....
        . . . . . V
        . . . . . V
649 . . . . . VPDICH
656 . . . . . VPCP5.....
658 . . . . . Q2
662 . . . . . VPCP6.....
664 . . . . . PVE-1
668 . . . . . ABCDSP.....
670 . . . . . PVE-2
674 . . . . . BLCSRD.....

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(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 AND FEB 2010 *
* VERSION 4.1R *
* RGMHEC2000 WWW.HEC-1.COM *
* RUN DATE 07MAR21 TIME 17:57:35 *
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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100 yr 24 hr event
WOODLANDVILLAGE PHASE 23 MODEL
FILE NAME VPH-FBO.DAT
USING BALANCED STORM
FULL BUILD OUT USES 3 BASINS IN NORTH

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7 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

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IT HYDROGRAPH TIME DATA
NMIN 10 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 800 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 6 0 ENDING DATE

```

NDTIME 1310 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .17 HOURS  
 TOTAL TIME BASE 133.17 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE- FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 1.00 .99 .98 .97

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION			
					RATIO 1 1.00	RATIO 2 .99	RATIO 3 .98	RATIO 4 .97
HYDROGRAPH AT +	A	.720	1	FLOW TIME	121.51 12.83	117.04 12.83	112.64 12.83	108.31 12.83
HYDROGRAPH AT +	B	1.780	1	FLOW TIME	220.78 13.33	213.16 13.33	205.63 13.33	198.22 13.33
2 COMBINED AT +	D@A&B	2.500	1	FLOW TIME	305.45 13.17	294.83 13.17	284.36 13.17	274.03 13.17
DIVERSION TO +	D-AB	2.500	1	FLOW TIME	152.72 13.17	147.41 13.17	142.18 13.17	137.02 13.17
HYDROGRAPH AT +	D-A&B	2.500	1	FLOW TIME	152.72 13.17	147.41 13.17	142.18 13.17	137.02 13.17
ROUTED TO +	RCH-1	2.500	1	FLOW TIME	154.00 13.67	148.35 13.67	142.60 13.67	134.73 13.67
HYDROGRAPH AT +	C	1.260	1	FLOW TIME	173.70 13.00	167.28 13.00	160.97 13.00	154.75 13.00
2 COMBINED AT +	J1@A&B	3.760	1	FLOW TIME	292.49 13.33	277.67 13.33	264.27 13.50	253.43 13.50
ROUTED TO +	RCH-2	3.760	1	FLOW TIME	289.48 13.50	275.52 13.50	261.29 13.67	250.68 13.67
HYDROGRAPH AT +	D	1.000	1	FLOW TIME	166.69 12.83	160.98 12.83	155.35 12.83	149.80 12.83
2 COMBINED AT +	J2ABCD	4.760	1	FLOW TIME	375.21 13.50	358.74 13.50	340.56 13.50	321.28 13.50
DIVERSION TO +	J2	4.760	1	FLOW TIME	187.60 13.50	179.37 13.50	170.28 13.50	160.64 13.50
HYDROGRAPH AT +	DJ2	4.760	1	FLOW TIME	187.60 13.50	179.37 13.50	170.28 13.50	160.64 13.50
HYDROGRAPH AT +	E	.615	1	FLOW TIME	142.56 12.83	138.11 12.83	133.71 12.83	129.35 12.83
DIVERSION TO +	DE	.615	1	FLOW TIME	114.05 12.83	110.49 12.83	106.97 12.83	103.48 12.83
HYDROGRAPH AT +	D@E	.615	1	FLOW	28.51	27.62	26.74	25.87

				TIME	12.83	12.83	12.83	12.83
HYDROGRAPH AT								
+	F	.815	1	FLOW TIME	130.32 13.17	126.11 13.17	121.96 13.17	117.95 13.33
DIVERSION TO								
+	DF	.815	1	FLOW TIME	104.25 13.17	100.89 13.17	97.57 13.17	94.36 13.33
HYDROGRAPH AT								
+	D@F	.815	1	FLOW TIME	26.06 13.17	25.22 13.17	24.39 13.17	23.59 13.33
2 COMBINED AT								
+	J3-1	1.430	1	FLOW TIME	51.83 13.00	50.20 13.00	48.58 13.00	46.99 13.00
HYDROGRAPH AT								
+	J	1.140	1	FLOW TIME	13.79 17.83	10.25 18.17	6.53 18.33	2.83 18.50
2 COMBINED AT								
+	J3-2	2.570	1	FLOW TIME	51.83 13.00	50.20 13.00	48.58 13.00	46.99 13.00
HYDROGRAPH AT								
+	G	.810	1	FLOW TIME	263.54 13.17	257.51 13.17	251.51 13.17	245.56 13.17
DIVERSION TO								
+	DDG	.810	1	FLOW TIME	210.83 13.17	206.01 13.17	201.21 13.17	196.44 13.17
HYDROGRAPH AT								
+	D@G	.810	1	FLOW TIME	52.71 13.17	51.50 13.17	50.30 13.17	49.11 13.17
HYDROGRAPH AT								
+	H	.740	1	FLOW TIME	282.19 12.83	275.35 12.83	268.54 12.83	261.78 12.83
DIVERSION TO								
+	DDH	.740	1	FLOW TIME	225.75 12.83	220.28 12.83	214.83 12.83	209.43 12.83
HYDROGRAPH AT								
+	D@H	.740	1	FLOW TIME	56.44 12.83	55.07 12.83	53.71 12.83	52.36 12.83
4 COMBINED AT								
+	J3	8.880	1	FLOW TIME	312.19 13.33	300.98 13.00	291.34 13.00	281.83 13.00
ROUTED TO								
+	RCH-3	8.880	1	FLOW TIME	307.27 13.50	297.87 13.17	285.79 13.17	276.82 13.17
DIVERSION TO								
+	D-J3	8.880	1	FLOW TIME	153.63 13.50	148.93 13.17	142.90 13.17	138.41 13.17
HYDROGRAPH AT								
+	D@J3	8.880	1	FLOW TIME	153.63 13.50	148.93 13.17	142.90 13.17	138.41 13.17
HYDROGRAPH AT								
+	IEAST	.180	1	FLOW TIME	126.16 12.33	123.09 12.33	120.03 12.33	117.00 12.33
DIVERSION TO								
+	DDG	.180	1	FLOW TIME	100.93 12.33	98.47 12.33	96.03 12.33	93.60 12.33
HYDROGRAPH AT								
+	D@IE	.180	1	FLOW TIME	25.23 12.33	24.62 12.33	24.01 12.33	23.40 12.33
HYDROGRAPH AT								
+	OEAST	.210	1	FLOW TIME	2.86 17.17	2.21 17.50	1.59 17.83	.98 18.00
2 COMBINED AT								
+	CP2	.390	1	FLOW TIME	25.23 12.33	24.62 12.33	24.01 12.33	23.40 12.33
2 COMBINED AT								
+	CPO+J3	9.270	1	FLOW TIME	156.64 13.17	152.34 13.17	146.24 13.17	141.68 13.17
DIVERSION TO								
+	DNA	9.270	1	FLOW TIME	40.00 12.50	40.00 12.50	40.00 12.50	40.00 12.50



HYDROGRAPH AT									
+	D@NOA	9.270	1	FLOW TIME	116.64 13.17	112.34 13.17	106.24 13.17	101.68 13.17	
ROUTED TO									
+	NP-A	9.270	1	FLOW TIME	53.33 14.33	52.16 14.33	51.05 14.33	49.76 14.33	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5105.83 14.33	5105.72 14.33	5105.60 14.33	5105.48 14.33	
HYDROGRAPH AT									
+	K-1	.077	1	FLOW TIME	60.74 12.50	59.54 12.50	58.35 12.50	57.16 12.50	
DIVERSION TO									
+	DDK1	.077	1	FLOW TIME	30.37 12.50	29.77 12.50	29.17 12.50	28.58 12.50	
HYDROGRAPH AT									
+	D@K1	.077	1	FLOW TIME	30.37 12.50	29.77 12.50	29.17 12.50	28.58 12.50	
HYDROGRAPH AT									
+	K-2	.105	1	FLOW TIME	83.14 12.33	81.48 12.50	79.86 12.50	78.24 12.50	
DIVERSION TO									
+	DDK2	.105	1	FLOW TIME	41.57 12.33	40.74 12.50	39.93 12.50	39.12 12.50	
HYDROGRAPH AT									
+	D@K2	.105	1	FLOW TIME	41.57 12.33	40.74 12.50	39.93 12.50	39.12 12.50	
HYDROGRAPH AT									
+	K-3	.033	1	FLOW TIME	32.15 12.33	31.50 12.33	30.86 12.33	30.22 12.33	
DIVERSION TO									
+	DDK3	.033	1	FLOW TIME	16.07 12.33	15.75 12.33	15.43 12.33	15.11 12.33	
HYDROGRAPH AT									
+	D@K3	.033	1	FLOW TIME	16.07 12.33	15.75 12.33	15.43 12.33	15.11 12.33	
3 COMBINED AT									
+	CP-K	.215	1	FLOW TIME	87.22 12.33	85.42 12.33	83.63 12.33	81.85 12.33	
HYDROGRAPH AT									
+	EM-5	.030	1	FLOW TIME	56.53 12.33	55.82 12.33	55.11 12.33	54.40 12.33	
ROUTED TO									
+	DP-EM5	.030	1	FLOW TIME	21.64 12.67	21.41 12.67	21.19 12.67	20.96 12.67	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	26.44 12.67	26.41 12.67	26.37 12.67	26.33 12.67	
2 COMBINED AT									
+	CPEM5	.245	1	FLOW TIME	104.71 12.50	102.86 12.50	101.01 12.50	99.17 12.50	
DIVERSION TO									
+	DNB	.245	1	FLOW TIME	40.00 12.33	40.00 12.33	40.00 12.33	40.00 12.33	
HYDROGRAPH AT									
+	D@NOB	.245	1	FLOW TIME	64.71 12.50	62.86 12.50	61.01 12.50	59.17 12.50	
ROUTED TO									
+	NP-B	.245	1	FLOW TIME	8.28 17.50	8.25 17.67	8.22 17.33	8.20 17.50	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5107.78 17.83	5107.75 17.67	5107.72 17.50	5107.70 17.33	
2 COMBINED AT									
+	NORTH	9.515	1	FLOW TIME	61.48 14.33	60.30 14.33	59.17 14.33	57.87 14.33	
HYDROGRAPH AT									
+	M	.560	1	FLOW TIME	229.45 12.67	223.62 12.67	217.83 12.67	212.08 12.67	
ROUTED TO									
+	RES-M	.560	1	FLOW	59.65	58.59	57.49	56.41	

				TIME	13.67	13.67	13.67	13.67
				** PEAK STAGES IN FEET **				
			1	STAGE	4.96	4.86	4.75	4.64
				TIME	13.67	13.67	13.67	13.67
HYDROGRAPH AT								
+	OFF-4	.060	1	FLOW	27.36	26.64	25.94	25.24
				TIME	12.50	12.50	12.50	12.50
2 COMBINED AT								
+	M+OFF4	.620	1	FLOW	67.04	65.81	64.59	63.22
				TIME	13.00	13.00	13.00	13.00
DIVERSION TO								
+	DDM	.620	1	FLOW	13.41	13.16	12.92	12.64
				TIME	13.00	13.00	13.00	13.00
HYDROGRAPH AT								
+	DØM	.620	1	FLOW	53.63	52.65	51.67	50.58
				TIME	13.00	13.00	13.00	13.00
HYDROGRAPH AT								
+	OFF-3	.191	1	FLOW	88.81	86.71	84.62	82.55
				TIME	12.67	12.67	12.67	12.67
2 COMBINED AT								
+	OF3+4	.811	1	FLOW	131.95	128.56	125.18	121.76
				TIME	12.83	12.83	12.83	12.83
HYDROGRAPH AT								
+	EM-1	.046	1	FLOW	80.73	79.70	78.67	77.65
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	JEM1+	.857	1	FLOW	175.19	171.35	167.54	163.74
				TIME	12.50	12.50	12.50	12.50
HYDROGRAPH AT								
+	TRI	.009	1	FLOW	6.67	6.51	6.36	6.20
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	CPPP1	.866	1	FLOW	179.31	175.38	171.48	167.60
				TIME	12.50	12.50	12.50	12.50
ROUTED TO								
+	PP-1	.866	1	FLOW	64.36	63.51	62.67	61.85
				TIME	14.50	14.50	14.33	14.33
				** PEAK STAGES IN FEET **				
			1	STAGE	22.73	22.59	22.45	22.31
				TIME	14.50	14.50	14.33	14.33
ROUTED TO								
+	RCHPP1	.866	1	FLOW	64.36	63.51	62.67	61.85
				TIME	14.67	14.67	14.50	14.50
HYDROGRAPH AT								
+	EM-3	.023	1	FLOW	44.94	44.36	43.79	43.21
				TIME	12.17	12.17	12.17	12.17
2 COMBINED AT								
+	JCH1	.889	1	FLOW	66.22	65.38	64.53	63.71
				TIME	14.33	14.33	14.33	14.33
HYDROGRAPH AT								
+	WV20-B	.017	1	FLOW	20.35	19.99	19.63	19.28
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	JCH2	.906	1	FLOW	84.45	83.17	81.90	80.64
				TIME	12.33	12.33	12.33	12.33
DIVERSION TO								
+	DNC	.906	1	FLOW	40.00	40.00	40.00	40.00
				TIME	12.17	12.17	12.17	12.17
HYDROGRAPH AT								
+	DØNOC	.906	1	FLOW	44.45	43.17	41.90	40.64
				TIME	12.33	12.33	12.33	12.33
ROUTED TO								
+	NP-C	.906	1	FLOW	31.58	31.59	31.60	31.62
				TIME	23.00	22.83	22.67	22.50
				** PEAK STAGES IN FEET **				
			1	STAGE	5097.36	5097.36	5097.36	5097.36
				TIME	23.00	22.83	22.67	22.50
2 COMBINED AT								
+	CP-NOR	10.421	1	FLOW	85.85	84.02	82.27	80.34
				TIME	14.50	14.50	14.50	14.33

HYDROGRAPH AT									
+	IWEST	.350	1	FLOW TIME	187.08	182.50	177.95	173.43	
					12.50	12.50	12.50	12.50	
DIVERSION TO									
+	DDIW	.350	1	FLOW TIME	149.67	146.00	142.36	138.74	
					12.50	12.50	12.50	12.50	
HYDROGRAPH AT									
+	D@IW	.350	1	FLOW TIME	37.42	36.50	35.59	34.69	
					12.50	12.50	12.50	12.50	
HYDROGRAPH AT									
+	OWEST	.180	1	FLOW TIME	5.07	3.90	2.79	1.52	
					17.50	17.67	18.00	18.17	
2 COMBINED AT									
+	CP1	.530	1	FLOW TIME	37.42	36.50	35.59	34.69	
					12.50	12.50	12.50	12.50	
2 COMBINED AT									
+	NOR+I	10.951	1	FLOW TIME	89.47	87.61	85.86	84.00	
					14.50	14.33	14.33	14.33	
HYDROGRAPH AT									
+	EM-3A	.010	1	FLOW TIME	22.31	22.03	21.75	21.48	
					12.17	12.17	12.17	12.17	
HYDROGRAPH AT									
+	EM-4	.100	1	FLOW TIME	156.73	154.52	152.31	150.11	
					12.33	12.33	12.33	12.33	
2 COMBINED AT									
+	CEMB1	.110	1	FLOW TIME	174.31	171.89	169.47	167.05	
					12.33	12.33	12.33	12.33	
ROUTED TO									
+	EMB-1	.110	1	FLOW TIME	52.15	51.62	51.00	50.39	
					12.83	12.83	12.83	12.83	
				** PEAK STAGES IN FEET **					
			1	STAGE	5082.02	5081.97	5081.92	5081.87	
				TIME	12.83	12.83	12.83	12.83	
ROUTED TO									
+	RHEMB1	.110	1	FLOW TIME	51.80	51.26	50.61	50.03	
					12.83	12.83	12.83	12.83	
HYDROGRAPH AT									
+	EM-6	.078	1	FLOW TIME	122.27	120.54	118.82	117.10	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	EM-7	.034	1	FLOW TIME	19.87	19.33	18.79	18.26	
					12.33	12.33	12.33	12.33	
3 COMBINED AT									
+	CP-PP2	.222	1	FLOW TIME	171.07	168.38	165.48	162.79	
					12.33	12.33	12.33	12.33	
ROUTED TO									
+	PP-2	.222	1	FLOW TIME	10.22	10.09	9.98	9.91	
					20.50	20.67	20.50	20.67	
				** PEAK STAGES IN FEET **					
			1	STAGE	5101.11	5101.05	5100.98	5100.91	
				TIME	20.67	20.67	20.67	20.67	
2 COMBINED AT									
+	JCHAN2	11.173	1	FLOW TIME	98.78	96.84	94.99	93.08	
					14.50	14.50	14.33	14.33	
ROUTED TO									
+	CHAN-2	11.173	1	FLOW TIME	98.74	96.82	94.98	92.98	
					14.50	14.50	14.50	14.33	
HYDROGRAPH AT									
+	L2	.234	1	FLOW TIME	148.45	145.13	141.82	138.53	
					12.50	12.50	12.50	12.50	
DIVERSION TO									
+	D-L	.234	1	FLOW TIME	74.23	72.56	70.91	69.26	
					12.50	12.50	12.50	12.50	
HYDROGRAPH AT									
+	D@L	.234	1	FLOW TIME	74.23	72.56	70.91	69.26	
					12.50	12.50	12.50	12.50	
ROUTED TO									
+	RES-L	.234	1	FLOW TIME	33.83	33.12	32.41	31.71	
					12.83	12.83	12.83	12.83	
				** PEAK STAGES IN FEET **					
			1	STAGE	3.58	3.51	3.44	3.37	

				TIME	12.83	12.83	12.83	12.83
HYDROGRAPH AT								
+	L3	.018	1	FLOW TIME	24.11 12.33	23.71 12.33	23.32 12.33	22.92 12.33
HYDROGRAPH AT								
+	VPH-1	.035	1	FLOW TIME	47.18 12.33	46.41 12.33	45.63 12.33	44.86 12.33
2 COMBINED AT								
+	VPCP-1	.053	1	FLOW TIME	71.29 12.33	70.12 12.33	68.95 12.33	67.77 12.33
ROUTED TO								
+	VPNEPD	.053	1	FLOW TIME	19.24 12.83	18.84 12.83	18.45 12.83	18.06 12.83
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	62.89 12.83	62.83 12.83	62.78 12.83	62.72 12.83
3 COMBINED AT								
+	VPCP1A	11.460	1	FLOW TIME	139.74 12.83	136.78 12.83	133.85 12.83	130.77 12.83
ROUTED TO								
+	RECH4A	11.460	1	FLOW TIME	138.06 12.83	135.08 12.83	132.40 12.83	129.27 12.83
ROUTED TO								
+	RCH4B	11.460	1	FLOW TIME	136.63 13.00	133.75 13.00	130.98 13.00	127.98 13.17
HYDROGRAPH AT								
+	WV-20A	.013	1	FLOW TIME	7.92 12.33	7.72 12.33	7.51 12.33	7.31 12.33
ROUTED TO								
+	HASKEL	.013	1	FLOW TIME	2.00 12.83	1.96 12.83	1.92 12.83	1.89 12.83
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	5195.33 12.83	5195.32 12.83	5195.30 12.83	5195.29 12.83
HYDROGRAPH AT								
+	EM-2	.062	1	FLOW TIME	67.41 12.50	66.33 12.50	65.25 12.50	64.17 12.50
2 COMBINED AT								
+	20A+2	.075	1	FLOW TIME	69.27 12.50	68.15 12.50	67.04 12.50	65.93 12.50
ROUTED TO								
+	EMG-1	.075	1	FLOW TIME	35.65 12.83	35.09 12.83	34.54 12.83	33.98 12.83
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	88.69 12.83	88.65 12.83	88.61 12.83	88.57 12.83
ROUTED TO								
+	EMG-1	.075	1	FLOW TIME	35.08 13.00	34.82 13.00	33.90 13.00	33.70 13.00
HYDROGRAPH AT								
+	EMTC	.053	1	FLOW TIME	39.62 12.33	38.41 12.33	37.32 12.50	36.28 12.50
HYDROGRAPH AT								
+	EM-10	.053	1	FLOW TIME	29.86 12.50	28.98 12.50	28.11 12.50	27.24 12.50
3 COMBINED AT								
+	JEM02	.181	1	FLOW TIME	88.46 12.50	86.58 12.50	83.74 12.50	81.44 12.50
ROUTED TO								
+	EMO-2	.181	1	FLOW TIME	49.68 13.17	48.52 13.17	47.22 13.17	45.95 13.17
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	69.74 13.17	69.69 13.17	69.63 13.17	69.58 13.17
ROUTED TO								
+	EMOc	.181	1	FLOW TIME	49.30 13.17	48.14 13.17	46.77 13.33	45.57 13.33
HYDROGRAPH AT								
+	EM-11	.012	1	FLOW TIME	15.44 12.17	14.99 12.17	14.54 12.17	14.10 12.17



HYDROGRAPH AT									
+	EM-9	.021	1	FLOW TIME	27.01	26.23	25.45	24.67	
					12.17	12.17	12.17	12.17	
3 COMBINED AT									
+	JG2&B2	.214	1	FLOW TIME	53.33	52.11	50.67	49.31	
					13.17	13.17	13.17	13.17	
HYDROGRAPH AT									
+	EM-8	.046	1	FLOW TIME	45.35	44.08	42.81	41.54	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	EM-12	.015	1	FLOW TIME	28.78	28.10	27.41	26.72	
					12.17	12.17	12.17	12.17	
3 COMBINED AT									
+	TODETN	.275	1	FLOW TIME	112.78	109.94	107.10	104.27	
					12.33	12.33	12.33	12.33	
ROUTED TO									
+	DETN	.275	1	FLOW TIME	33.01	32.32	31.61	30.91	
					14.67	14.67	14.67	14.67	
				** PEAK STAGES IN FEET **					
			1	STAGE	3.50	3.43	3.36	3.29	
				TIME	14.67	14.67	14.67	14.67	
2 COMBINED AT									
+	J4B	11.735	1	FLOW TIME	161.77	158.26	154.59	150.95	
					13.50	13.50	13.50	13.50	
ROUTED TO									
+	RCH-4C	11.735	1	FLOW TIME	161.67	158.15	154.51	150.86	
					13.50	13.50	13.50	13.50	
HYDROGRAPH AT									
+	A3	.055	1	FLOW TIME	81.57	80.33	79.10	77.86	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	A3A	.007	1	FLOW TIME	10.21	10.03	9.85	9.68	
					12.17	12.17	12.17	12.17	
2 COMBINED AT									
+	COMBA3	.062	1	FLOW TIME	90.04	88.67	87.29	85.92	
					12.33	12.33	12.33	12.33	
ROUTED TO									
+	RES-6	.062	1	FLOW TIME	34.25	33.89	33.54	33.19	
					12.67	12.67	12.67	12.67	
				** PEAK STAGES IN FEET **					
			1	STAGE	5078.85	5078.78	5078.71	5078.64	
				TIME	12.67	12.67	12.67	12.67	
HYDROGRAPH AT									
+	A3B	.026	1	FLOW TIME	35.10	34.53	33.95	33.38	
					12.33	12.33	12.33	12.33	
DIVERSION TO									
+	PARK	.026	1	FLOW TIME	8.78	8.63	8.49	8.35	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	D-PARK	.026	1	FLOW TIME	26.33	25.89	25.46	25.04	
					12.33	12.33	12.33	12.33	
ROUTED TO									
+	RES-5	.026	1	FLOW TIME	15.37	15.10	14.83	14.57	
					12.50	12.50	12.50	12.50	
				** PEAK STAGES IN FEET **					
			1	STAGE	5071.14	5071.11	5071.08	5071.06	
				TIME	12.50	12.50	12.50	12.50	
ROUTED TO									
+	R-9	.026	1	FLOW TIME	14.98	14.51	14.32	14.18	
					12.67	12.67	12.67	12.67	
HYDROGRAPH AT									
+	A13A	.006	1	FLOW TIME	6.66	6.53	6.41	6.29	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	A13B	.040	1	FLOW TIME	46.30	45.46	44.62	43.78	
					12.33	12.33	12.33	12.33	
2 COMBINED AT									
+	COMA13	.046	1	FLOW TIME	52.96	51.99	51.03	50.07	
					12.33	12.33	12.33	12.33	
HYDROGRAPH AT									
+	A12A	.015	1	FLOW	18.64	18.30	17.97	17.63	

				TIME	12.17	12.17	12.17	12.17
HYDROGRAPH AT								
+	A12	.020	1	FLOW TIME	27.30 12.17	26.79 12.17	26.28 12.17	25.77 12.17
2 COMBINED AT								
+	COMA12	.035	1	FLOW TIME	45.94 12.17	45.09 12.17	44.25 12.17	43.40 12.17
3 COMBINED AT								
+	JRES3	.107	1	FLOW TIME	99.96 12.33	98.15 12.33	96.36 12.33	94.47 12.33
ROUTED TO								
+	RES-3	.107	1	FLOW TIME	47.40 12.67	45.98 12.67	44.65 12.67	43.35 12.67
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	5061.87 12.67	5061.84 12.67	5061.81 12.67	5061.79 12.67
HYDROGRAPH AT	A13	.050	1	FLOW TIME	60.24 12.33	59.18 12.33	58.12 12.33	57.06 12.33
HYDROGRAPH AT	A12B	.030	1	FLOW TIME	68.94 12.17	68.06 12.17	67.18 12.17	66.31 12.17
3 COMBINED AT								
+	JRES1	.187	1	FLOW TIME	128.12 12.33	124.86 12.33	121.55 12.33	118.37 12.17
ROUTED TO								
+	RES-1	.187	1	FLOW TIME	15.81 14.33	15.58 14.33	15.35 14.33	15.12 14.33
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	5060.30 14.33	5060.26 14.33	5060.22 14.33	5060.19 14.33
3 COMBINED AT	ABMSR	11.984	1	FLOW TIME	203.26 13.17	199.08 13.17	194.91 13.17	190.65 13.17
HYDROGRAPH AT	OFF-1	.023	1	FLOW TIME	14.87 12.33	14.50 12.33	14.12 12.33	13.75 12.33
ROUTED TO								
+	R8	.023	1	FLOW TIME	14.17 12.50	13.83 12.50	13.49 12.50	12.98 12.50
HYDROGRAPH AT	A5	.060	1	FLOW TIME	101.37 12.33	99.97 12.33	98.58 12.33	97.18 12.33
HYDROGRAPH AT	CSR-7	.014	1	FLOW TIME	17.56 12.33	17.26 12.33	16.96 12.33	16.66 12.33
3 COMBINED AT								
+	J-1	.097	1	FLOW TIME	129.54 12.33	127.49 12.33	125.44 12.33	123.40 12.33
ROUTED TO								
+	EXDET	.097	1	FLOW TIME	118.99 12.50	120.21 12.50	121.42 12.50	122.46 12.50
				** PEAK STAGES IN FEET **				
			1	STAGE TIME	5125.29 12.50	5125.29 12.50	5125.29 12.50	5125.29 12.50
DIVERSION TO	D-DIV	.097	1	FLOW TIME	59.50 12.50	60.10 12.50	60.71 12.50	61.23 12.50
HYDROGRAPH AT	DIV	.097	1	FLOW TIME	59.50 12.50	60.10 12.50	60.71 12.50	61.23 12.50
ROUTED TO	REXDET	.097	1	FLOW TIME	54.37 12.50	54.01 12.50	53.90 12.50	52.96 12.50
HYDROGRAPH AT	OFF-2	.050	1	FLOW TIME	28.29 12.33	27.55 12.33	26.82 12.33	26.09 12.33
ROUTED TO	R-19	.050	1	FLOW TIME	28.11 12.50	27.41 12.50	26.72 12.50	26.39 12.50

HYDROGRAPH AT									
+	CSR-6A	.005	1	FLOW TIME	5.79 12.33	5.68 12.33	5.58 12.33	5.47 12.33	
ROUTED TO									
+	EXDT1A	.005	1	FLOW TIME	5.02 12.33	5.00 12.33	4.97 12.33	4.95 12.33	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5105.30 12.33	5105.27 12.33	5105.24 12.33	5105.21 12.33	
2 COMBINED AT									
+	J-6	.055	1	FLOW TIME	33.01 12.50	32.27 12.50	31.53 12.50	31.16 12.50	
HYDROGRAPH AT									
+	CSR-6	.025	1	FLOW TIME	35.04 12.33	34.47 12.33	33.91 12.33	33.36 12.33	
2 COMBINED AT									
+	CPXDT1	.080	1	FLOW TIME	59.86 12.33	58.63 12.33	57.41 12.33	55.94 12.33	
ROUTED TO									
+	EXDT1	.080	1	FLOW TIME	20.24 12.83	20.03 12.83	19.82 12.83	19.61 12.83	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5106.94 12.83	5106.82 12.83	5106.69 12.83	5106.56 12.83	
HYDROGRAPH AT									
+	A1	.090	1	FLOW TIME	124.95 12.33	122.93 12.33	120.92 12.33	118.92 12.33	
2 COMBINED AT									
+	J8	.170	1	FLOW TIME	139.01 12.33	136.74 12.33	134.49 12.33	132.17 12.33	
ROUTED TO									
+	R21	.170	1	FLOW TIME	119.58 12.50	117.72 12.50	115.86 12.50	113.97 12.50	
2 COMBINED AT									
+	JRES2	.266	1	FLOW TIME	173.95 12.50	171.73 12.50	169.76 12.50	166.93 12.50	
ROUTED TO									
+	RES2	.266	1	FLOW TIME	15.37 16.83	15.23 16.67	15.09 16.67	14.95 16.67	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5070.98 16.83	5070.90 16.83	5070.83 16.83	5070.75 16.67	
ROUTED TO									
+	R22	.266	1	FLOW TIME	15.37 16.83	15.23 16.83	15.09 16.83	14.95 16.67	
HYDROGRAPH AT									
+	CSR-4	.030	1	FLOW TIME	41.96 12.17	41.21 12.17	40.47 12.17	39.72 12.17	
ROUTED TO									
+	EXDET2	.030	1	FLOW TIME	9.79 12.67	9.75 12.67	9.71 12.67	9.67 12.67	
				** PEAK STAGES IN FEET **					
			1	STAGE TIME	5096.59 12.67	5096.51 12.67	5096.42 12.67	5096.34 12.67	
HYDROGRAPH AT									
+	CSR-3	.005	1	FLOW TIME	9.54 12.17	9.39 12.17	9.24 12.17	9.10 12.17	
2 COMBINED AT									
+	J11	.035	1	FLOW TIME	15.89 12.33	15.68 12.33	15.48 12.33	15.28 12.33	
ROUTED TO									
+	DITCH	.035	1	FLOW TIME	17.59 12.50	17.34 12.50	17.08 12.50	16.82 12.50	
HYDROGRAPH AT									
+	A2	.050	1	FLOW TIME	64.81 12.17	63.67 12.17	62.53 12.17	61.40 12.17	
3 COMBINED AT									
+	JRES15	.352	1	FLOW TIME	80.64 12.33	79.25 12.33	77.87 12.33	76.51 12.33	
ROUTED TO									
+	RES15	.352	1	FLOW	10.22	10.12	10.02	9.92	

				TIME	29.33	29.17	29.17	29.00
				** PEAK STAGES IN FEET **				
1				STAGE	5062.98	5062.93	5062.88	5062.83
				TIME	29.50	29.33	29.17	29.17
ROUTED TO								
+	R23	.352	1	FLOW	10.22	10.12	10.02	9.92
				TIME	29.50	29.67	29.33	29.50
HYDROGRAPH AT								
+	RPE	.120	1	FLOW	110.88	108.73	106.59	104.45
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	ACS-1	.472	1	FLOW	110.88	108.73	106.59	104.45
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	VP3P3	12.456	1	FLOW	242.42	237.34	233.27	227.19
				TIME	12.67	12.67	12.67	12.67
HYDROGRAPH AT								
+	L1	.029	1	FLOW	38.51	37.88	37.24	36.60
				TIME	12.33	12.33	12.33	12.33
HYDROGRAPH AT								
+	P	.031	1	FLOW	55.48	54.55	53.62	52.70
				TIME	12.17	12.17	12.17	12.17
2 COMBINED AT								
+	VP3P2	.060	1	FLOW	83.57	82.15	80.73	79.32
				TIME	12.17	12.17	12.17	12.17
HYDROGRAPH AT								
+	Q	.052	1	FLOW	70.09	68.94	67.78	66.63
				TIME	12.33	12.33	12.33	12.33
2 COMBINED AT								
+	VP3P2A	.112	1	FLOW	142.83	140.49	138.16	135.84
				TIME	12.33	12.33	12.33	12.33
DIVERSION TO								
+	VPH	.112	1	FLOW	12.00	12.00	12.00	12.00
				TIME	12.00	12.00	12.00	12.00
HYDROGRAPH AT								
+	D0VPH	.112	1	FLOW	130.83	128.49	126.16	123.84
				TIME	12.33	12.33	12.33	12.33
ROUTED TO								
+	VPHRP	.112	1	FLOW	44.34	43.47	42.60	41.73
				TIME	12.67	12.67	12.67	12.67
				** PEAK STAGES IN FEET **				
1				STAGE	5066.43	5066.35	5066.26	5066.17
				TIME	12.67	12.67	12.67	12.67
HYDROGRAPH AT								
+	VPH2	.010	1	FLOW	13.51	13.28	13.05	12.82
				TIME	12.17	12.17	12.17	12.17
2 COMBINED AT								
+	VP3P3	.122	1	FLOW	49.80	48.85	47.90	46.94
				TIME	12.50	12.50	12.50	12.50
HYDROGRAPH AT								
+	VPH-3	.010	1	FLOW	13.51	13.28	13.05	12.82
				TIME	12.17	12.17	12.17	12.17
HYDROGRAPH AT								
+	VPH-4	.011	1	FLOW	14.86	14.60	14.35	14.10
				TIME	12.17	12.17	12.17	12.17
HYDROGRAPH AT								
+	VPH-5	.005	1	FLOW	7.59	7.46	7.33	7.20
				TIME	12.17	12.17	12.17	12.17
4 COMBINED AT								
+	VP3P-4	.148	1	FLOW	81.01	79.81	78.60	77.40
				TIME	12.33	12.33	12.33	12.33
ROUTED TO								
+	VPDICH	.148	1	FLOW	43.54	42.90	42.25	41.61
				TIME	13.00	13.00	13.00	13.00
				** PEAK STAGES IN FEET **				
1				STAGE	5063.05	5062.98	5062.91	5062.83
				TIME	13.00	13.00	13.00	13.00
2 COMBINED AT								
+	VP3P5	12.604	1	FLOW	283.71	278.10	273.48	266.87
				TIME	12.67	12.67	12.67	12.67





**5-YEAR EVENT PROPOSED CONDITIONS THROUGH PHASE 20 OF WOODLAND VILLAGE**

5 Year Event  
Base Model; Woodland  
Village through Pb 20

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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998 AND FEB 2010
* VERSION 4.1R
* RGMHEC2000 WWW.HEC-1.COM
* RUN DATE 07MAR21 TIME 17:24:13
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.  
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DDIAGRAM
1 ID 100 yr 24 hr event
2 ID VILLAGE PARKWAY HOMES 5 YEAR EVENT
3 ID FILE NAME VPH-5YR.DAT
4 ID USING TYPE II STORM DISTRIBUTION
5 ID BASE MODEL FROM WOODLAND VILLAGE PH 20
* DARF AREA (SQ. MI.)
* 1.00 0 - 2
* 0.99 2.1 - 8
* 0.98 8.1 - 16
* 0.97 16.1 - 29
* 0.96 29.1 - 43
* 0.95 43.1 - 63
* 0.94 63.1 - 98
6 IT 10 800
7 IO 5 0
8 JR PREC 1.0 .99 .98 .97 .96 .95
9 KK A
10 BA 0.72
11 PH
12 LS 1.7 54 .24 .44 .73 .98 1.16 1.56 2.06 2.56
13 UD .62
14 KK B
15 BA 1.78
16 LS 1.63 55
17 UD 1.1
18 KK D@A&B
19 HC 2
20 KK D-A&B
21 DT D-AB
22 DI 0 10 50 100 500
23 DQ 0 5 25 50 250
24 KK RCH-1
25 KM ROUTE A&B TO J1@AB
26 RD 10200 .04 .12 TRAP 3 1
27 KK C
28 BA 1.26
29 LS 1.7 54
30 UD .82
31 KK J1@A&B
32 HC 2
33 KK RCH-2
34 RD 3500 .06 .12 TRAP 10 2.5

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HEC-1 INPUT

PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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35	KK	D					
36	BA	1.0					
37	LS	1.57	50				
38	UD	.63					
39	KK	J2ABCD					
40	HC	2					
41	KK	DJ2					
42	KM	CHANGE DIVERSION FROM 50% TO 75%					
43	DT	J2					
44	DI	0	10	50	100	500	
45	DQ	0	7.5	37.5	75	375	
46	KK	E					
47	BA	.615					
48	LS	1.45	58				
49	UD	.68					
50	KK	DØE					
51	DT	DE					
52	DI	0	10	50	100	500	
53	DQ	0	10	50	100	500	
54	KK	F					
55	BA	0.815					
56	LS	1.51	57				
57	UD	1					
58	KK	DØF					
59	DT	DF					
60	DI	0	10	50	100	500	
61	DQ	0	10	50	100	500	
62	KK	J3-1					
63	HC	2					
64	KK	J					
65	BA	1.14					
66	LU	4	0.1				
67	UD	.67					
68	KK	J3-2					
69	HC	2					
70	KK	G					
71	BA	0.81					
72	LS	1.03	66				
73	UD	.93					

1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
74	KK	DØG									
75	DT	DDG									
76	DI	0	10	50	100	500					
77	DQ	0	10	50	100	500					
78	KK	H									
79	BA	0.74									
80	LS	1.12	64								
81	UD	.63									
82	KK	DØH									
83	DT	DDH									
84	DI	0	10	50	100	500					
85	DQ	0	10	50	100	500					
86	KK	J3									
87	HC	4									
88	KK	RCH-3									
89	RD	8000	.04	.05		TRAP	10	1			
90	KK	DØJ3									
91	DT	D-J3									
92	DI	0	10	50	100	500					
93	DQ	0	5	25	50	250					
94	KK	IEAST									
95	BA	.18									
96	LS		64								
97	UD	.22									
98	KK	DØIE									
99	DT	DDG									
100	DI	0	10	50	100	500					
101	DQ	0	8	40	80	400					
102	KK	OEAST									
103	BA	.21									
104	LU	4	.1								



105 KK CP2  
 106 HC 2  
 107 KK CPO+J3  
 108 HC 2  
 109 KK DENOA  
 110 DT DNA  
 111 DI 0 40 60 100 500 1000  
 112 DQ 0 0 40 40 40 40  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

113 KK RS-NOA NORTH RESERVOIR A  
 114 KM 36" OUTLET  
 115 RS 1 STOR 0  
 116 SA 0 .17 .91 2.24 3.55 4.94  
 117 SE 5101.5 5102 5103 5104 5105 5106  
 118 SQ 0 6 19 35 50 60  
 119 SE 5101.5 5102.5 5103.5 5104.5 5105.5 5106.5  
 120 KK I-KWATERSHED CONSISTING OF K+ EM-3+EM-5 APPROX.  
 121 BA .3741  
 122 LS 65  
 123 UD 0.61

124 KK DVI-K DIVERT FLOW FROM I-K SAME RATE AS FROM K  
 125 DT D-IK  
 126 DI 0 10 100 500  
 127 DQ 0 5 50 250

128 KK WV20-B PART OF WV-20 GOING NORTH  
 129 BA .017  
 130 LS 74  
 131 UD .16

132 KK CPEM5  
 133 HC 2

134 KK DENO B  
 135 DT DNB  
 136 DI 0 40 60 100 500 1000  
 137 DQ 0 0 40 40 40 40

138 KK RS-NOB NORTH RESERVOIR B  
 139 KM 12" OUTLET  
 140 RS 1 STOR 0  
 141 SA 0 0.02 0.16 0.52 1.73 3.30 5.24 5.38 5.52  
 142 SE 5102.5 5103 5104 5104 5106 5107 5108 5109 5110  
 143 SQ 0 2.2 4.5 5.6 7 8 9 10 11  
 144 SE 5102.5 5103.5 5104.5 5105.5 5106.5 5107.5 5108.5 5109.5

145 KK NORTH  
 146 HC 2

147 KK M  
 148 BA 0.56  
 149 LS 1.17 63  
 150 UD 0.52

151 KK RES-M  
 152 RS 1 STOR 0  
 153 SA 2.5 2.56 2.66 2.79 1.95 3.15 3.4 3.72 4.12  
 154 SE 0 1.38 2.06 2.68 3.29 3.99 4.87 5.91 7.1  
 155 SQ 0 6 19 35 50 60 72 78 90  
 156 SE 0 1 2 3 4 5 6 7 8  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

157 KK OFF-4 OFFSITE 4  
 158 BA .06  
 159 LS 63  
 160 UD .42

161 KK M+OFF4 COMBINE OFF4 + POND M  
 162 HC 2

163 KK DEM  
 164 DT DDM  
 165 DI 0 10 50 100 500 1000  
 166 DQ 0 2 10 20 100 200

167 KK OFF-3  
 168 BA 0.191  
 169 LS 65  
 170 UD 0.52

171 KK OF3+4 COMBINE OFF3 & OFF4 & POND M  
 172 HC 2

173 KK EM-1  
 174 BA .046  
 175 LS 88  
 176 UD 0.25

177 KK JEM1+ COMBINE EM1, POND M, OFF3 & OFF4  
 178 KM SAME AS JM EM1 OFF3 OFF4 IN HEC-HMS  
 179 HC 2

180 KK TRI TRIANGULAR AREA EAST OF VILLAGE PKWY  
 181 BA .009  
 182 LS 64.5  
 183 UD 0.16

184 KK CPPP1 ADD TRIANGULAR AREA TO FLOW INTO PP-1  
 185 HC 2

186 KK PP-1  
 187 KM NOW WITH 30" OUTLET  
 188 RS 1 STOR 0  
 189 SA 0 .11 .34 .73 1.19 1.82 1.96 2.10 2.24  
 190 SA 2.52  
 191 SE 14.34 15 16 17 18 19 20 21 22  
 192 SE 24  
 193 SQ 0 5.5 16 28 38 45 50 57 62  
 194 SQ 70 75  
 195 SE 14.34 15.34 16.34 17.34 18.34 19.34 20.34 21.34 22.34  
 196 SE 24.34

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

197 KK RCHPP1  
 198 RD 2475 .007 .04 TRAP 3 3

199 KK D@NOC  
 200 DT DNC  
 201 DI 0 40 80 100 500 1000  
 202 DQ 0 0 40 40 40 40

203 KK RS-NOC NORTH RESERVOIR C  
 204 KM 30" OUTLET  
 205 RS 1 STOR 0  
 206 SA 0 .22 .82 2.4 3.85 4.54 5.03 5.31  
 207 SE 5094 5095 5096 5097 5098 5099 5100 5101  
 208 SQ 0 5.5 16 28 38 45 50 57  
 209 SE 5094 5095 5096 5097 5098 5099 5100 5101

210 KK CP-NOR COMBINE 3 NORTH DET BASINS  
 211 HC 2

212 KK IWEST  
 213 BA .35  
 214 LS 64  
 215 UD .37

216 KK D@IW  
 217 DT DDIW  
 218 DI 0 10 50 100 500  
 219 DQ 0 8 40 80 400

220 KK OWEST  
 221 BA .18  
 222 LU 4 .1

223 KK CP1  
 224 HC 2

225 KK NOR+I COMBINE FLOW FROM 3 DET BASINS & OFFSITE WATERSHED I  
 226 HC 2

227 KK EM4  
 228 BA .1193  
 229 LS 84  
 230 UD .25

231 KK EMB-1  
 232 RS 1 STOR 0  
 233 SA 1.5 1.54 1.6 1.68 1.79 1.95 2.15  
 234 SE 5078 5079.1 5079.69 5080.25 5080.95 5081.86 5082.96  
 235 SQ 0 8 26 40 52 60  
 236 SE 5078 5079 5080 5081 5082 5083

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

237 KK RHEMB1 REACH EMB-1  
 238 RD 759 .0066 .04 TRAP 3 3

239 KK EM-6  
 240 BA .0455  
 241 LS 1.6 84



313	DI	0	10	50	100	500				
314	DQ	0	10	50	100	500				
315	KK	VPCP3	COMBINE FLOWS GOING TO RET PONDS							
316	HC	2								

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

317	KK	VPNEPD	RETENTION/DETENTION POND							
318	KM	18-IN RCP OUTLET@ 60 FT								
319	RS	1	STOR	0						
320	SA	.14	.14	.34	.73	.94	1.13			
321	SE	56	57.9	58	62	64	66			
322	SQ	0	0	0	0	4	13	20	26	30
323	SE	56	57.9	58	60	61	62	63	64	65

324	KK	VPCP1A	COMBINE OUTFLOW FROM PVH NE POND WITH MAIN CHANNEL							
325	HC	3								

326	KK	RECH4A								
327	RD	395	.001	.04		TRAP	8		3	

328	KK	RCH4B								
329	RD	665	.001	.04		TRAP	10		3	

330	KK	WV-20A	PART OF WV-20 GOING SOUTH							
-----	----	--------	---------------------------	--	--	--	--	--	--	--

331	BA	.013								
332	LS		61							
333	UD	.15								

334	KK	HASKEL	12" RCP OUTLET							
-----	----	--------	----------------	--	--	--	--	--	--	--

335	RS	1	STOR	0						
336	SA	0	.47	.55	.60	.65				
337	SE	5194.5	5195	5196	5197	5198				
338	SQ	0	2.4	4.7	6	7.5				
339	SE	5194.5	5195.5	5196.5	5197.5	5198.5				

340	KK	EM-2								
341	BA	.0621								
342	LS		78							
343	UD	.32								

344	KK	20A+2	COMBINE W VILLAGE 20A POND WITH EM-2							
345	KM	FLOW GOES INTO POND EMG-1								
346	HC	2								

347	KK	EMG-1	DETENTION POND EMG-1							
348	RS	1	STOR	0						
349	SA	0.8	0.83	.87	.93	1.02	1.13	1.29		
350	SE	86	87.1	87.69	88.25	88.95	89.86	90.96		
351	SQ	0	8	26	40	52	60			
352	SE	86	87	88	89	90	91			

353	KK	EMG-1								
354	RD	1630	.01	.04		TRAP	3		3	

355	KK	EMTC								
356	BA	.053								
357	LS	1.5	79							
358	UD	.27								

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

359	KK	EM-10								
360	BA	.053								
361	LS	1.5	72							
362	UD	.32								

363	KK	JEM02								
364	HC	3								

365	KK	EMO-2								
366	RS	1	STOR	0						
367	SA	1.2	1.25	1.26	1.27	1.29	1.3	1.32	1.34	1.39
368	SE	67	68.49	68.91	69.31	69.72	70.21	70.69	71.31	72.8
369	SQ	0	11	32	56	76	90	100		
370	SE	67	68	69	70	71	72	73		

371	KK	EM0c								
372	RD	615	.003	.04		TRAP	0		3	

373	KK	EM-11								
374	BA	.012								
375	LS	1.5	86							
376	UD	.13								

377	KK	EM-9								
378	BA	.021								
379	LS	1.5	86							
380	UD	.13								





447	KK	A12																		
448	BA	.02																		
449	LS		73																	
450	UD	.12																		
451	KK	COMA12																		
452	HC	2																		
453	KK	JRES3																		
454	HC	3																		
455	KK	RES-3																		
456	RS	1	STOR	0																
457	SA	1	1.2	1.35	1.55	1.8														
458	SE	5059	5060	5061	5062	5063														
459	SQ	0	0	7.3	53.15	116.35														
460	KK	A13																		
461	BA	.05																		
462	LS		74																	
463	UD	.17																		
464	KK	A12B																		
465	BA	.03																		
466	LS		88																	
467	UD	.12																		
468	KK	JRES1																		
469	HC	3																		
470	KK	RES-1																		
471	RS	1	STOR	0																
472	SA	.0006	.0812	.2929	.6341	1.0634	1.5306	2.0022	2.4899	3.0079	3.5568									
473	SA	4.1272	5.1068	5.5454	6.8719															
474	SE	5057	5057.2	5057.4	5057.6	5057.8	5058	5058.2	5058.4	5058.6	5058.8									
475	SE	5059	5060	5061	5062															
476	SQ	0	0	0	0	0	0	0	1.2	2.4	3.6									
477	SQ	4.8	14	20	20															

HEC-1 INPUT

PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

478	KK	ABMSR																		
479	HC	3	ABOVE MUD SPRINGS ROAD																	
480	KK	OFF-1																		
481	BA	.0226																		
482	LS		63																	
483	UD	.22																		
484	KK	RB																		
485	RD	2000	.054	.05		TRAP	15	1												
486	KK	A5																		
487	BA	.06																		
488	LS		84																	
489	UD	.17																		
490	KK	CSR-7																		
491	BA	.014																		
492	LS		75																	
493	UD	.18																		
494	KK	J-1																		
495	HC	3																		
496	KK	EXDET																		
497	RS	1	STOR	0																
498	SA	0.27	0.28	0.37	0.47	0.52	0.52	0.52												
499	SE	5118	5119	5121	5125	5125.25	5125.5	5126												
500	SQ	0	0	9.8	23	99.5	238	631.1												
501	KK	DIV																		
502	DT	D-DIV																		
503	DI	0	10	100	1000															
504	DQ	0	5	50	500															
505	KK	REXDET																		
506	RD	1787	.025	.013		TRAP	40	1												
507	KK	OFF-2																		
508	BA	.0496																		
509	LS		63																	
510	UD	.27																		
511	KK	R-19																		
512	RD	1400	.02	.05		TRAP	15	1												
513	KK	CSR-6A																		
514	BA	.005																		
515	LS		73																	
516	UD	.17																		

HEC-1 INPUT

PAGE 14



584	RD	2600	.02	.05	TRAP	5	1
585	KK	RPE					
586	BA	0.12					
587	LS		72				
588	UD	.28					
589	KK	ACS-1					
590	HC	2					
591	KK	VPH2					
592	BA	0.01					
593	LS		77				
594	UD	0.16					

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

595	KK	VPH-3								
596	BA	.01								
597	LS		77							
598	UD	0.15								
599	KK	VPCP2								
600	HC	2								
601	KK	VPH-4								
602	BA	.011								
603	LS		77							
604	UD	0.15								
605	KK	VPH-5								
606	BA	.005								
607	LS		77							
608	UD	.13								
609	KK	RCLDP								
610	DR	SOUTH								
611	KK	VPCP-4								
612	HC	4								
613	KK	VPDICH								
614	KM	OUTLETIS 30" RCP @ ELEV 5058.15								
615	RS	1 STOR 0								
616	SA	.0001 0.13 0.42 0.74 1								
617	SE	5058.1 5059.5 5060 5062 5063.5								
618	SQ	0 5 16 29 35 44 46								
619	SE	5058.1 5059.1 5060.1 5061.1 5062.1 5063.1 5063.5								
620	KK	.02								
621	BA	.013								
622	LS		77							
623	UD	.16								
624	KK	VPCP6COMBINED FLOW IN MUD SPRINGS CHANNEL								
625	HC	4								
626	KK	PVE-1								
627	BA	.0128								
628	LS		76							
629	UD	.13								
630	KK	ABCDSP								
631	HC	2								
632	KK	PVE-2								
633	BA	.011								
634	LS		76							
635	UD	.13								

1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

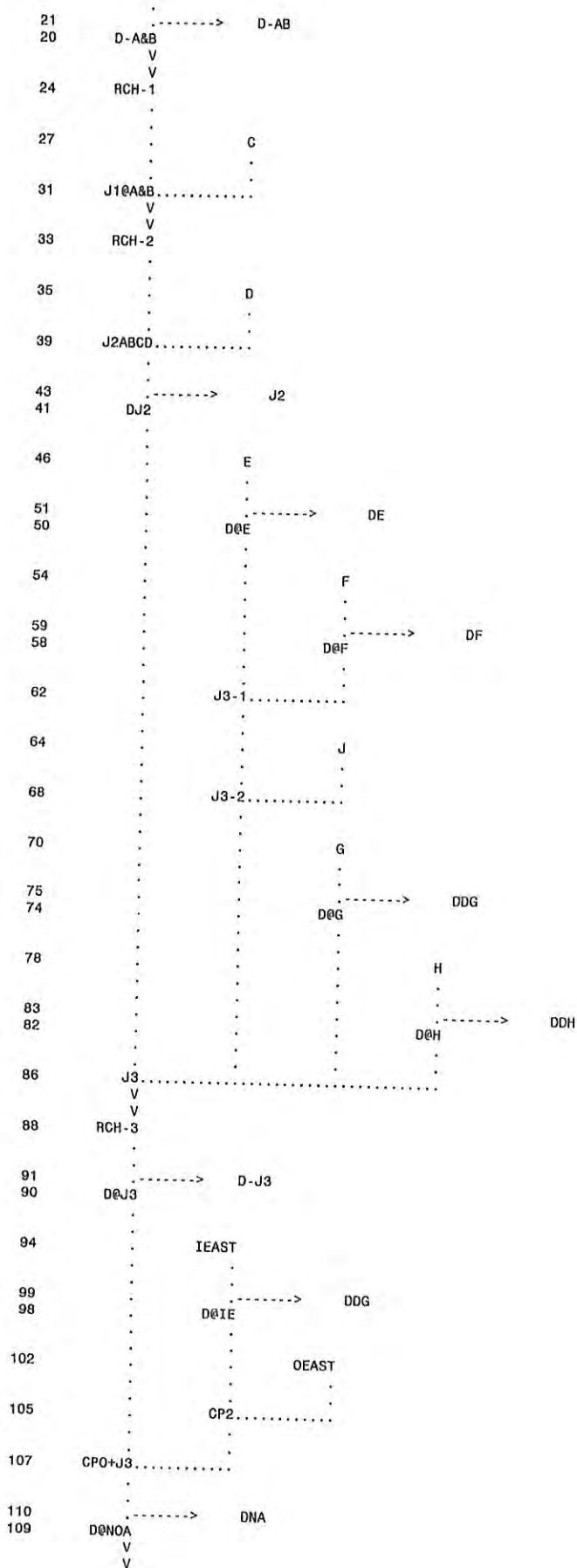
636	KK	BLCSRD								
637	HC	2								
638	ZZ									

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW	
LINE	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW	
NO.			
9	A		
	.		
14	.	B	
	.		
18	D@A&B.....		





113	RS-NOA		
120		I-K	
125			D-IK
124		DVI-K	
128			WV20-B
132		CPEM5	
135			DNB
134		D@NOB	
		V	
		V	
138		RS-NOB	
145	NORTH		
147		M	
		V	
		V	
151		RES-M	
157			OFF-4
161		M+OFF4	
164			DDM
163		D@M	
167			OFF-3
171		OF3+4	
173			EM-1
177		JEM1+	
180			TRI
184		CPPP1	
		V	
		V	
186		PP-1	
		V	
		V	
197		RCHPP1	
200			DNC
199		D@NOC	
		V	
		V	
203		RS-NOC	
210	CP-NOR		
212		IWEST	
217			DDIW
216		D@IW	
220			OWEST
223		CP1	
225	NOR+I		
227		EM4	
		V	

231	.	.	V		
	.	.	EMB-1		
	.	.	V		
	.	.	V		
237	.	.	RHEMB1		
	.	.	.		
239	.	.	.	EM-6	
	.	.	.	.	
243	.	.	.	.	EM-7
	.	.	.	.	.
247	.	.	CP-PP2	.....	
	.	.	V		
	.	.	V		
249	.	.	PP-2		
	.	.	.		
256	JCHAN2	.....	.		
	.	.	V		
258	CHAN-2		.		
	.	.	.		
260	.	.	L2		
	.	.	.		
265	.	.	.....	D-L	
264	.	.	D&L		
	.	.	V		
	.	.	V		
268	.	.	RES-L		
	.	.	.		
274	.	.	.	L3	
	.	.	.	.	
278	.	.	.	.	VPH-1
	.	.	.	.	.
282	.	.	.	VPCP-1	.....
	.	.	.	.	.
284	.	.	.	.	L1
	.	.	.	.	.
288	.	.	.	.	P
	.	.	.	.	.
292	.	.	.	VPCP2	.....
	.	.	.	.	.
294	.	.	.	.	Q
	.	.	.	.	.
298	.	.	.	VPCP2A	.....
	.	.	.	.	.
301	.	.	.	.	.
300	.	.	.	.....	VPH
	.	.	.	DEVPH	
	.	.	.	V	
	.	.	.	V	
304	.	.	.	VPHRP	
	.	.	.	.	
312	.	.	.	.	.
311	.	.	.	.....	SOUTH
	.	.	.	D-SOU	
	.	.	.	.	
315	.	.	.	VPCP3	.....
	.	.	.	V	
	.	.	.	V	
317	.	.	.	VPNEPD	
	.	.	.	.	
324	VPCP1A	.....	.		
	.	.	V		
	.	.	V		
326	RECH4A		.		
	.	.	V		
	.	.	V		
328	RCH4B		.		
	.	.	.		
330	.	.	WV-20A		
	.	.	V		
	.	.	V		
334	.	.	HASKEL		
	.	.	.		
340	.	.	.	EM-2	
	.	.	.	.	

344	.	20A+2	.....		
	.	V			
	.	V			
347	.	EMG-1			
	.	V			
	.	V			
353	.	EMG-1			
	.				
355	.		EMTC		
	.				
359	.			EM-10	
	.				
363	.	JEMO2	.....		
	.	V			
	.	V			
365	.	EMO-2			
	.	V			
	.	V			
371	.	EMOc			
	.				
373	.		EM-11		
	.				
377	.			EM-9	
	.				
381	.	JG2&B2	.....		
	.				
383	.		EM-8		
	.				
387	.			EM-12	
	.				
391	.	TODETN	.....		
	.	V			
	.	V			
393	.	DETN			
	.				
399	.	J4B	.....		
	.	V			
	.	V			
401	.	RCH-4C			
	.				
403	.	A3			
	.				
407	.		A3A		
	.				
411	.	COMBA3	.....		
	.	V			
	.	V			
413	.	RES-6			
	.				
418	.		A3B		
	.				
423	.				
422	.		D-PARK	PARK	
	.		V		
	.		V		
426	.		RES-5		
	.		V		
	.		V		
431	.		R-9		
	.				
433	.			A13A	
	.				
437	.			A13B	
	.				
441	.		COMA13	.....	
	.				
443	.			A12A	
	.				
447	.			A12	
	.				
451	.			COMA12	.....



```

453 . . . . . JRES3 .....
      . . . . . V
455 . . . . . RES-3
      . . . . .
460 . . . . . A13
      . . . . .
464 . . . . . A12B
      . . . . .
468 . . . . . JRES1 .....
      . . . . . V
470 . . . . . RES-1
      . . . . .
478 . . . . . ABMSR .....
      . . . . .
480 . . . . . OFF-1
      . . . . . V
484 . . . . . R8
      . . . . .
486 . . . . . A5
      . . . . .
490 . . . . . CSR-7
      . . . . .
494 . . . . . J-1 .....
      . . . . . V
496 . . . . . EXDET
      . . . . .
502 . . . . . D-DIV
501 . . . . . DIV
      . . . . . V
505 . . . . . REXDET
      . . . . .
507 . . . . . OFF-2
      . . . . . V
511 . . . . . R-19
      . . . . .
513 . . . . . CSR-6A
      . . . . . V
517 . . . . . EXDT1A
      . . . . .
522 . . . . . J-6 .....
      . . . . .
524 . . . . . CSR-6
      . . . . .
528 . . . . . CPXDT1 .....
      . . . . . V
530 . . . . . EXDT1
      . . . . .
535 . . . . . A1
      . . . . .
539 . . . . . J8 .....
      . . . . . V
541 . . . . . R21
      . . . . .
543 . . . . . JRES2 .....
      . . . . . V
545 . . . . . RES2
      . . . . . V
553 . . . . . R22
      . . . . .
555 . . . . . CSR-4
      . . . . . V
559 . . . . . EXDET2
      . . . . .

```

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564 . . . . . CSR-3
568 . . . . . J11.....
570 . . . . . V
570 . . . . . V
570 . . . . . DITCH
572 . . . . . A2
576 . . . . . JRES15.....
576 . . . . . V
576 . . . . . V
578 . . . . . RES15
578 . . . . . V
578 . . . . . V
583 . . . . . R23
585 . . . . . RPE
589 . . . . . ACS-1.....
591 . . . . . VPH2
595 . . . . . VPH-3
599 . . . . . VPCP2.....
601 . . . . . VPH-4
605 . . . . . VPH-5
610 . . . . .
609 . . . . . RCLDP <----- SOUTH
611 . . . . . VPCP-4.....
611 . . . . . V
613 . . . . . V
613 . . . . . VPDICH
620 . . . . . Q2
624 . . . . . VPCP6.....
626 . . . . . PVE-1
630 . . . . . ABCDSP.....
632 . . . . . PVE-2
636 . . . . . BLCSRD.....

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(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 AND FEB 2010 *
* VERSION 4.1R *
* RGMHEC2000 WWW.HEC-1.COM *
* RUN DATE 07MAR21 TIME 17:24:13 *
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* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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100 yr 24 hr event  
VILLAGE PARKWAY HOMES 5 YEAR EVENT  
FILE NAME VPH-5YR.DAT  
USING TYPE II STORM DISTRIBUTION  
BASE MODEL FROM WOODLAND VILLAGE PH 20

7 IO

OUTPUT CONTROL VARIABLES

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IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

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IT HYDROGRAPH TIME DATA  
 NMIN 10 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 800 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 6 0 ENDING DATE  
 NDTIME 1310 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .17 HOURS  
 TOTAL TIME BASE 133.17 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION  
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION  
 RATIOS OF PRECIPITATION  
 1.00 .99 .98 .97 .96 .95

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	
				1.00	.99	.98	.97	.96	.95	
HYDROGRAPH AT										
+	A	.720	1	FLOW	4.11	3.91	3.72	3.53	3.34	3.16
				TIME	18.00	18.00	18.00	18.00	18.00	18.17
HYDROGRAPH AT										
+	B	1.780	1	FLOW	11.68	11.14	10.62	10.10	9.59	9.09
				TIME	18.00	18.00	18.17	18.17	18.17	18.33
2 COMBINED AT										
+	D@A&B	2.500	1	FLOW	15.78	15.05	14.33	13.63	12.93	12.24
				TIME	18.00	18.00	18.00	18.17	18.17	18.17
DIVERSION TO										
+	D-AB	2.500	1	FLOW	7.89	7.53	7.17	6.81	6.47	6.12
				TIME	18.00	18.00	18.00	18.17	18.17	18.17
HYDROGRAPH AT										
+	D-A&B	2.500	1	FLOW	7.89	7.53	7.17	6.81	6.47	6.12
				TIME	18.00	18.00	18.00	18.17	18.17	18.17
ROUTED TO										
+	RCH-1	2.500	1	FLOW	7.89	7.52	7.16	6.80	6.45	6.11
				TIME	19.00	19.17	19.17	19.17	19.17	19.33
HYDROGRAPH AT										
+	C	1.260	1	FLOW	7.13	6.79	6.45	6.11	5.78	5.45
				TIME	18.00	18.17	18.17	18.17	18.17	18.17
2 COMBINED AT										
+	J1@A&B	3.760	1	FLOW	14.94	14.18	13.46	12.73	12.00	11.31
				TIME	18.00	18.17	18.17	18.33	18.50	18.50
ROUTED TO										
+	RCH-2	3.760	1	FLOW	15.14	14.31	13.63	12.87	12.16	11.46
				TIME	18.33	18.00	18.50	18.67	18.83	18.50
HYDROGRAPH AT										
+	D	1.000	1	FLOW	6.30	5.96	5.63	5.31	5.04	4.81
				TIME	15.33	15.50	15.50	15.67	17.50	18.00
2 COMBINED AT										
+	J2ABCD	4.760	1	FLOW	21.08	20.06	19.02	17.99	17.10	16.11
				TIME	17.50	18.00	18.17	17.83	18.00	18.17
DIVERSION TO										
+	J2	4.760	1	FLOW	15.81	15.04	14.27	13.49	12.83	12.08
				TIME	17.50	18.00	18.17	17.83	18.00	18.17
HYDROGRAPH AT										
+	DJ2	4.760	1	FLOW	5.27	5.01	4.78	4.50	4.28	4.03
				TIME	17.50	18.00	18.17	17.83	18.00	18.17
HYDROGRAPH AT										
+	E	.615	1	FLOW	6.68	6.37	6.07	5.77	5.48	5.20
				TIME	15.00	15.00	15.17	15.17	15.33	15.33



+		CPO+J3	9.270	1	FLOW TIME	3.14 18.17	2.95 17.67	2.83 17.83	2.69 18.00	2.53 18.17	2.38 18.83
	DIVERSION TO										
+		DNA	9.270	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
	HYDROGRAPH AT										
+		D@NOA	9.270	1	FLOW TIME	3.14 18.17	2.95 17.67	2.83 17.83	2.69 18.00	2.53 18.17	2.38 18.83
	ROUTED TO										
+		RS-NOA	9.270	1	FLOW TIME	3.04 18.17	2.92 17.83	2.78 18.00	2.62 18.17	2.47 18.17	2.32 18.33
					** PEAK STAGES IN FEET **						
				1	STAGE TIME	5102.01 18.17	5101.99 17.83	5101.96 18.00	5101.94 18.17	5101.91 18.17	5101.89 18.33
	HYDROGRAPH AT										
+		I-K	.374	1	FLOW TIME	14.46 13.00	13.77 13.00	13.08 13.00	12.42 13.00	11.76 13.00	11.12 13.00
	DIVERSION TO										
+		D- IK	.374	1	FLOW TIME	7.23 13.00	6.88 13.00	6.54 13.00	6.21 13.00	5.88 13.00	5.56 13.00
	HYDROGRAPH AT										
+		DVI-K	.374	1	FLOW TIME	7.23 13.00	6.88 13.00	6.54 13.00	6.21 13.00	5.88 13.00	5.56 13.00
	HYDROGRAPH AT										
+		WV20-B	.017	1	FLOW TIME	3.67 12.33	3.57 12.33	3.48 12.33	3.38 12.33	3.29 12.33	3.19 12.33
	2 COMBINED AT										
+		CPEM5	.391	1	FLOW TIME	8.35 13.00	7.98 13.00	7.61 13.00	7.26 13.00	6.90 13.00	6.56 13.00
	DIVERSION TO										
+		DNB	.391	1	FLOW TIME	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00	.00 .00
	HYDROGRAPH AT										
+		D@NOB	.391	1	FLOW TIME	8.35 13.00	7.98 13.00	7.61 13.00	7.26 13.00	6.90 13.00	6.56 13.00
	ROUTED TO										
+		RS-NOB	.391	1	FLOW TIME	4.66 15.17	4.61 15.17	4.56 15.00	4.52 14.83	4.44 14.83	4.32 14.83
					** PEAK STAGES IN FEET **						
				1	STAGE TIME	5104.64 15.33	5104.60 15.17	5104.56 15.17	5104.52 15.00	5104.47 15.00	5104.42 14.83
	2 COMBINED AT										
+		NORTH	9.661	1	FLOW TIME	7.54 17.67	7.25 17.33	6.92 17.33	6.61 17.50	6.33 17.67	6.06 17.83
	HYDROGRAPH AT										
+		M	.560	1	FLOW TIME	15.70 12.83	14.78 13.00	13.96 13.00	13.16 13.00	12.39 13.00	11.64 13.17
	ROUTED TO										
+		RES-M	.560	1	FLOW TIME	7.39 18.33	7.06 18.33	6.71 18.50	6.34 18.50	5.96 18.67	5.74 18.67
					** PEAK STAGES IN FEET **						
				1	STAGE TIME	1.11 18.33	1.08 18.33	1.05 18.50	1.03 18.50	.99 18.67	.96 18.67
	HYDROGRAPH AT										
+		OFF-4	.060	1	FLOW TIME	1.78 12.67	1.66 12.67	1.56 12.83	1.47 12.83	1.38 12.83	1.29 12.83
	2 COMBINED AT										
+		M+OFF4	.620	1	FLOW TIME	8.19 18.17	7.82 18.17	7.44 18.17	7.03 18.33	6.64 18.17	6.40 18.17
	DIVERSION TO										
+		DDM	.620	1	FLOW TIME	1.64 18.17	1.56 18.17	1.49 18.17	1.41 18.33	1.33 18.17	1.28 18.17
	HYDROGRAPH AT										
+		D@M	.620	1	FLOW TIME	6.65 18.17	6.26 18.17	5.95 18.17	5.62 18.33	5.31 18.17	5.12 18.17
	HYDROGRAPH AT										
+		OFF-3	.191	1	FLOW TIME	7.91 12.83	7.51 12.83	7.12 12.83	6.74 12.83	6.37 12.83	6.00 12.83
	2 COMBINED AT										
+		OF3+4	.811	1	FLOW TIME	10.28 12.83	9.73 12.83	9.20 12.83	8.69 13.00	8.23 13.00	7.82 15.17





+	EM-7	.061	1	FLOW TIME	19.10 12.33	18.71 12.33	18.33 12.33	17.94 12.33	17.55 12.33	17.17 12.33
3 COMBINED AT										
+	CP-PP2	.226	1	FLOW TIME	27.78 12.50	27.05 12.50	26.34 12.50	25.64 12.50	24.96 12.50	24.30 12.50
ROUTED TO										
+	PP-2	.226	1	FLOW TIME	18.99 13.83	18.84 13.83	18.69 13.83	18.49 13.67	18.16 13.67	17.84 13.67
** PEAK STAGES IN FEET **										
1	STAGE TIME				5174.12 13.83	5174.07 13.83	5174.03 13.83	5173.98 13.67	5173.91 13.67	5173.85 13.67
2 COMBINED AT										
+	JCHAN2	11.283	1	FLOW TIME	42.46 13.83	41.99 13.67	41.98 13.83	40.56 13.67	39.62 13.67	38.70 13.67
ROUTED TO										
+	CHAN-2	11.283	1	FLOW TIME	42.45 13.83	41.97 13.83	41.37 13.83	40.54 13.83	39.57 13.83	38.62 13.83
HYDROGRAPH AT										
+	L2	.234	1	FLOW TIME	14.35 12.50	13.63 12.50	12.93 12.50	12.24 12.50	11.56 12.50	10.89 12.50
DIVERSION TO										
+	D-L	.234	1	FLOW TIME	7.18 12.60	6.82 12.50	6.46 12.50	6.12 12.50	5.78 12.50	5.45 12.50
HYDROGRAPH AT										
+	D0L	.234	1	FLOW TIME	7.18 12.50	6.82 12.50	6.46 12.50	6.12 12.50	5.78 12.50	5.45 12.50
ROUTED TO										
+	RES-L	.234	1	FLOW TIME	3.25 14.00	3.13 14.00	3.01 14.00	2.90 14.17	2.78 14.17	2.67 14.17
** PEAK STAGES IN FEET **										
1	STAGE TIME				.59 14.00	.57 14.00	.55 14.00	.53 14.17	.51 14.17	.49 14.17
HYDROGRAPH AT										
+	L3	.018	1	FLOW TIME	4.91 12.33	4.80 12.33	4.69 12.33	4.57 12.33	4.46 12.33	4.35 12.33
HYDROGRAPH AT										
+	VPH-1	.035	1	FLOW TIME	9.63 12.33	9.40 12.33	9.18 12.33	8.96 12.33	8.74 12.33	8.52 12.33
2 COMBINED AT										
+	VPCP-1	.053	1	FLOW TIME	14.54 12.33	14.20 12.33	13.86 12.33	13.53 12.33	13.20 12.33	12.87 12.33
HYDROGRAPH AT										
+	L1	.029	1	FLOW TIME	7.84 12.33	7.66 12.33	7.48 12.33	7.29 12.33	7.11 12.33	6.93 12.33
HYDROGRAPH AT										
+	P	.031	1	FLOW TIME	11.21 12.17	10.95 12.17	10.69 12.17	10.42 12.17	10.16 12.17	9.90 12.17
2 COMBINED AT										
+	VPCP2	.060	1	FLOW TIME	16.84 12.17	16.43 12.17	16.03 12.17	15.62 12.17	15.22 12.17	14.83 12.17
HYDROGRAPH AT										
+	Q	.052	1	FLOW TIME	14.30 12.33	13.97 12.33	13.63 12.33	13.31 12.33	12.98 12.33	12.65 12.33
2 COMBINED AT										
+	VPCP2A	.112	1	FLOW TIME	29.23 12.33	28.56 12.33	27.89 12.33	27.22 12.33	26.56 12.33	25.90 12.33
DIVERSION TO										
+	VPH	.112	1	FLOW TIME	12.00 12.17	12.00 12.17	12.00 12.17	12.00 12.17	12.00 12.17	12.00 12.33
HYDROGRAPH AT										
+	D0VPH	.112	1	FLOW TIME	17.23 12.33	16.56 12.33	15.89 12.33	15.22 12.33	14.56 12.33	13.90 12.33
ROUTED TO										
+	VPHRP	.112	1	FLOW TIME	5.89 13.83	5.68 14.00	5.46 14.00	5.24 14.17	5.01 14.17	4.79 14.33
** PEAK STAGES IN FEET **										
1	STAGE TIME				5062.62 13.83	5062.60 14.00	5062.58 14.00	5062.56 14.17	5062.54 14.17	5062.53 14.33
DIVERSION TO										
+	SOUTH	.112	1	FLOW TIME	5.89 13.83	5.68 14.00	5.46 14.00	5.24 14.17	5.01 14.17	4.79 14.33



+	JG2&B2	.214	1	FLOW TIME	7.19 15.00	6.95 15.17	6.72 15.17	6.49 15.17	6.26 15.33	6.04 15.33
	HYDROGRAPH AT									
+	EM-8	.046	1	FLOW TIME	1.28 14.00	1.22 14.00	1.16 14.17	1.10 14.33	1.05 14.50	.99 14.67
	HYDROGRAPH AT									
+	EM-12	.015	1	FLOW TIME	.93 13.00	.87 13.00	.81 13.17	.76 13.33	.72 13.67	.69 13.83
	3 COMBINED AT									
+	TODETN	.275	1	FLOW TIME	9.16 15.00	8.85 15.00	8.55 15.00	8.24 15.00	7.94 15.00	7.64 15.00
	ROUTED TO									
+	DETN	.275	1	FLOW TIME	5.54 19.50	5.35 19.67	5.18 19.67	5.00 19.67	4.84 19.83	4.67 19.83
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	1.00 19.50	.97 19.67	.94 19.67	.91 19.83	.88 19.83	.85 20.00
	2 COMBINED AT									
+	J4B	11.957	1	FLOW TIME	47.78 14.67	46.64 14.33	45.68 14.17	44.56 14.17	43.35 14.17	42.17 14.17
	ROUTED TO									
+	RCH-4C	11.957	1	FLOW TIME	47.76 14.67	46.62 14.33	45.62 14.17	44.51 14.17	43.32 14.17	42.15 14.17
	HYDROGRAPH AT									
+	A3	.055	1	FLOW TIME	18.55 12.33	18.17 12.33	17.80 12.33	17.42 12.33	17.05 12.33	16.68 12.33
	HYDROGRAPH AT									
+	A3A	.007	1	FLOW TIME	1.97 12.17	1.92 12.17	1.87 12.17	1.82 12.17	1.78 12.17	1.73 12.17
	2 COMBINED AT									
+	COMBA3	.062	1	FLOW TIME	20.23 12.33	19.81 12.33	19.39 12.33	18.98 12.33	18.57 12.33	18.16 12.33
	ROUTED TO									
+	RES-6	.062	1	FLOW TIME	9.18 12.67	8.95 12.67	8.72 12.67	8.49 12.67	8.27 12.67	8.04 12.67
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5075.50 12.67	5075.48 12.67	5075.46 12.67	5075.43 12.67	5075.41 12.67	5075.39 12.67
	HYDROGRAPH AT									
+	A3B	.026	1	FLOW TIME	7.18 12.33	7.01 12.33	6.85 12.33	6.68 12.33	6.52 12.33	6.36 12.33
	DIVERSION TO									
+	PARK	.026	1	FLOW TIME	1.79 12.33	1.75 12.33	1.71 12.33	1.67 12.33	1.63 12.33	1.59 12.33
	HYDROGRAPH AT									
+	D-PARK	.026	1	FLOW TIME	5.38 12.33	5.26 12.33	5.13 12.33	5.01 12.33	4.89 12.33	4.77 12.33
	ROUTED TO									
+	RES-5	.026	1	FLOW TIME	2.41 12.67	2.35 12.67	2.29 12.67	2.24 12.67	2.18 12.67	2.12 12.67
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5069.56 12.67	5069.55 12.67	5069.53 12.67	5069.52 12.67	5069.51 12.67	5069.49 12.67
	ROUTED TO									
+	R-9	.026	1	FLOW TIME	2.38 12.83	2.32 12.83	2.26 12.83	2.20 12.83	2.18 12.83	2.13 12.83
	HYDROGRAPH AT									
+	A13A	.006	1	FLOW TIME	1.08 12.33	1.05 12.33	1.02 12.33	.99 12.33	.95 12.33	.92 12.33
	HYDROGRAPH AT									
+	A13B	.040	1	FLOW TIME	7.92 12.33	7.69 12.33	7.47 12.33	7.25 12.33	7.03 12.33	6.81 12.33
	2 COMBINED AT									
+	COMA13	.046	1	FLOW TIME	9.00 12.33	8.74 12.33	8.49 12.33	8.23 12.33	7.98 12.33	7.73 12.33
	HYDROGRAPH AT									
+	A12A	.015	1	FLOW TIME	3.49 12.33	3.40 12.33	3.31 12.33	3.23 12.33	3.14 12.33	3.06 12.33
	HYDROGRAPH AT									
+	A12	.020	1	FLOW TIME	4.57 12.17	4.43 12.17	4.30 12.17	4.16 12.17	4.03 12.17	3.90 12.17





+	EXDT1A	.005	1	FLOW TIME	1.02 12.33	.99 12.33	.96 12.33	.94 12.33	.91 12.33	.88 12.33
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5103.62 12.33	5103.60 12.33	5103.58 12.33	5103.57 12.33	5103.55 12.33	5103.53 12.33
2 COMBINED AT										
+	J-6	.055	1	FLOW TIME	2.00 12.67	1.91 12.83	1.82 12.83	1.76 12.67	1.57 12.83	1.53 12.83
HYDROGRAPH AT										
+	CSR-6	.025	1	FLOW TIME	7.43 12.33	7.26 12.33	7.10 12.33	6.93 12.33	6.77 12.33	6.61 12.33
2 COMBINED AT										
+	CPXDT1	.080	1	FLOW TIME	8.45 12.33	8.25 12.33	8.06 12.33	7.87 12.33	7.68 12.33	7.49 12.33
ROUTED TO										
+	EXDT1	.080	1	FLOW TIME	4.19 13.00	4.07 13.00	3.96 13.00	3.85 12.83	3.72 12.83	3.58 12.83
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5101.88 13.00	5101.86 13.00	5101.83 12.83	5101.81 12.83	5101.78 12.83	5101.75 12.83
HYDROGRAPH AT										
+	A1	.090	1	FLOW TIME	26.44 12.33	25.85 12.33	25.26 12.33	24.68 12.33	24.09 12.33	23.52 12.33
2 COMBINED AT										
+	J8	.170	1	FLOW TIME	29.31 12.33	28.64 12.33	27.98 12.33	27.32 12.33	26.66 12.33	26.01 12.33
ROUTED TO										
+	R21	.170	1	FLOW TIME	25.30 12.50	24.73 12.50	24.17 12.50	23.60 12.50	23.04 12.50	22.48 12.50
2 COMBINED AT										
+	JRES2	.266	1	FLOW TIME	30.48 12.50	29.80 12.50	29.12 12.50	28.42 12.50	27.75 12.50	27.07 12.50
ROUTED TO										
+	RES2	.266	1	FLOW TIME	8.43 15.50	8.30 15.50	8.18 15.50	8.05 15.33	7.92 15.33	7.79 15.33
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5067.81 15.50	5067.78 15.50	5067.74 15.50	5067.71 15.33	5067.67 15.33	5067.64 15.33
ROUTED TO										
+	R22	.266	1	FLOW TIME	8.43 15.50	8.30 15.50	8.18 15.50	8.05 15.50	7.91 15.50	7.79 15.50
HYDROGRAPH AT										
+	CSR-4	.030	1	FLOW TIME	7.75 12.17	7.55 12.17	7.34 12.17	7.14 12.17	6.94 12.17	6.74 12.17
ROUTED TO										
+	EXDET2	.030	1	FLOW TIME	3.13 12.67	3.05 12.67	2.98 12.67	2.90 12.67	2.82 12.67	2.75 12.67
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5092.28 12.67	5092.25 12.67	5092.22 12.67	5092.19 12.67	5092.16 12.67	5092.13 12.67
HYDROGRAPH AT										
+	CSR-3	.005	1	FLOW TIME	2.15 12.17	2.10 12.17	2.06 12.17	2.01 12.17	1.97 12.17	1.92 12.17
2 COMBINED AT										
+	J11	.035	1	FLOW TIME	4.25 12.33	4.15 12.33	4.04 12.33	3.94 12.33	3.84 12.33	3.73 12.33
ROUTED TO										
+	DITCH	.035	1	FLOW TIME	4.65 12.67	4.62 12.67	4.38 12.67	4.25 12.67	4.06 12.67	3.93 12.67
HYDROGRAPH AT										
+	A2	.050	1	FLOW TIME	12.58 12.33	12.28 12.33	11.98 12.33	11.68 12.33	11.38 12.33	11.09 12.33
3 COMBINED AT										
+	JRES15	.352	1	FLOW TIME	16.29 12.33	15.88 12.33	15.38 12.33	14.93 12.33	14.59 12.33	14.17 12.67
ROUTED TO										
+	RES15	.352	1	FLOW TIME	3.88 25.17	3.75 25.17	3.62 25.17	3.48 25.17	3.35 25.17	3.21 25.17
				** PEAK STAGES IN FEET **						
			1	STAGE TIME	5060.80 25.17	5060.77 25.17	5060.74 25.17	5060.70 25.17	5060.67 25.17	5060.64 25.00



**APPENDIX D**  
**DETENTION POND DATA**

**VILLAGE PARKWAY HOMES**  
**DETENTION/RETENTION POND DETAILS**

WEST POND

ELEVATION, FT	AREA, ACRES
5060	0.278
5062	0.607
5064	0.848
5066	0.972
5067	1.013

Outlet: 30 inch rcp at elevation 5061.5

NORTHEAST POND

ELEVATION, FT	AREA, ACRES
5056	0.14*
5057.9	0.14*
5058	0.34
5062	0.73
5064	0.94
5066	1.13

\*The bottom 2 feet of the pond will be filled with rock. The area shown is the total area multiplied by 0.4, the porosity of gravel.

Outlet: 18-inch rcp at elevation 5060

SOUTHEAST POND

ELEVATION, FT	AREA, ACRES
5058.1	0.0001
5059.5	0.13
5060	0.42
5062	0.74
5063.5	1.0

Outlet: 30 inch rcp at elevation 5058.1







### GENERAL NOTES

- 1) ALL PLANTING AND IRRIGATION SHALL BE INSTALLED PER LOCAL GOVERNING CODES.
- 2) TREES
  - ONE HALF OF ALL DECIDUOUS TREES SHALL HAVE A MINIMUM CALIPER OF 2 INCHES THE REMAINING MAY HAVE A CALIPER OF 1" AT TIME OF PLANTING.
  - ONE HALF OF ALL EVERGREEN TREES SHALL HAVE A MINIMUM HEIGHT OF 7 FEET, THE REMAINING MAY HAVE A HEIGHT OF 5 FEET AT TIME OF PLANTING.
- 3) FINAL PLANT SELECTION AND LAYOUT WILL BE BASED ON SOUND HORTICULTURAL PRACTICES RELATING TO MICRO-CLIMATE, SOIL, AND WATER REGIMES. ALL TREES WILL BE STAKED SO AS TO REMAIN UPRIGHT AND PLUMB FOLLOWING INSTALLATION. PLANT SIZE AND QUALITY AT TIME OF PLANTING WILL BE PER THE AMERICAN STANDARD FOR NURSERY STOCK (ANSI Z60.1-1990).
- 4) ALL SHRUB BEDS WILL RECEIVE 4" DEPTH MULCH WITH WEED CONTROL.
- 5) ALL LANDSCAPING WILL BE AUTOMATICALLY IRRIGATED. CONTAINER PLANTINGS WILL BE DRIP IRRIGATED BASED ON THE SPECIFIC HORTICULTURAL REQUIREMENTS OF EACH SPECIES. A REDUCED-PRESSURE-TYPE BACKFLOW PREVENTOR WILL BE PROVIDED ON THE IRRIGATION SYSTEM AS REQUIRED PER CODE.
- 6) PLAN IS CONCEPTUAL. PLANT QUANTITIES INDICATED ARE PER CITY OF RENO CODE REQUIREMENTS. PLANT LOCATIONS, FINAL SPECIES SELECTION, AND SIZE AT PLANTING SHALL BE DETERMINED DURING DEVELOPMENT OF THE FINAL CONSTRUCTION DOCUMENTS.

### PLANT LEGEND

- FLOWERING TREE
- DECIDUOUS SHADE TREE
- EVERGREEN TREE
- COMMON AREA LANDSCAPING
- STREETSCAPE
- RE-VEGETATION AREA

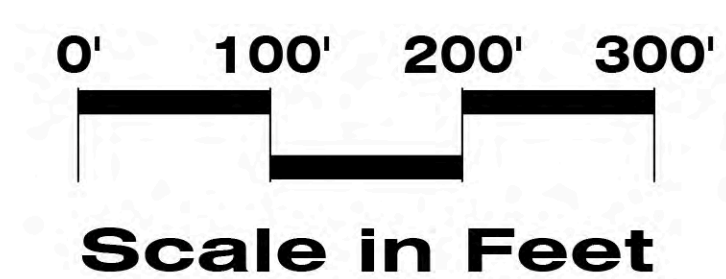
### LANDSCAPE DATA

DEVELOPMENT SITE AREA = 2,034,615 SQ FT (46.7 ACRES)  
 ZONING: HDS (HIGH DENSITY SUBURBAN)  
 TOWNHOME REQUIRED LANDSCAPE AREA = 146,400 SQ FT (3.36 ACRES) MIN.  
 (20% OF TOWNHOME DEVELOPMENT SITE 732,000 SQ FT (16.8 ACRES))  
 INCLUDES  
 • COMMON AREA LANDSCAPE  
 • FRONT, BACK AND SIDE YARDS WHERE ADJACENT TO THE STREET  
 • STREETScape ALONG WOODLAND VILLAGE PARKWAY - 1 TREE PER 50 LN FT

SINGLE FAMILY  
 • 1 TREE PER LOT OR 50 LN FT OF STREET FRONTAGE FOR FRONT AND SIDE YARDS  
 • 1 TREE PER 50 LN FT ALONG WOODLAND VILLAGE PARKWAY

PARKING TREES REQUIRED  
 • 1 TREE PER 20 LN FT IN OFF-SET ROWS FOR PARKING SCREENING BETWEEN MF AND SF  
 • 1 TREE PER 10 PARKING SPACES

NOTE: FINAL NUMBERS OF TREES SHOWN IN COMMON AREAS TO BE DETERMINED DURING FINAL DESIGN.



No.	Revision	Date

LA No: 082-814-01-21  
 Designed: KRJ  
 Drawn: KRJ  
 Checked: RWH  
 Date: 9/9/21



GEOTECHNICAL INVESTIGATION FOR  
VILLAGE PARKWAY TOWNHOMES  
WOODLAND VILLAGE  
RENO, NEVADA

File No. 31097

February 5, 2021

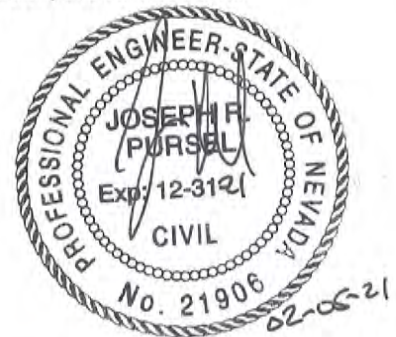


Prepared For:

Mr. Robert Lissner  
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4790 Caughlin Parkway, #519  
Reno, Nevada 89519

Prepared By:

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5405 Mae Anne Avenue  
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Joseph R. Pursel  
Geotechnical Division Manager



February 5, 2021

Mr. Robert Lissner  
Woodland Village North, LLC  
4790 Caughlin Parkway, #519  
Reno, Nevada 89519

Job No. 31097

RE: Geotechnical Investigation  
Village Parkway Townhomes  
Woodland Village  
Reno, NV

Dear Client Name:


Attached please find the results of our geotechnical investigation for the proposed Village Parkway Townhomes, located in Woodland Village, north of Reno, Nevada. Summit excavated 14 exploratory test pits to characterize the site for townhomes. Material testing was performed on samples obtained from the site. Results of the analyses and logs of the test pits are included as sheets in this report.

The site is currently vacant, with one abandoned structure towards the north end, and typical high desert grasses and shrubs throughout. Silty Sands (SM) were encountered primarily on this site along with some area of poor and well graded sand. The access to the site is proposed off of Village Parkway, an existing and year-round maintained roadway. The site appears to be suitable for the proposed improvements.

The following report provides geotechnical recommendations and guidelines for the design and construction of the project. We wish to thank you for the opportunity of providing our services. We are readily available to answer any related questions.

Sincerely,

**SUMMIT ENGINEERING CORPORATION**

  
Joseph R. Pursel, P.E.  
Geotechnical Division Manager

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**GEOTECHNICAL INVESTIGATION  
VILLAGE PARKWAY TOWNHOMES  
RENO, NEVADA**

**I. INTRODUCTION**

**A. Project Description**

This report presents the results of our Geotechnical Investigation to evaluate Village Parkway Townhome site for construction of townhomes, utilities and surface improvements in Woodland Village. Exploration, laboratory testing and engineering analyses were conducted to provide geotechnical recommendations for the design and construction of the project.

The subject property is located adjacent to Village Parkway, Woodland Village, in the Cold Springs area North of Reno, Nevada. On the west of the property is open, vacant land, sloping up to foothills. On the east and south sides of the property are existing single family homes and development. On the north side mainly vacant land, with one large parcel residence adjacent, and the waste water treatment plant farther to the north. There is an abandoned structure on the northern 1/3 of the project site. The site is bound on the east by Village Parkway and Mud Springs Road. The site gently slopes to the east and south, with the western boundary increasing in elevation adjacent to the foothills. The site is covered with sparse vegetation typically found in the high desert, including, but not limited to, grasses, sagebrush, rabbitbrush. The site is located in the northeast ¼ of the northeast ¼, the southeast ¼ of the northeast ¼, and the northeast ¼ of the southeast ¼ of Section 17, Township 21 North, Range 18 East in Reno, Nevada. Sheet 1 presents a vicinity map. Sheet 2 presents the project site with test pit locations.

It is our understanding that the proposed development will entail the construction of a 372 unit townhome site, with site grading, flat work, paving, utilities including drainage retention/detention structures.

The site will have access from Village Parkway, a fully paved and year-round maintained roadway.

**B. Purpose and Scope**

The purpose of this investigation was to determine subsurface soil and bedrock conditions and to provide geotechnical design criteria for the proposed townhomes. The scope of this investigation included surface reconnaissance, subsurface exploration, analysis of field and laboratory data, research of pertinent geologic literature and report preparation. This report provides conclusions and recommendations



concerning:

- General subsurface conditions and geology
- Site preparation and earthwork
- Engineering properties of the soils and bedrock that will influence design of future structures, including:
  - Bearing capacities
  - Settlement potential
  - Lateral earth pressures
  - Portland cement concrete
  - Asphalt concrete
  - Seismic design criteria
  - Infiltration for drainage structure design and sizing

### **C. Field Exploration and Laboratory Testing**

Summit Engineering Corporation conducted the subsurface investigation by excavating 14 exploratory test pits to depths of up to 13 feet below existing grade. The exploratory test pits were excavated with a medium sized Link Belt Track Excavator equipped with a 48” side bucket. Representative samples of the soil were collected from the test pits. Selected samples were tested at Summit’s laboratory and other outside laboratories. A Professional Engineer supervised the logging of the subsurface conditions encountered. Sheet 1 shows the vicinity map and Sheet 2 presents a site map with the locations of the test pits. Sheet 3 shows the geologic data surrounding the site. Sheet 4 shows the faults in the surrounding area. Sheets 5 through 18 display the logs of soils and bedrock encountered in the excavations. Sheets 19 and 20 show the logs of the infiltration pits. Sheet 21 provides a key to the excavation logs as well as a copy of the Unified Soil Classification System used to identify the site soils. Sheet 22 provides the results to the sieve value for the samples. Sheet 23 provides the results to the plastic index results for the samples. Sheet 24 provides the results to the resistance value for one sample. Sheet 25 provides the results for two sulfate samples.

Representative bulk samples were taken from the excavations every two feet of depth or every significant lithologic change. Representative samples were tested as follows: 1) sieve analyses tests (ASTM D422); 2) moisture content tests (ASTM D2216); 3) Atterberg limits tests (ASTM 4318), to confirm field soil classifications; 4) an R-value test (ASTM D2844) to determine a flexible pavement structural section; and

5) a soluble sulfates test to determine if the native soils are reactive with Portland cement concrete. The index test results can be used to estimate engineering properties of the native soil/bedrock. Results of the laboratory tests are displayed on the test pit logs, and presented independently in Appendix D. All laboratory testing was conducted in accordance with the applicable standards.

## II. DISCUSSION

### A. Site Description

The site is located in the Cold Springs area of Reno, NV, adjacent to Village Parkway. The site consists mainly high desert grasses and shrubs. Surrounding the subject site are single family developments and open land.

### B. Site Geology

The project is located in Reno, Nevada. The most current geologic area map is Soeller and Nielson's 1980 Geologic Map of the Reno NW Quadrangle, Nevada. The rock types encountered were identified by those authors as the following:

**Qs: Flood Plain Deposits:** Pale to dark yellowish-brown and pale brownish white beds of moderately to well-sorted fine to very fine sand, and poorly sorted sandy clay and mud.

**Qfg: Alluvial Fan Deposits:** Gray to yellowish-brown deposits of sandy to pebbly cobble and boulder gravel.

**Qb: Beach Deposits:** Lakeshore deposits of pale yellowish-brown to pale yellowish-white, granular medium to coarse sand, sandy pebble gravel, and granule gravel.

The site has been mapped by F.E.M.A. (Federal Emergency Management Agency Map Numbers 32031C2825H and 32031C2805H) as being in Zone X. Zone X is described as "Area of Minimal Flood Hazard."

### C. Regional Seismicity

The property, according to International Building Code 2012/2015 maps, may be subject to strong seismic acceleration, 0.509 (S1) ground acceleration, a major seismic event. The effect of seismic shaking, therefore, is an important consideration.

The site has native soil profile D – Default, since the top 100’ of soils conditions is not known. The following table summarizes seismic design parameters for the 2012/2015 International Building Code criteria for structural design of the project:

**IBC SEISMIC DESIGN**

Site Class	D - Default
Soil Profile Type	Stiff Soil
Soil Shear Wave Velocity ( $\bar{v}_s$ )	600 to 1,200 ft/s
Standard penetration resistance (N)	15 to 50
Soil undrained shear strength ( $s_u$ )	1,000 to 2,000 psf
Site Coefficient ( $F_a$ ) w/ short accel. ( $s_s$ )	1.2
Site Coefficient ( $F_v$ ) w/ 1-sec. accel. ( $s_1$ )	*
Max. ground motion, 0.2-sec SA ( $S_s$ ), %g	1.54
Max. ground motion, 1.0-sec SA ( $S_1$ ), %g	0.509
Design acceleration, $S_{DS}$ , g	1.232
Design acceleration, $S_{D1}$ , g	*

**NOTE** \*: Structural Engineer shall determine these values in accordance with ASCE 7-16, Section 11.4.8, Exception 2.

The site is located in Woodland Village, in the Cold Springs area of Reno, NV. Earthquake activity is difficult to predict and it is not known which documented fault system may produce an earthquake event and associated surface rupture. Current research by the Nevada Bureau of Mines and Geology and the University of Nevada, Reno indicates that a local earthquake event of Richter scale magnitude 7.0 would not be unlikely.

At the present time, there are not any local codes that provide guidelines for the evaluation of seismic risk or surface rupture hazard associated with Quaternary (Holocene and Pleistocene) faults, except a minimum 50 foot set back from occupied structures. The State of Nevada requires the use of seismic provisions set by the IBC, as well as adoptions of appropriate local standards (NRS 278.580.5). For the purposes of assessing seismic hazard and potential fault rupture hazard, standard engineering practice is to pursue the most diligent investigation of those faults deemed to be most likely to be active. Most geological consultants in Nevada follow the conventions established by the Nevada Earthquake Safety Council, whose guidelines are based on the Alquist-Priolo Act of 1972 in California. Per these guidelines, faults with evidence of movement in Holocene time (past 12,000 years) are considered “Holocene active”. Those faults with evidence of displacement during Late Pleistocene time (10,000 to 130,000 years ago) would be considered “Late Quaternary active”. Faults with evidence of last displacement having occurred during middle and early Quaternary time (130,000 years to 1,600,000 years ago) are considered “Quaternary Active Faults” (formerly “potentially active”). Faults with last displacement older than 1,600,000 years are deemed “inactive”. Active faults are afforded a greater degree of study and analysis than those regarded as inactive. Normally, any fault suspected of being active, as demonstrated by offset of the argillic (topsoil)



horizon, poses a greater risk to development and requires a minimum setback of 50 feet for occupied structures. **No mapped active faults cross the site or are within 50 feet of the site (Sheet 4) nor were any encountered during this investigation.** An inactive fault does bisect the site in a north-south direction. All published data indicates this fault as inactive and no evidence of past seismic activity was found in the exploration. The closest mapped active faults (<15,000 years) are approximately 0.25 miles to the south. The seismic hazard at the Village Parkway Townhomes is probably no greater than other comparable locations in the area that are located at comparable distances to identified faults.

Occupied structures have been built over and adjacent to inactive faults in the greater Reno area for decades, without significant harm to residents from temblors affecting the area. Building codes have evolved in recent years to provide adequate structural protection to residents for the level of tremors experienced to date. Summit Engineering does not recommend siting occupied structures across any fault, regardless of activity classification.

Groundwater was not encountered during the exploratory work by Summit. Liquefaction, a hazard in seismic zones where water-saturated, loose soils lose their bearing during seismic shaking, is not anticipated to be a problem on the project site.

#### **D. Subsurface Materials and Conditions**

Based on a total of 14 exploratory test pits completed in this area, along with the 2 infiltration pits, the native material appeared to be the only material present and there was no evidence of uncontrolled fill on the site. The native material was present throughout the test pits up to the depth of excavation. The majority of this material was silty sands, SM. All material on-site meeting structural fill parameters in Appendix A will be suitable to be used to provide suitable support for proposed structures.

Groundwater was not encountered on the site. Groundwater is not anticipated to impact development of the site.

### **III. CONCLUSIONS AND RECOMMENDATIONS**

From a geotechnical engineering standpoint, it is our opinion that the site at Village Parkway is suitable for the construction of the proposed 372 townhome improvements provided that the recommendations contained in this report are incorporated into design and construction. The following sections present our conclusions and recommendations concerning the proposed project.

#### **A. Foundation Considerations**

Native non-expansive gravels and sands will be suitable to provide direct foundation support. If any clay or expansive silts are found they should not be used to provide direct foundation support. Analysis obtained from field and laboratory testing indicates native materials (Silty Sands (SM)) that can typically support up to **2,000 pounds per square foot** for dead plus long term live loads, on spread type footings with less than 1 inch of total settlement and less than 1/2 inch of differential settlement across the length of the structures.

In Silty Sands (SM), passive soil resistance to lateral movement may be calculated using an equivalent fluid weight of 150 pounds per square foot per foot of depth and a coefficient of friction of 0.25. Active lateral soil pressure may be calculated using an equivalent fluid weight of 45 pounds per square foot per foot of depth. The at-rest soil pressure may be calculated using an equivalent fluid pressure of 60 pounds per square foot per foot of depth. These values assume that the native non-expansive granular soils and bedrock will provide direct foundation support

#### **B. Grading and Filling**

Any uncontrolled fill materials and clayey sand, if encountered, shall be removed prior to placing any fill. These materials are unsuitable for use as fill in structural areas due to the amount of deleterious materials observed. Therefore, these materials shall only be placed as the final lift of fill in landscaped areas.

All areas that are to receive fill or structural loading shall be scarified to a depth of at least 12 inches, moisture conditioned to within 2 percent of optimum, and re-compacted to at least 90 percent relative compaction (ASTM D 1557). If the native subgrade is too coarse to density test, then moisture conditioning and compaction shall be completed to the satisfaction of the Geotechnical Engineer. A proof rolling program of a minimum 5 complete passes with a minimum 10 ton roller or a Cat 825 self propelled sheepfoot may be acceptable. For footing trenches, 3 complete passes with hand compactors may be adequate.

All fill, except rock fill (<30% retained on the ¾” sieve), shall be placed in 12-inch maximum lifts, moisture conditioned to within 2 percent of optimum, and compacted to at least 90 percent (ASTM D1557). It is anticipated that many of the on-site materials will be amenable to density testing.

In structural areas, the maximum particle size shall be 12 inches. This material shall be placed in 12 inch lifts (maximum) moisture conditioned and compacted to the satisfaction of the Geotechnical Engineer. Care should be taken to insure that voids between cobbles and boulders are filled with finer materials. Five complete passes with a minimum 10 ton roller or a Cat 825 Sheepsfoot compactor may achieve adequate compaction. Acceptance of the density requirements shall be by observation of lift thickness, moisture conditioned, and applied compaction effort.

Any imported material for use in structural areas shall meet the specifications of Appendix A, Section 3.2 “structural fill material”. (Per the Standard Specifications for Public Works Construction 2016).

The following guideline specification is provided if it is decided to import structural cap material to the site.

<u>Sieve Sizes</u>	<u>Percentage Passing (by weight)</u>
6 Inch	100
¾ Inch	70-100
No. 40	15-50
No. 200	10-30
Liquid Limit (max.)	38
Plastic Index (max.)	15
Expansion Index (max.)	20
R-value (min.)	30

All imported structural cap material shall be moisture conditioned to within 2 percent of optimum and placed in 12 inch (max) finished lifts and compacted to a minimum 90 percent compaction relative to ASTM D 1557.

**C. Surface and Subsurface Drainage**

Surface drainage shall be diverted away from all buildings and not be permitted to pond or pool adjacent to foundations. It is recommended that all crawlspaces be lined with Visqueen sheeting, and that positive crawlspace drainage be provided to a collection point. A small diameter pipe (2 to 4-inch) may be placed beneath and perpendicular to the footing, sloped to drain to daylight, or the drain rock bedding of the sewer service lateral to the street may be utilized to drain the crawlspace. Slab-on-grade foundation systems may require subsurface drainage dependent on conditions encountered during grading. The Geotechnical

Engineer shall determine whether subsurface drainage is required at that time.

Grading plans should be designed to minimize the potential for infiltrated precipitation or yard irrigation to migrate laterally and down slope along the cut/fill interface and surfacing in down slope lots. Roof gutters and downspouts are recommended to discharge water well away from foundation areas.

#### **D. Slope Stability and Erosion Control**

The results of our exploration and testing indicate that 2:1 (H:V) slopes will be stable for on-site materials in cut and fill. All cut and fill slopes should incorporate brow ditches to divert surface drainage away from the slope face. Any major cut or fill slopes shall include mid-height benches in accordance with International Building Code standards.

The potential for dust generation, both during and after construction, is moderately high at this project. Dust control will be mandatory on this project in order to comply with air quality standards. The contractor shall submit a dust control plan and obtain the required permit from Washoe County prior to commencing site grading.

Stabilization of all slopes and areas disturbed by construction will be required to prevent erosion and to control dust. Stabilization may consist of riprap, re-vegetation and landscaping, or dust palliative. Slopes steeper than 3:1 (H:V) will require stabilization.

#### **E. Trenching and Excavation**

All trenching and excavation shall be conducted in accordance with all local, state, and federal (OSHA) standards. In general, all soil encountered during exploration meets the criteria for OSHA Type C soils. Any oversized material loosened during excavation will require scaling prior to permitting workmen to enter the trench.

Any area in question should be examined by the Geotechnical Engineer. The following table is reproduced from Occupational Safety and Health, Subpart P, 1926.652, Appendix B:



**TABLE B-1**

**MAXIMUM ALLOWABLE SLOPES**

SOIL OR ROCK TYPE	MAXIMUM ALLOWABLE SLOPES (H:V) <sup>[1]</sup> FOR EXCAVATIONS LESS THAN 20 FEET DEEP <sup>[3]</sup>
STABLE ROCK TYPE A <sup>[2]</sup> TYPE B TYPE C	VERTICAL (90°) 3/4:1 (53°) 1:1 (45°) 1 1/2:1 (34°)

**NOTES**

1. Numbers shown in parentheses next to maximum allowable slopes are angles expressed in degrees from the horizontal. Angles have been rounded off.
2. A short-term maximum allowable slope of 1/2 H:1V (63°) is allowed in excavations in Type A soil that are 12 feet (3.67 m) or less in depth. Short-term maximum allowable slopes for excavations greater than 12 feet (3.67 m) in depth shall be 3/4 H:1V (53°).
3. Sloping or benching for excavations greater than 20 feet deep shall be designed by a registered professional engineer.

Bedding and initial backfill over the pipe will require import to meet the specifications of the utility having jurisdiction. On-site soils may be used for trench backfill, provided particles over 4 inches in diameter are removed. Imported structural cap material or native silty sands or native gravels will be required within 3 feet below bottom of footing and 2 feet below bottom of pavement subgrade. All trench backfill shall be placed in 8 inch (max.) finished lifts, moisture conditioned to within 2 percent of optimum, and densified to at least 90 percent relative compaction (ASTM D1557). If metal pipes are to be utilized, corrosion protective measures shall be taken.

**F. Asphaltic Concrete Design**

The site is currently in the City of Reno. For the paving areas, the anticipated equivalent 18,000 pound Single Axle Load (ESAL) is 240,186. This is based on an assumed 1,980 light vehicle trips per day and 20 3-axle or more trucks, including school buses and waste disposal trucks. A proposed structural section for this area is to be 4 inches of asphalt on 12 inches of cement treated base on 20" of pit run (structural fill), and which is more than sufficient to support the anticipated traffic of passenger vehicles. The resultant "R" value tested for the light traffic private parking area subgrade is 0 (Sheet 24). A Type 3 (1/2 inch size) mix is recommended for all areas for a smoother, more flush finished surface, which is less susceptible to moisture penetration. A 50 Blow, Marshall mix design with 2-4 percent air voids is recommended for this

project. The use of PGG4-28NV is also recommended in order to increase the resistance to thermal cracking and help reduce pavement maintenance over the life of the pavement. A mix design shall be submitted to the Geotechnical Engineer for approval one week prior to paving.

Subgrade material that meets structural requirements, shall be scarified to a minimum depth of 6 inches, moisture conditioned to within 2 percent of optimum, and compacted to at least 90 percent. If structural requirements are not met, all areas should receive 2 feet of structural material. Aggregate base materials shall be Type 2, Class B. The aggregate base materials shall be approved by the Geotechnical Engineer prior to incorporation into the pavement structure. Aggregate base shall be moisture conditioned to within 2 percent of optimum and compacted to at least 95 percent compaction (ASTM D 1557).

**G. Concrete Slabs**

Any dedicated concrete walkways and driveways should be directly underlain by aggregate base per City of Reno standards. Decomposed granite, the same unit thickness as aggregate base, can be used in lieu of aggregate base under private walks and driveways. The concrete mix design for exterior concrete shall have a minimum of 6 sacks of Portland cement, with a maximum water to cement ratio of 0.45, and air content between 4.5 and 7.5 percent. This recommendation is to provide resistance to freeze-thaw cycles that occur in the Reno/Sparks area. Additional requirements for exterior concrete are as follows:

Minimum compression strength = 4,000 psi,

Maximum slump = 4”

Interior slab-on-grade and foundation concrete shall follow criteria established by the project structural engineer. Soluble sulfates have a detrimental effect on Portland cement concrete. Two samples were taken from on-site yielded results of <0.01 percent water soluble sulfate (Sheet 25). Therefore, the sulfate exposure is ranked “Negligible”.

**TABLE 1904.3**

**REQUIREMENTS FOR CONCRETE EXPOSED TO SULFATE-CONTAINING SOLUTIONS**

SULFATE EXPOSURE	WATER SOLUBLE SULFATE (SO <sub>4</sub> ) IN SOIL, PERCENT BY WEIGHT	SULFATE (SO <sub>4</sub> ) IN WATER (ppm)	CEMENT TYPE  ASTM C150	CEMENT TYPE  ASTM C595	CEMENT TYPE  ASTM C1157	MAXIMUM WATER-CEMENTITIOUS MATERIALS RATIO, BY WEIGHT, NORMAL - WEIGHT AGGREGATE CONCRETE <sup>a</sup>	MINIMUM <i>f</i> <sub>c</sub> NORMAL-WEIGHT AND LIGHTWEIGHT AGGREGATE CONCRETE (psi) <sup>a</sup>
Negligible	0.00 – 0.10	0 - 150	-	-	-	-	-
Moderate	0.10 - 0.20	150 - 1,500	II	II, IP (MS),	MS	0.50	4,000

				IS(MS), P(MS), I(PM)(MS), I(SM)(MS)			
<b>Severe</b>	0.20 – 2.00	1,500 – 10,000	V	-	HS	0.45	4,500
<b>Very severe</b>	Over 2.00	Over 10,000	V plus pozzolan <sup>c</sup>	-	HS plus pozzolan <sup>d</sup>	0.45	4,500

For SI: 1 pound per square inch=0.00689 Mpa.

- a. A lower-water-cementitious materials ratio or higher strength may be required for low permeability or for protection against corrosion of embedded items or freezing and thawing (see Table 1904.2.2).
- b. Seawater.
- c. Pozzolan that has been determined by test or service record to improve sulfate resistance when used in concrete contain Type V cement.
- d. Pozzolan that has been determined by test or service record to improve sulfate resistance when used in concrete contain Type HS blended cement.

Structural concrete mix designs for interior and private improvements only should meet one of the following criteria:

<b>TYPE OF CEMENT</b>	<b>MINIMUM SACKS OF CEMENT PER CUBIC YARD</b> (prior to replacement with fly ash)	<b>MAXIMUM WATER TO CEMENTIOUS MATERIALS RATIO</b>
Type II	6	0.5
Type II and fly ash	5.5	0.53
Type IP	5.5	0.53
Type V	5.5	0.53
Type V and fly ash	5.5	0.53

Concrete mix designs shall be determined per Chapter 7 of “Design and Control of Concrete Mixtures” by the Portland Cement Association and as further modified by IBC 2012 standards, and submitted to the Geotechnical Engineer for approval at least one week prior to pouring the concrete.

Structural concrete mix designs for interior and private improvements only should meet one of the criteria found in the Portland Cement Association “Design and Control of Concrete Mixtures” Chapter 9, 2011.

The Reno area is in a climatic zone of low humidity and concrete is susceptible to shrinkage cracking and curling during curing. All concrete work shall follow the procedures of the American Concrete Institute.

## **H. Anticipated Construction Problems**

The site has a strong potential for dust generation, and will require constant dust suppression measures

during construction.

## **I. Infiltration Results**

Two infiltration pits were dug and infiltration tests performed to aid in sizing, design and analysis of drainage structure. Infiltration Pit 1, on the west side of the project, had an infiltration rate of 2 minutes per inch at 10 feet below surface grade. Infiltration Pit 2, on the east side of the project, had an infiltration rate of 7 minutes per inch at 6 feet below surface grade. Logs of the infiltration pits are found on sheets 19 and 20, results are presented in Appendix C.



## LIMITATIONS

This report is prepared solely for the use of Summit Engineering's client. Any entity wishing to utilize this report must obtain permission from them prior to doing so. Our services consist of professional opinions and recommendations made in accordance with generally accepted soil and foundation engineering principles and practices. The analyses and recommendations contained in this report are based on our site reconnaissance, the information derived from our field exploration and laboratory testing, our understanding of the proposed development, and the assumption that the soil conditions in the proposed building and grading areas do not deviate from the anticipated conditions.

Unanticipated variations in soil conditions could exist in unexplored areas on the site. If any soil or groundwater conditions are encountered at the site that are different from those discussed in this report, our firm should be immediately notified so that our recommendations can be modified to accommodate the situation. In addition, if the scope of the proposed construction, including proposed loads or structural location, changes from that described in this report, our firm should be notified.

Recommendations made in this report are based on the assumption that an adequate number of tests and inspections will be made during construction to verify compliance with these recommendations. Such tests and inspections should include, but not necessarily be limited to, the following:

- . Review of site construction plans for conformance with soils investigation.
- . Observation and testing during site preparation, grading, excavation and placement of fill.
- . Observation and testing of materials and placement of asphalt concrete and site concrete.
- . Foundation observation and review.
- . Consultation as may be required during construction.

The findings in this report are valid as of the present date; however, changes in the conditions of the property can occur with the passage of time, whether they are due to natural processes or to the works of man on this or adjacent lands. In addition, changes in applicable or appropriate standards occur, whether they result from legislation or from the broadening of knowledge. Accordingly, the findings in this report might be invalidated, wholly or partially, by changes outside of our control.

## REFERENCES

American Society of Civil Engineers, Online Hazard Tool: <https://asce7hazardtool.online/>

Manual of Concrete Practice, American Concrete Institute, 2008

Federal Emergency Management Agency, 2009, Flood Insurance Rate Map Washoe County, Nevada and Incorporated Areas: Maps 32031C280H and 32031C2825H.

International Code Council, 2018, International Conference of Building Officials.

Nevada Bureau of Mines and Geology: <http://www.nbmg.unr.edu>

Soeller, S.A., and Nielson, R.C., 1980, Geologic Map of the Reno NW Quadrangle, Nevada: Nevada Bureau of Mines and Geology

Standard Specifications for Public Works Construction 2016.

U.S. Geological Survey: <http://geohazards.usgs.gov/designmaps/us/application.php>

# APPENDIX A

**APPENDIX A**  
**SPECIFICATIONS FOR**  
**SITE PREPARATION, EXCAVATION, COMPACTION**  
**STRUCTURAL FILL AND SUBGRADE PREPARATION**

**1.0 GENERAL**

- 1.1** Standard Specifications - Where referred to in these specifications, "Standard Specifications" shall mean the Standard Specifications for Public Works Construction (2016 edition).
- 1.2** Scope - All work shall be done in accordance with the Standard Specifications except as may be modified by the specifications outlined below. The work done under these specifications shall include clearing, stripping, removal of unsuitable material, excavation and preparation of natural soil, placement and compaction of on-site and/or imported fill material, or as specifically referred to in the plans or specifications.
- 1.3** Geotechnical Engineer - When used herein, Geotechnical Engineer shall mean the engineer or a representative under the engineer's supervision. The work covered by these specifications shall be inspected by a Geotechnical Engineer, who shall be retained by the Owner. The Geotechnical Engineer will be present during the site preparation and grading to inspect the work and to perform the tests necessary to evaluate material quality and compaction. The Geotechnical Engineer shall submit a report to the Owner, including a tabulation of all tests performed.
- 1.4** Soils Report - A "Geotechnical Investigation" report, prepared by Summit Engineering Corporation, is available for review and may be used as a reference to the surface and subsurface soil and groundwater conditions on these projects. The Contractor shall make his own interpretation with regards to the methods and equipment necessary to perform the excavations.



**1.5** Percent Relative Compaction - Where referred to herein, percent relative compaction shall mean the in-place dry unit weight of soil expressed as a percentage of the maximum dry unit weight of the same material, as determined by ASTM D-1557, laboratory compaction test procedure. Optimum moisture content is the moisture content corresponding to the maximum dry density determined by ASTM D-1557.

## **2.0 SITE PREPARATION AND EARTHWORK**

**2.1** All earthwork and site preparation should be performed in accordance with the requirements of this report and attached specifications, and the Standard Specifications.

**2.2** Clearing - Areas to be graded shall be cleared of brush and debris. These materials shall be removed from the site and discarded by an acceptable means approved by the owner.

**2.3** Stripping - Surface soils containing roots and organic matter shall be stripped from areas to be graded and stockpiled or discarded as specified by the plans and specifications or at the discretion of the owner. Strippings may be used as the final lift of fill for areas to be planted.

**2.4** Dust Control - The contractor shall prevent and maintain control of all dust generated during construction in compliance with all federal, state, county, and city regulations. The project specifications should include an indemnification by the contractor of the engineer and owner for all dust generated during the entire construction period.

**2.5** Materials - All material not suitable for use as structural fill, shall be removed from the sites by the Contractor, or placed in non-structural fill areas. The Geotechnical Engineer shall determine the suitability of material for reuse as structural fill.

**2.6** Ground Surface - The ground surface exposed by stripping and/or excavation shall be scarified to a minimum depth of 12 inches, moisture conditioned, by aerating or adding water, to within 2 percent of optimum moisture content and compacted to 90 percent relative compaction, unless otherwise specified. Compaction of the ground surface shall be approved by the Geotechnical Engineer prior to placement of fill, structural fill, aggregate base, and/or Portland cement concrete.

2.7 Backfill of test pits and trenches – Our exploration pits and trenches were backfilled without mechanical compaction. In structural areas, backfill in the pits should be removed and replaced in lifts with compactive effort.

### 3.0 **FILL MATERIAL**

3.1 Fill material shall be free of perishable, organic material. Rock used in the fill shall be placed in such a manner that no voids are present, either between or around the rock, after compacting the layer.

3.2 Structural Fill Material (SSPWC) - Material shall consist of suitable non-expansive soils having a plasticity index less than 12, and a minimum “R”-value of 30. The gradation requirements shall be as follows:

<u>Sieve Sizes</u>	<u>Percentage Passing (by weight)</u>
4"	100
3/4"	70 - 100
#40	15 - 50
#200	10 - 30

Materials not meeting the above requirements may be suitable for use as structural cap material at the discretion of the Geotechnical Engineer. Samples of imported fill proposed for use as structural cap material shall be submitted to the Geotechnical Engineer and approved before it is delivered to a site.

3.3 Rock Fill - Fill material containing over 30 percent (by weight) of rock larger than 3/4 inches in greatest dimension is defined as rock fill. Rock Fill located five or more feet below finished grade may be constructed in loose lifts up to the maximum size of the rock in the material but not exceeding diameters of 18 inches. The voids around the rock in each rock fill lift shall be filled with granular material and fines and compacted to the satisfaction of the Geotechnical Engineer. Rocks larger than 18 inches in diameter shall be placed in non-structural areas or in deep fills at the discretion of the geotechnical engineer. Care should be taken to fill all voids with finer grained materials. No nesting of larger rocks shall be allowed. Rock fill shall not be used for slab-on-grade construction without the approval of the Geotechnical Engineer. The maximum allowable particle size shall be

decreased by the Geotechnical Engineer if the achieved compaction is not satisfactory to the Geotechnical Engineer or “nesting” is observed by the Geotechnical Engineer.

#### **4.0 EARTHWORK AND FILL PLACEMENT**

- 4.1** Placement - Fill material shall be placed in layers that shall not exceed 12 inches of compacted thickness, unless otherwise approved by the Geotechnical Engineer. Each layer shall be evenly spread and moisture conditioned to within 2 percent of optimum moisture content. Unless otherwise specified, each layer of earth fill shall be compacted to 90 percent relative compaction. Compaction shall be approved by the Geotechnical Engineer. Rock fill shall be placed in accordance with the appropriate sections of the Standard Specifications. Rock fill placement and compaction shall be approved by the Geotechnical Engineer. Full time inspection of fill placement is required in structural areas and areas designated as dedicated improvement for the City of Reno, unless otherwise approved by the Engineer.
- 4.2** Keyways - Where the fill extends onto native slopes with gradients greater than 5:1, the fill shall be keyed into the native soils. The keys will have a minimum width of equipment width or 10 feet, whichever is lesser, and constructed with a minimum 5 percent slope into the hillside.
- 4.3** Compaction Equipment - The Contractor shall provide and use equipment of a type and weight suitable for the conditions encountered in the field. The equipment shall be capable of obtaining the required degree of compaction in all areas including those that are inaccessible to ordinary rolling equipment.
- 4.4** Reworking - When, in the judgment of the Geotechnical Engineer, sufficient compaction effort has not been used, or where the field density tests indicate that the required compaction or moisture content has not been obtained, subgrade and/or fill materials shall be reworked and compacted as needed to obtain the required density and moisture content. This reworking shall be accomplished prior to the placement of fill, structural fill, aggregate base, and/or Portland cement concrete.

- 4.5** Unstable Areas - If pumping or other indications of instability are noted, fill and/or subgrade materials shall be evaluated by the Geotechnical Engineer, scarified, left to dry, and re-compacted or removed and replaced as needed to obtain the required density and moisture content. This work shall be accomplished prior to the placement of fill, structural fill, aggregate base, and/or Portland cement concrete.
- 4.6** Frozen Materials – Fill shall not be placed on frozen materials, nor shall frozen material be utilized as fill.

## **5.0 EXCAVATION AND SLOPE REQUIREMENTS**

- 5.1** Finished cut slopes shall not exceed 2 horizontal to 1 vertical and fill slopes should not exceed ratios of 2 horizontal to 1 vertical. Slopes steeper than three horizontal to one vertical or more than ten feet in height should be protected from erosion using riprap, vegetation, or a similar designated and acceptable means meeting the applicable standards.
- 5.2** Temporary, unsupported construction slopes less than ten feet in height may stand at a slope as steep as 1:1 (H:V) provided that the length of the unsupported slope does not exceed twenty feet. These temporary slopes should not remain unsupported for extended periods of time.

## **6.0 FOUNDATIONS AND FOOTING**

- 6.1** Spread type continuous and column footings should be designed, to impose a maximum net dead plus long-term live load of **2,000 pounds per square foot**. Net bearing pressures of up to one-third in excess of the given bearing value are permitted for transient live loads from wind and earthquake.
- 6.2** Exterior footings should be embedded a minimum of 24 inches below the lowest adjacent final compacted subgrade to provide adequate frost protection and confinement. Isolated interior footings should be imbedded per IBC requirements. The recommendations of this report are applicable to all footings.
- 6.3** The design coefficient of friction is 0.25. The passive soil pressure was calculated as 150 pounds per cubic foot (150 psf per foot of depth). The active soil pressure was similarly



was calculated as 45 pounds per cubic foot. The at-rest soil pressure, when walls are braced on the top and the bottom, was calculated as 60 pounds per cubic foot. These design values assume the non-expansive granular soils that meet parameters for structural fill are providing vertical and lateral support. All exterior footings shall be embedded a minimum 24 inches below adjacent finished grade for frost protection, and a minimum of four feet above groundwater.

**6.4** Backfill of footing excavations or formed footings should be moisture conditioned to within 2 percent of optimum moisture content and compacted to a minimum of 90 percent relative compaction.

**6.5** All footing excavations should be clear of loose material prior to placement of concrete. The bottom of the footing excavation should be scarified to a depth of 12 inches, moisture conditioned to within 2 percent of optimum moisture content, and compacted to a minimum of 90 percent relative compaction.

**7.0 UTILITY TRENCH BACKFILL**

**7.1** Bedding Material - Bedding material shall meet one of the following gradation requirements listed below and shall be non-plastic:

Bedding will require import to meet one of the following specifications:

	<b>CLASS A BACKFILL</b>	<b>CLASS B BACKFILL</b>	<b>CLASS C BACKFILL</b>
<b>SIEVE SIZE</b>	<b>% PASSING</b>	<b>%PASSING</b>	<b>% PASSING</b>
1"	-	-	100
¾"	-	-	90-100
½"	-	100	-
3/8"	100	-	10-55
#4	90-100	0-15	0-10
#50	10-40	-	-
#100	3-20	-	-
#200	0-15	0-3	-

Bedding as defined in this report shall be within 6 inches of the bottom of the pipe, within 12 inches of the sides of the pipe, and within 12 inches, or to a depth required from the top of the pipe to the top of the groundwater table, whichever is greater, over the pipe. Where groundwater is encountered, filter fabric or filter material shall encapsulate the bedding, if Class B or Class C backfill is utilized. The filter fabric shall be a 10 oz./sq. yd. non-woven geotextile.

Individual utility companies may have additional specifications, which should also be followed.

**7.2** Placement and Compaction - Bedding material shall first be placed so that the pipe is supported for the full length of the barrel with full bearing on the bottom segment of the pipe equal to a minimum of 0.4 times the outside diameter of the barrel. Bedding shall also extend to one foot above the top of the pipe. Pipe bedding within 6 inches of the pipe shall be placed in thin layers not exceeding 8 inches in loose thickness, conditioned to the proper moisture content for compaction. Class A backfill shall be compacted to at least 90 percent relative compaction. Class B and/or C backfill shall be compacted to the satisfaction of the Geotechnical Engineer. All other trench backfill shall be placed in thin layers not exceeding 8 inches in loose thickness, conditioned to within 2 percent of optimum moisture content, and compacted as required for adjacent fill, or if not specified, to at least 90 percent compaction in areas under structures, utilities, roadways, parking areas, and concrete flatwork.

**7.3** Drain Rock - Any necessary subsurface drainage systems shall use drain rock conforming to the following Class C gradation:

<u>Sieve Sizes</u>	<u>Percentage Passing (by weight)</u>
1"	100
3/4"	90-100
3/8"	10-55
#4	0-10

**8.0 CONCRETE SLAB-ON-GRADE AND FLATWORK CONSTRUCTION**

**8.1** Slab-on-grade - When used in this report, slab-on-grade shall refer to all interior concrete floors.

- 8.2** Concrete flatwork - A general term, flatwork refers to all exterior concrete site work including sidewalks, driveways, curb and gutters, and patios.
- 8.3** Subgrade - The upper twelve inches of subgrade beneath the aggregate base under concrete flatwork and slabs-on-grade shall be scarified, moisture conditioned to within 2 percent of optimum moisture content, and compacted to 90 percent relative compaction. Compaction shall be approved by the Geotechnical Engineer.
- 8.4** Concrete Mix Design - The contractor shall submit a concrete mix design to the Geotechnical Engineer for review and approval 1 week prior to placement of any concrete. The exterior concrete mix design shall utilize a minimum of 6 sacks of Portland Cement Concrete and a maximum water cement ratio of 0.45. Exterior concrete shall also meet the following specifications:

Minimum 28 day compressive strength = 4000 psi.

Air content = 4.5 – 7.5%

Maximum slump = 4 inches

Interior concrete mix designs shall comply with the structural plans and the tables included in Section G of this report.

Admixtures - All admixtures incorporated in the mix design shall be approved by the Geotechnical Engineer.

Finishing - All finishing shall be done in the absence of bleed water. No water shall be added to placed concrete during finishing.

- 8.5** Over-excavation - Soils within three feet of flatwork or five feet of slab-on-grade shall be over-excavated. Over-excavations should extend at least two feet laterally beyond the edge of the flatwork/slab-on-grade section.
- 8.6** Base - Base material shall be compacted to 95 percent relative compaction. Compaction shall be approved by the Geotechnical Engineer. Type II Class B aggregate base meeting the following requirements shall be used:

Gradation Requirements

<u>Sieve Size</u>	<u>Percentage Passing (by weight)</u>
1"	100
3/4"	90-100
#4	35-65
#16	15-40
#200	2-10

Plasticity Index should meet the following requirements:

<u>Percentage Passing #200 (by weight)</u>	<u>Plasticity Index Maximum</u>
0.1 to 3.0	15
3.1 to 4.0	12
4.1 to 5.0	9
5.1 to 8.0	6
8.0 to 11.0	4

Other Requirements

R-value	Minimum of 70
Fractured faces	Minimum of 35%
LA Abrasion	Maximum of 45%
Liquid Limit	Maximum of 35%

- 8.7** Concrete slab-on-grade thickness and compressive strength requirements shall be in accordance with design criteria provided by the Structural Engineer. Minimum slab thickness and compressive strength for flatwork shall be in accordance with the applicable requirements.
  
- 8.8** Concrete work shall conform to all requirements of ACI 301-2008, Specifications for Structural Concrete for Buildings, except as modified by supplemental requirements.
  
- 8.9** To facilitate curing of the slab, base materials shall be kept moist until placement of the concrete.
  
- 8.10** Excessive slump (high water cement ratio) of the concrete and/or improper curing procedures used during hot or cold weather could lead to excessive shrinkage, cracking or curling of slabs and other flatwork.

## **9.0 RETAINING WALLS**

- 9.1** Retaining walls should be designed using a passive pressure calculated as 150 pounds per cubic foot and active soil pressure calculated as 45 pounds per cubic foot. A base coefficient of 0.25 should be used for resistance to sliding.
- 9.2** Footings should be placed at least 24 inches below the lowest adjacent finished grade. Subgrade shall be prepared as per these specifications.
- 9.3** In addition to active soil pressures the effects of any surcharge from adjacent structures or roadways should be included in calculating lateral pressures on retaining walls.
- 9.4** The design pressures given assume the soils retained are granular, non-expansive and free draining.
- 9.5** Retaining wall backfill should be moisture conditioned to within 2 percent of optimum and compacted to 85 percent in non-structural areas and 90 percent in structural areas. The use of heavy compaction equipment could cause excessive lateral pressures, which may cause failure of the wall.
- 9.6** Installation of weep holes or a continuous drain along the base of the wall is recommended to prevent water from being retained behind the wall.
- 9.7** An interceptor swale should be provided at the top of all retaining walls.

## **10.0 ASPHALTIC CONCRETE PAVEMENT**

- 10.1** Material and Procedure - The asphalt-concrete material and placement procedures shall conform to appropriate sections of the "Standard Specifications". Aggregate materials for asphaltic concrete shall conform to the requirements listed for Type 3 aggregate in Section 200.02.02 of the "Standard Specifications, 2016". A Type 3, 50-blow, Marshall mix design with 2 to 4 percent air voids is recommended for all areas. PG64-28NV is also recommended for this project. The Contractor shall submit proposed asphalt-concrete mix



designs to the Geotechnical Engineer for review and approval 1 week prior to paving. Asphalt materials should be compacted to a minimum of 92 percent of its theoretical maximum specific gravity or 96 percent of its Marshall density.

**10.2** Subgrade Preparation - After completion of the utility trench backfill and prior to the placement of aggregate base, the upper 12 inches of finished subgrade soil or structural fill material shall be moisture conditioned to at within 2 percent of optimum and compacted to at least 90 percent. This may require scarifying, moisture conditioning and compacting.

**10.3** Aggregate Base Rock - After the subgrade and/or structural fill is properly prepared, the aggregate base material shall be placed uniformly on the approved areas. Aggregate base shall be placed in such a manner as to prevent segregation of the different sizes of material and any such segregation, unless satisfactorily corrected, shall be cause for rejection at the discretion of the Geotechnical Engineer. The aggregate base material shall be spread for compaction in layers not to exceed six inches; moisture conditioned to within 2 percent of optimum, and compacted to at least 95 percent compaction. Aggregate base materials shall meet the requirements of Section 200.01.03 of the "Standard Specifications, 2016" for Type 2, Class B aggregate base. The aggregate base materials shall be approved by the Geotechnical Engineer prior to incorporation into the pavement structure.

## **11.0 SEISMIC DESIGN**

**11.1** Design of structures should include an allowance for earthquake loading. Structures should be designed in conjunction with IBC 2012 criteria for seismic acceleration of 0.509 g in soil profiles.

**APPENDIX B**  
**FLEXIBLE PAVEMENT SECTION**



# 1993 AASHTO Pavement Design

## DARWin Pavement Design and Analysis System

A Proprietary AASHTOWare  
Computer Software Product

### Flexible Structural Design Module

Village Parkway Townhome  
ADT=5,000  
R-Value=0  
4 inches AC on 12 Inches cement treated base on 20" Pit Run (Structural Fill)

### Flexible Structural Design

18-kip ESALs Over Initial Performance Period	240,186
Initial Serviceability	4.2
Terminal Serviceability	2
Reliability Level	85 %
Overall Standard Deviation	0.45
Roadbed Soil Resilient Modulus	772 psi
Stage Construction	1
 Calculated Design Structural Number	 5.50 in

### Specified Layer Design

<u>Layer</u>	<u>Material Description</u>	Struct Coef. <u>(Ai)</u>	Drain Coef. <u>(Mi)</u>	Thickness <u>(Di)(in)</u>	Width <u>(ft)</u>	Calculated <u>SN (in)</u>
1	4" AC	0.39	1	4	12	1.56
2	12" Cement Treated Base	0.23	1	12	12	2.76
3	20" Pit Run (Structural Fill)	0.06	1	20	12	1.20
Total	-	-	-	36.00	-	5.52

**APPENDIX C**  
**INFILTRATION RESULTS**



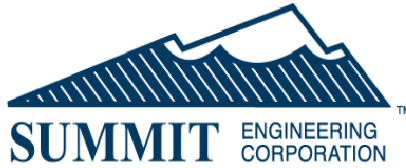
**SUMMIT ENGINEERING CORPORATION**  
**PERC RATE TEST**

<b>PROJECT NAME:</b>	Village Parkway Townhomes	<b>PROJECT NUMBER:</b>	31097
<b>TEST SPECIFICATIONS:</b>	Infiltration	<b>DATE:</b>	1/19/2021
<b>TECHNICIAN:</b>	JB		

<b>Hole No.</b>	IF-2	<b>Perc Rate:</b>	7	min/in	
<b>Depth from native ground to gravel:</b>	6 ft.				
<b>Soil Description:</b>	ML w/sand				
<b>Notes:</b>					
Time	Initial Depth (in)	Final Depth (in)	Inches Drop (in)	Time Interval	Min/in
9:49	6	11 4/16	5 4/16	15	2.9
10:05	6	9 9/16	3 9/16	15	4.2
10:20	6	8 15/16	2 15/16	15	5.1
10:35	6	8 8/16	2 8/16	15	6.0
10:50	6	8 3/16	2 3/16	15	6.9
11:05	6	8 2/16	2 2/16	15	7.1
11:20	6	8 2/16	2 2/16	15	7.1

<b>Hole No.</b>	IF-1	<b>Perc Rate:</b>	2	min/in	
<b>Depth from native ground to gravel:</b>	10 ft.				
<b>Soil Description:</b>	SM w/grvl				
<b>Notes:</b>					
Time	Initial Depth (in)	Final Depth (in)	Inches Drop (in)	Time Interval	Min/in
9:29	2	11 10/16	9 10/16	15	1.6
9:45	2	10 6/16	8 6/16	15	1.8
10:15	2	9 5/16	7 5/16	15	2.1
10:30	2	8 15/16	6 15/16	15	2.2
10:45	2	8 11/16	6 11/16	15	2.2
11:00	2	8 10/16	6 10/16	15	2.3
11:15	2	8 10/16	6 10/16	15	2.3

**APPENDIX D**  
**LABORATORY RESULTS**



Engineering The West Since 1978.

5405 Mae Anne Avenue  
Reno Nevada 89523

Phone (775) 747-8550 Fax (775) 747-8559

**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3371.0</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3277.6</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>2.8%</b>
DATE:	<b>1/27/2021</b>	WASH WEIGHT(g):	<b>1777.8</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-1, 5-6'</b>	CC:	1.07
		CU:	8.06
PI:	<b>NP</b>	SOIL CLASSIFICATION:	<b>SM</b>
LL:		SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>98</b>
		% PASSING #200:	<b>12.6</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		7.7		0.4	100	
#4		39.3		2.2	98	
#8		170.5		9.6	90	
#10		211.7		11.9	88	
#16		385.6		21.7	78	
#30		621.4		35.0	65	
#40		790.1		44.4	56	
#50		975.6		54.9	45	
#100		1330.6		74.8	25	
#200		1553.1		87.4	12.6	
PAN		1627.5				

NOTES:



Engineering The West Since 1978.

5405 Mae Anne Ave  
Reno, NV 89523

Phone (775) 747-8550 Fax (775) 747-8559

**Grading Analysis (ASTM C-136)**

JOB NAME: Woodland Village Town Homes      DATE: 1/28/2021  
 JOB NUMBER: 31097      TECHNICIAN: MC  
 LAB NUMBER: 2529

TOTAL COARSE WEIGHT 921.1      BEFORE WASH WEIGHT 1944.0  
 TOTAL WET FINE WIGHT 3954.1      FINE WET WEIGHT 3954.1  
 TOTAL DRY SAMPLE WIEGHT 4767.3      FINE DRY WEIGHT 3846.2  
 SIEVE FINE AND COARSE SPLIT 3/4      PERCENT MOISTURE 2.8

PI: 4.3

CU: 26.00

LL: 21.9

CC: 0.96

UCS CLASSIFICATION: SM w/grvl

SOIL NAME: Silty Sand with gravel

SIEVE	COARSE GRADATION			FINE GRADATION			COMBINED GRADATION	SPEC
	WEIGHT RETAINED	PERCENT RETAINED	PERCENT PASSING	WEIGHT RETAINED	PERCENT RETAINED	PERCENT PASSING		
6								
5								
4"								
3"	555.0	12	88				88	
2"	741.0	16	84				84	
1 1/2"	741.0	16	84				84	
1"	890.2	19	81				81	
3/4"	921.1	19	81				81	
1/2"				100.5	5	95	77	
3/8"				199.8	10	90	72	
#4				365.0	19	81	66	
#8				527.7	27	73	59	
#10				569.9	29	71	57	
#16				685.0	35	65	52	
#30				802.2	41	59	47	
#40				849.9	44	56	45	
#50				893.2	46	54	44	
#100				1037.5	53	47	38	
#200				1031.7	53	46.9	37.9	
PAN				1057.1	54			

Notes: TP-2, 3-4'



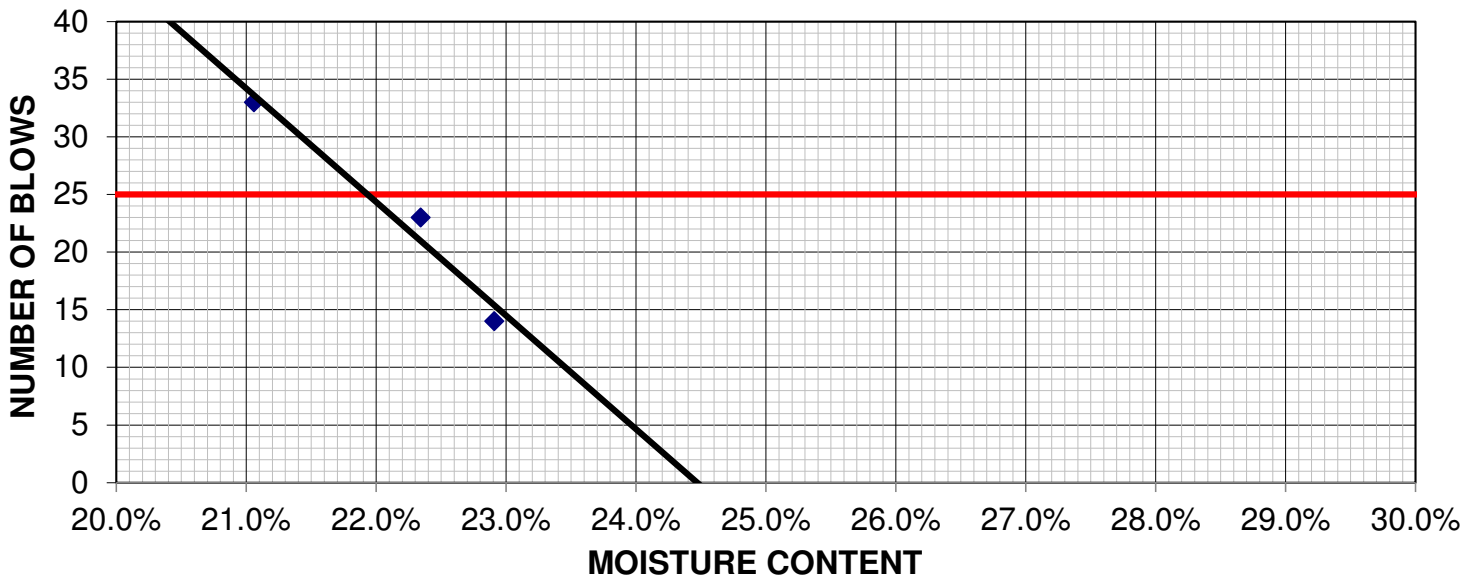
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/28/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-2, 3-4'

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 21.9  
 PLASTIC LIMIT: 17.6  
 PLASTICITY INDEX: 4.3

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	14	23	33
TARE NO.	l1	Q	T		B	Z	G
GROSS WET WEIGHT	7.71	7.24	7.97		12.13	12.81	13.92
GROSS DRY WEIGHT	7.05	6.72	7.36		10.46	11.15	12.17
TARE WEIGHT	3.25	3.84	3.86		3.17	3.72	3.86
NET DRY WEIGHT	3.80	2.88	3.50		7.29	7.43	8.31
WEIGHT OF WATER	0.66	0.52	0.61		1.67	1.66	1.75
% MOISTURE	17.37%	18.06%	17.43%		22.91%	22.34%	21.06%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_  
 \_\_\_\_\_





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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3278.3</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3152.2</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>4.0%</b>
DATE:	<b>1/28/2021</b>	WASH WEIGHT(g):	<b>1719.1</b>
TECHNICIAN:	<b>MC</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-3, 2.5-3.5'</b>	CC:	6.29
		CU:	5.77
PI:	<b>1.4</b>	SOIL CLASSIFICATION:	<b>SM</b>
LL:	<b>22.3</b>	SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>99</b>
		% PASSING #200:	<b>19.6</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		9.4		0.5	99	
#8		88.4		5.1	95	
#10		138.5		8.1	92	
#16		303.8		17.7	82	
#30		505.6		29.4	71	
#40		611.8		35.6	64	
#50		729.7		42.4	58	
#100		1079.0		62.8	37	
#200		1382.4		80.4	19.6	
PAN		1520.7				

NOTES:



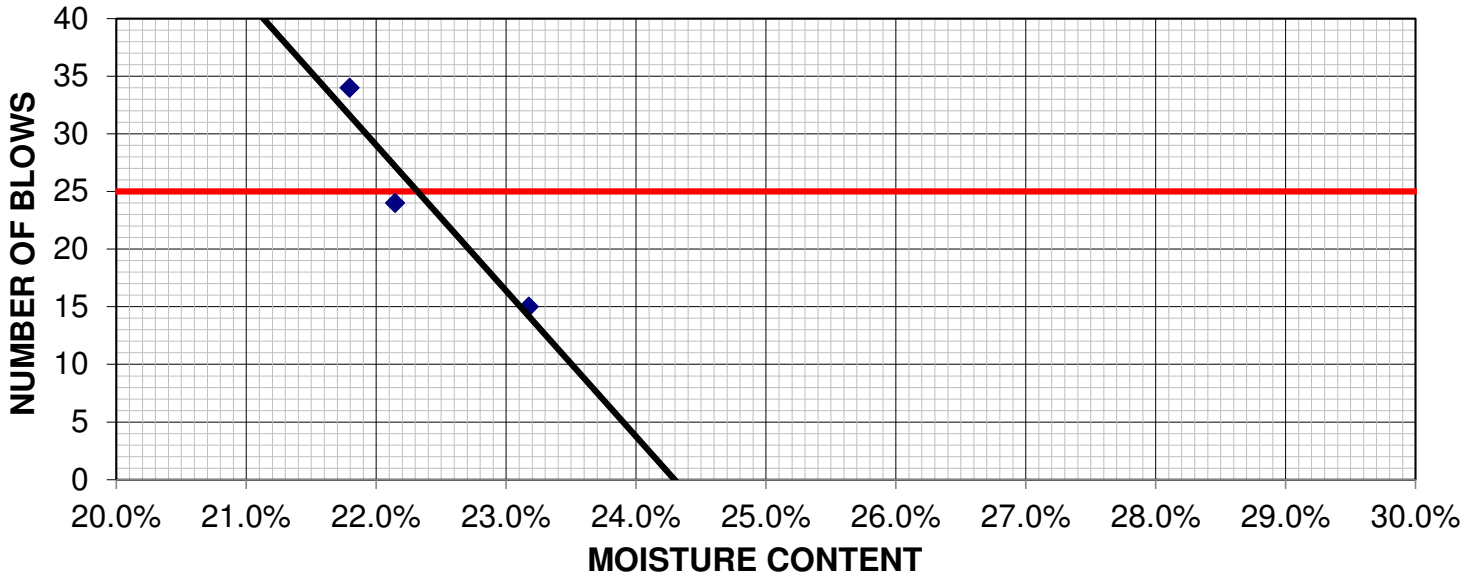
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/28/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-3, 2.5-3.5'

**Liquid and Plastic Limit (ASTM D 4318)**

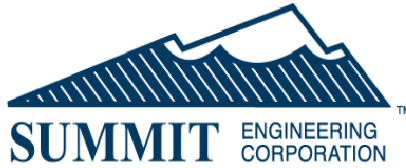
LIQUID LIMIT: 22.3  
 PLASTIC LIMIT: 20.9  
 PLASTICITY INDEX: 1.4

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	15	24	34
TARE NO.	L	W	F		D	C	P
GROSS WET WEIGHT	8.49	7.25	7.25		12.60	10.13	14.03
GROSS DRY WEIGHT	7.68	6.64	6.59		10.95	8.87	12.21
TARE WEIGHT	3.78	3.88	3.28		3.83	3.18	3.86
NET DRY WEIGHT	3.90	2.76	3.31		7.12	5.69	8.35
WEIGHT OF WATER	0.81	0.61	0.66		1.65	1.26	1.82
% MOISTURE	20.77%	22.10%	19.94%		23.17%	22.14%	21.80%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_  
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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland VillageTownhomes</b>	WET WEIGHT (g):	<b>4116.2</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>4027.9</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>2.2%</b>
DATE:	<b>1/25/2021</b>	WASH WEIGHT(g):	<b>1158.2</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-4, 7.5-8.5'</b>	CC:	2.78
		CU:	7.83
PI:	<b>NP</b>	SOIL CLASSIFICATION:	<b>SW</b>
		% PASSING #4:	<b>88</b>
LL:		SOIL NAME:	<b>Well Graded Sand</b>
		% PASSING #200:	<b>4.2</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		30.7		2.7	97	
3/8"		49.4		4.3	96	
#4		144.5		12.5	88	
#8		447.3		38.6	61	
#10		573.1		49.5	51	
#16		882.0		76.2	24	
#30		1011.0		87.3	13	
#40		1029.8		88.9	11	
#50		1051.7		90.8	9	
#100		1092.6		94.3	6	
#200		1109.7		95.8	4.2	
PAN		1111.1				

NOTES:



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### Grading Analysis (ASTM C-136)

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3246.3</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3120.7</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>4.0%</b>
DATE:	<b>1/28/2021</b>	WASH WEIGHT(g):	<b>1775.8</b>
TECHNICIAN:	<b>JB</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-5, 2-3'</b>	CC:	0.85
		CU:	10.48
PI:	4.9	SOIL CLASSIFICATION:	<b>SW</b>
LL:	24.5	SOIL NAME:	<b>Well Graded Sand</b>
		% PASSING #4:	<b>92</b>
		% PASSING #200:	<b>4.4</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"		12.0			100	
1/2"		28.9		1.6	98	
3/8"		50.2		2.8	97	
#4		141.7		8.0	92	
#8		512.3		28.8	71	
#10		638.5		36.0	64	
#16		899.3		50.6	49	
#30		1157.6		65.2	35	
#40		1304.6		73.5	27	
#50		1460.4		82.2	18	
#100		1608.5		90.6	9	
#200		1697.9		95.6	4.4	
PAN		1715.1				

NOTES:



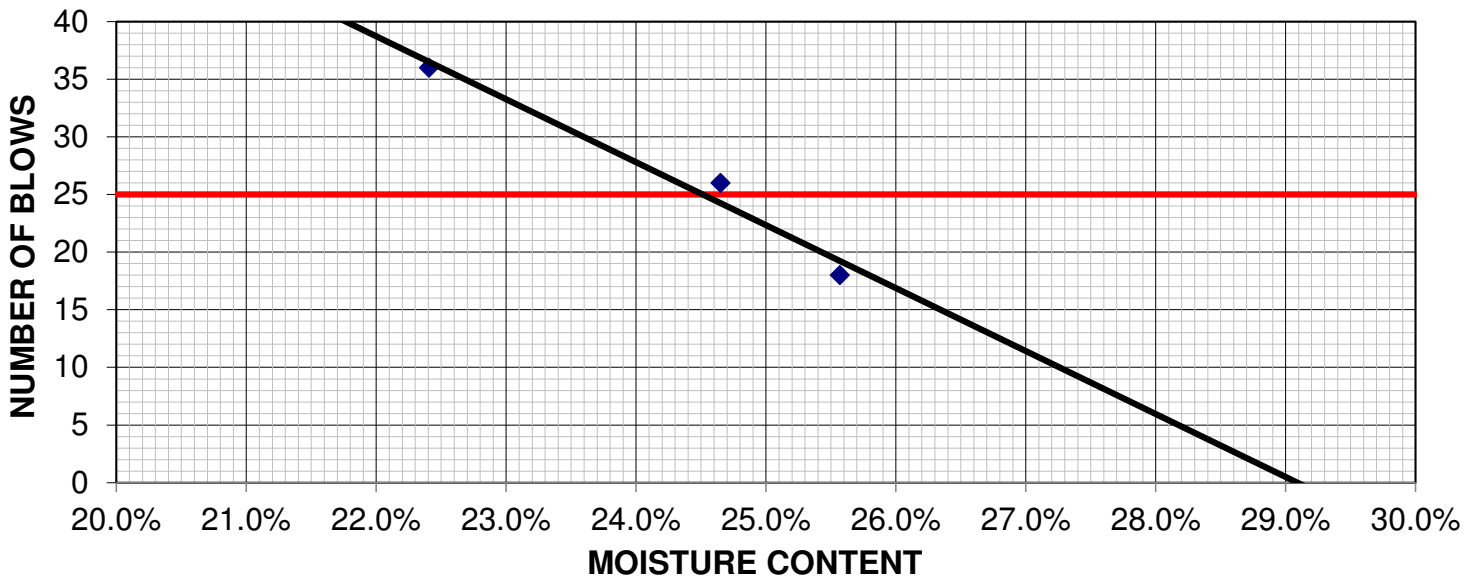
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/28/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-5, 2-3'

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 24.5  
 PLASTIC LIMIT: 19.6  
 PLASTICITY INDEX: 4.9

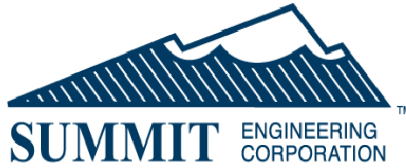
DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	18	26	36
TARE NO.	k	X	E		J1	G1	Y
GROSS WET WEIGHT	6.08	6.91	6.45		10.55	11.08	9.08
GROSS DRY WEIGHT	5.61	6.37	6.03		9.20	9.49	8.00
TARE WEIGHT	3.16	3.80	3.77		3.92	3.04	3.18
NET DRY WEIGHT	2.45	2.57	2.26		5.28	6.45	4.82
WEIGHT OF WATER	0.47	0.54	0.42		1.35	1.59	1.08
% MOISTURE	19.18%	21.01%	18.58%		25.57%	24.65%	22.41%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_  
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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3120.2</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>2851.1</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>9.4%</b>
DATE:	<b>1/27/2021</b>	WASH WEIGHT(g):	<b>1508.1</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-6, 6.5-7.5'</b>	CC:	0.53
		CU:	20.53
PI:	<b>1.4</b>	SOIL CLASSIFICATION:	<b>SM</b>
LL:	<b>23.7</b>	SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>92</b>
		% PASSING #200:	<b>37.0</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		122.6		8.1	92	
#8		230.5		15.3	85	
#10		251.9		16.7	83	
#16		330.0		21.9	78	
#30		436.3		28.9	71	
#40		514.3		34.1	66	
#50		628.2		41.7	58	
#100		781.6		51.8	48	
#200		950.7		63.0	37.0	
PAN		1072.2				

NOTES:



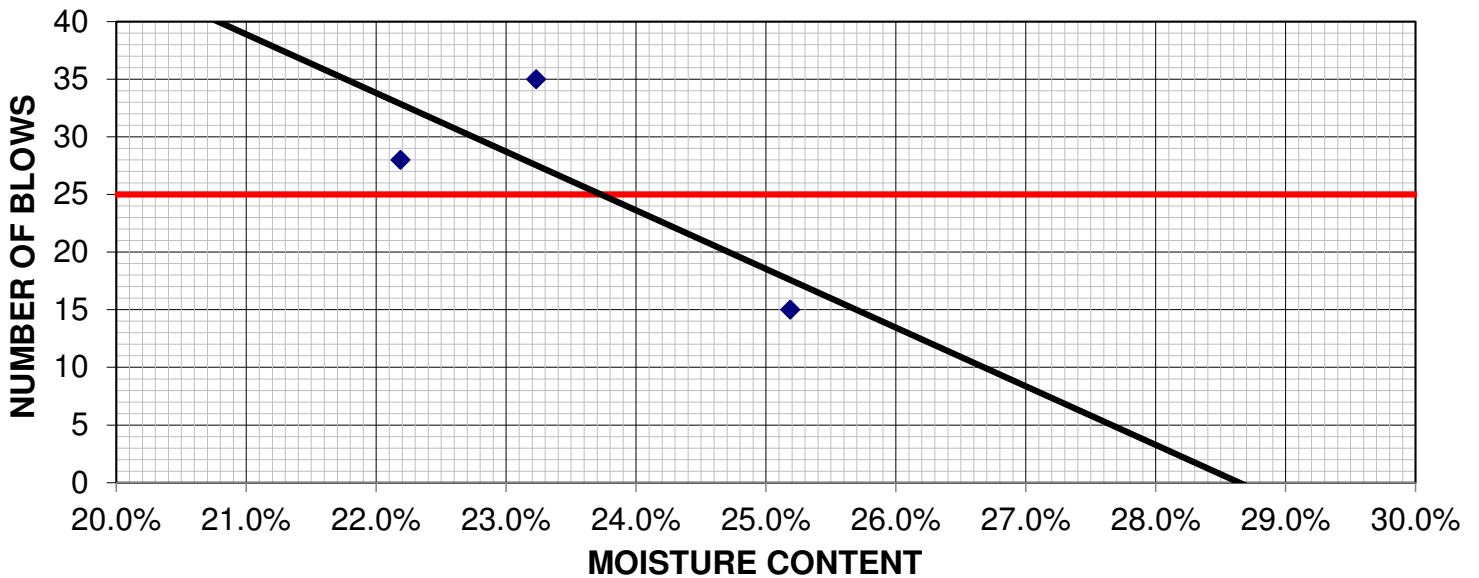
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/27/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-6, 6.5-7.5'

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 23.7  
 PLASTIC LIMIT: 22.3  
 PLASTICITY INDEX: 1.4

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	15	28	35
TARE NO.	K	R	Y		J1	V	G1
GROSS WET WEIGHT	7.88	6.73	7.14		12.32	10.86	11.58
GROSS DRY WEIGHT	7.02	6.07	6.43		10.63	9.46	9.97
TARE WEIGHT	3.16	3.16	3.18		3.92	3.15	3.04
NET DRY WEIGHT	3.86	2.91	3.25		6.71	6.31	6.93
WEIGHT OF WATER	0.86	0.66	0.71		1.69	1.40	1.61
% MOISTURE	22.28%	22.68%	21.85%		25.19%	22.19%	23.23%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_  
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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3871.1</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3709.5</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>4.4%</b>
DATE:	<b>1/27/2021</b>	WASH WEIGHT(g):	<b>1175.2</b>
TECHNICIAN:	<b>JB</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-7, 7.0-7.5'</b>	CC:	0.78
		CU:	23.57
PI:	<b>NP</b>	SOIL CLASSIFICATION:	<b>SW-SM</b>
LL:		SOIL NAME:	<b>Well Graded Sand- Silty Sand</b>
		% PASSING #4:	<b>97</b>
		% PASSING #200:	<b>11.4</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		34.5		2.9	97	
#8		277.8		23.6	76	
#10		354.0		30.1	70	
#16		558.0		47.5	53	
#30		696.6		59.3	41	
#40		761.0		64.8	35	
#50		819.6		69.7	30	
#100		932.7		79.4	21	
#200		1041.2		88.6	11.4	
PAN		1068.3				

NOTES:



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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>4203.3</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3988.7</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>5.4%</b>
DATE:	<b>1/26/2021</b>	WASH WEIGHT(g):	<b>1504.4</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-8, 6-6.5'</b>	CC:	0.80
		CU:	11.90
PI:	<b>NP</b>	SOIL CLASSIFICATION:	<b>SM</b>
LL:		SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>98</b>
		% PASSING #200:	<b>20.8</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		28.1		1.9	98	
#8		158.1		10.5	89	
#10		205.7		13.7	86	
#16		369.1		24.5	75	
#30		553.0		36.8	63	
#40		665.5		44.2	56	
#50		797.3		53.0	47	
#100		999.3		66.4	34	
#200		1191.1		79.2	20.8	
PAN		1291.7				

NOTES:



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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3007.0</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>2794.4</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>7.6%</b>
DATE:	<b>1/27/2021</b>	WASH WEIGHT(g):	<b>1287.0</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-9, 4.5-5.0'</b>	CC:	0.65
		CU:	5.09
PI:	<b>6.1</b>	SOIL CLASSIFICATION:	<b>SM</b>
LL:	<b>29.8</b>	SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>100</b>
		% PASSING #200:	<b>43.4</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		2.6		0.2	100	
#8		10.9		0.8	99	
#10		14.2		1.1	99	
#16		36.7		2.9	97	
#30		101.8		7.9	92	
#40		161.2		12.5	87	
#50		240.9		18.7	81	
#100		452.1		35.1	65	
#200		728.0		56.6	43.4	
PAN		918.6				

NOTES:





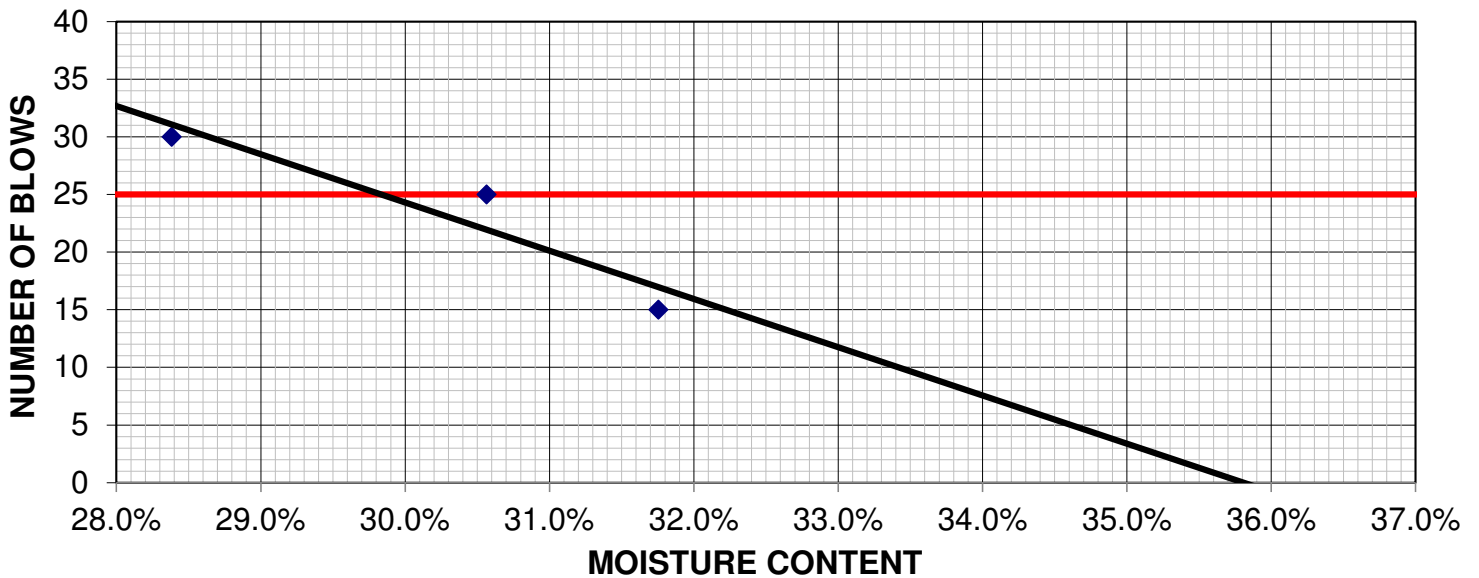
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/27/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-9, 4.5-5.0'

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 29.8  
 PLASTIC LIMIT: 23.7  
 PLASTICITY INDEX: 6.1

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	15	25	30
TARE NO.	A1	E	S		B	F1	G
GROSS WET WEIGHT	7.52	7.07	7.20		14.13	15.07	12.68
GROSS DRY WEIGHT	6.82	6.46	6.41		11.65	12.42	10.73
TARE WEIGHT	3.84	3.77	3.24		3.84	3.75	3.86
NET DRY WEIGHT	2.98	2.69	3.17		7.81	8.67	6.87
WEIGHT OF WATER	0.70	0.61	0.79		2.48	2.65	1.95
% MOISTURE	23.49%	22.68%	24.92%		31.75%	30.57%	28.38%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_



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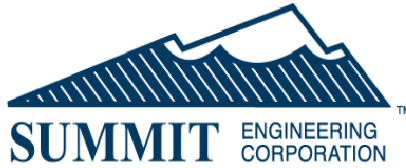
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### Grading Analysis (ASTM C-136)

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>4058.2</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3984.9</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>1.8%</b>
DATE:	<b>1/27/2021</b>	WASH WEIGHT(g):	<b>1601.2</b>
TECHNICIAN:	<b>JB</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-11, 2-3'</b>	CC:	0.96
		CU:	5.28
PI: <u>          </u> <u>          </u>	SOIL CLASSIFICATION: <u>          </u>	% PASSING #4:	<b>100</b>
LL: <u>          </u> <u>          </u>	SOIL NAME: <u>          </u>	% PASSING #200:	<b>10.8</b>
	<b>Poorly Graded Sand- Silty Sand</b>		

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		0.6		0.0	100	
#8		30.1		1.9	98	
#10		56.3		3.5	96	
#16		185.7		11.6	88	
#30		430.1		26.9	73	
#40		578.4		36.1	64	
#50		730.3		45.6	54	
#100		1119.8		69.9	30	
#200		1428.5		89.2	10.8	
PAN		1535.1				

NOTES:



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Reno Nevada 89523

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**Grading Analysis (ASTM C-136)**

JOB NAME:	<b>Woodland Village Townhomes</b>	WET WEIGHT (g):	<b>3923.7</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3864.8</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>1.5%</b>
DATE:	<b>1/25/2021</b>	WASH WEIGHT(g):	<b>1255.6</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-12, 6-7'</b>	CC:	1.29
		CU:	3.11
PI:	<b>NP</b>	SOIL CLASSIFICATION:	<b>SP</b>
		% PASSING #4:	<b>90</b>
LL:		SOIL NAME:	<b>Poorly Graded Sand</b>
		% PASSING #200:	<b>0.6</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		25.1		2.0	98	
3/8"		33.5		2.7	97	
#4		128.5		10.2	90	
#8		629.0		50.1	50	
#10		798.8		63.6	36	
#16		1076.1		85.7	14	
#30		1177.4		93.8	6	
#40		1212.9		96.6	3	
#50		1238.2		98.6	1	
#100		1246.5		99.3	1	
#200		1247.8		99.4	0.6	
PAN		0.0				

NOTES:



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### Grading Analysis (ASTM C-136)

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3741.0</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>3612.0</b>
LAB NUMBER:	<b>2529</b>	PERCENT MOISTURE:	<b>3.6%</b>
DATE:	<b>1/28/2021</b>	WASH WEIGHT(g):	<b>1720.3</b>
TECHNICIAN:	<b>MC</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>TP-14, 6.5-7.5'</b>	CC:	1.07
		CU:	36.46
PI:	0.4	SOIL CLASSIFICATION:	<b>SM w/grvl</b>
LL:	19.3	SOIL NAME:	<b>Silty Sand</b>
		% PASSING #4:	<b>83</b>
		% PASSING #200:	<b>13.3</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"		19.3			100	
1/2"		47.7		2.8	97	
3/8"		94.5		5.5	95	
#4		287.1		16.7	83	
#8		528.7		30.7	69	
#10		607.8		35.3	65	
#16		821.6		47.8	52	
#30		1036.4		60.2	40	
#40		1125.8		65.4	35	
#50		1209.2		70.3	30	
#100		1359.3		79.0	21	
#200		1490.9		86.7	13.3	
PAN		1530.8				

NOTES:



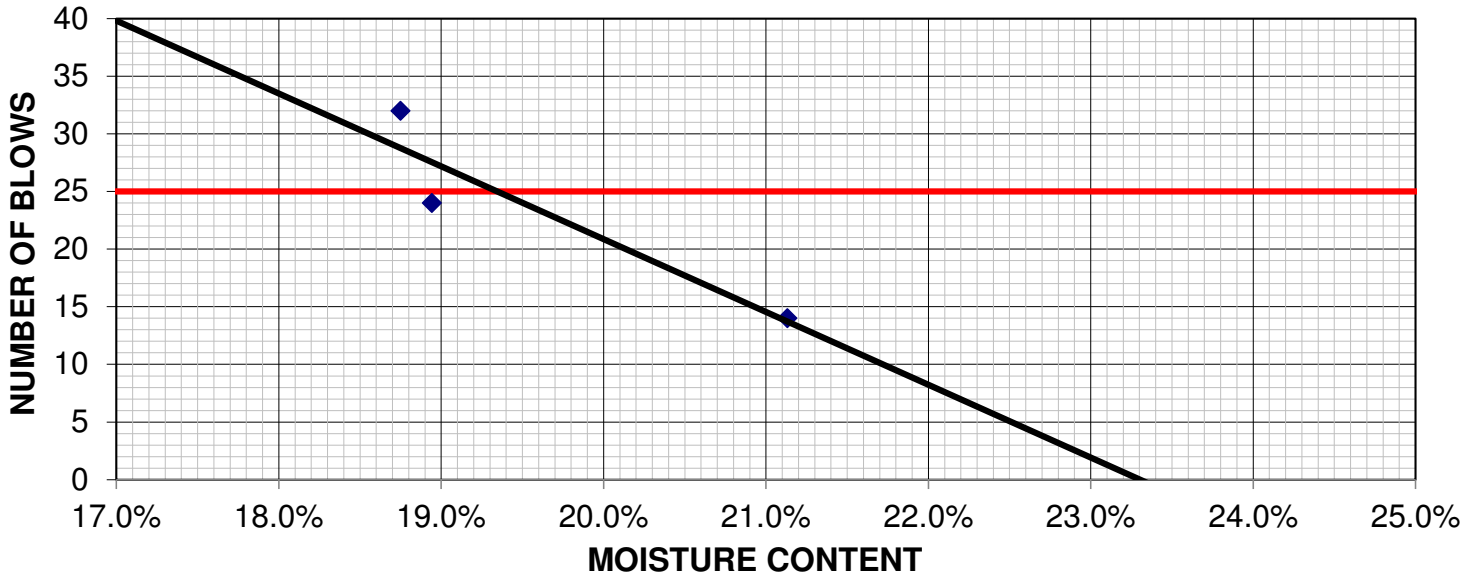
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 1/28/2021  
 TESTED BY: JB  
 LAB NUMBER: 2529  
 SAMPLE DESCRIPTION: TP-14, 6.5-7.5'

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 19.3  
 PLASTIC LIMIT: 18.9  
 PLASTICITY INDEX: 0.4

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	14	24	32
TARE NO.	S	F1	R		V	B	A1
GROSS WET WEIGHT	7.27	7.34	8.68		10.43	10.37	11.25
GROSS DRY WEIGHT	6.63	6.78	7.78		9.16	9.33	10.08
TARE WEIGHT	3.24	3.75	3.16		3.15	3.84	3.84
NET DRY WEIGHT	3.39	3.03	4.62		6.01	5.49	6.24
WEIGHT OF WATER	0.64	0.56	0.90		1.27	1.04	1.17
% MOISTURE	18.88%	18.48%	19.48%		21.13%	18.94%	18.75%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_  
 \_\_\_\_\_



# **SHEETS**

SITE



COLD SPRINGS  
MIDDLE SCHOOL

N



N.T.S.

VILLAGE PKWY

US 395

VICINITY MAP FOR  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV

JOB NO.: 31097  
APPR BY: JRP  
DRAWN BY: JRP  
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SHEET  
1  
OF  
25





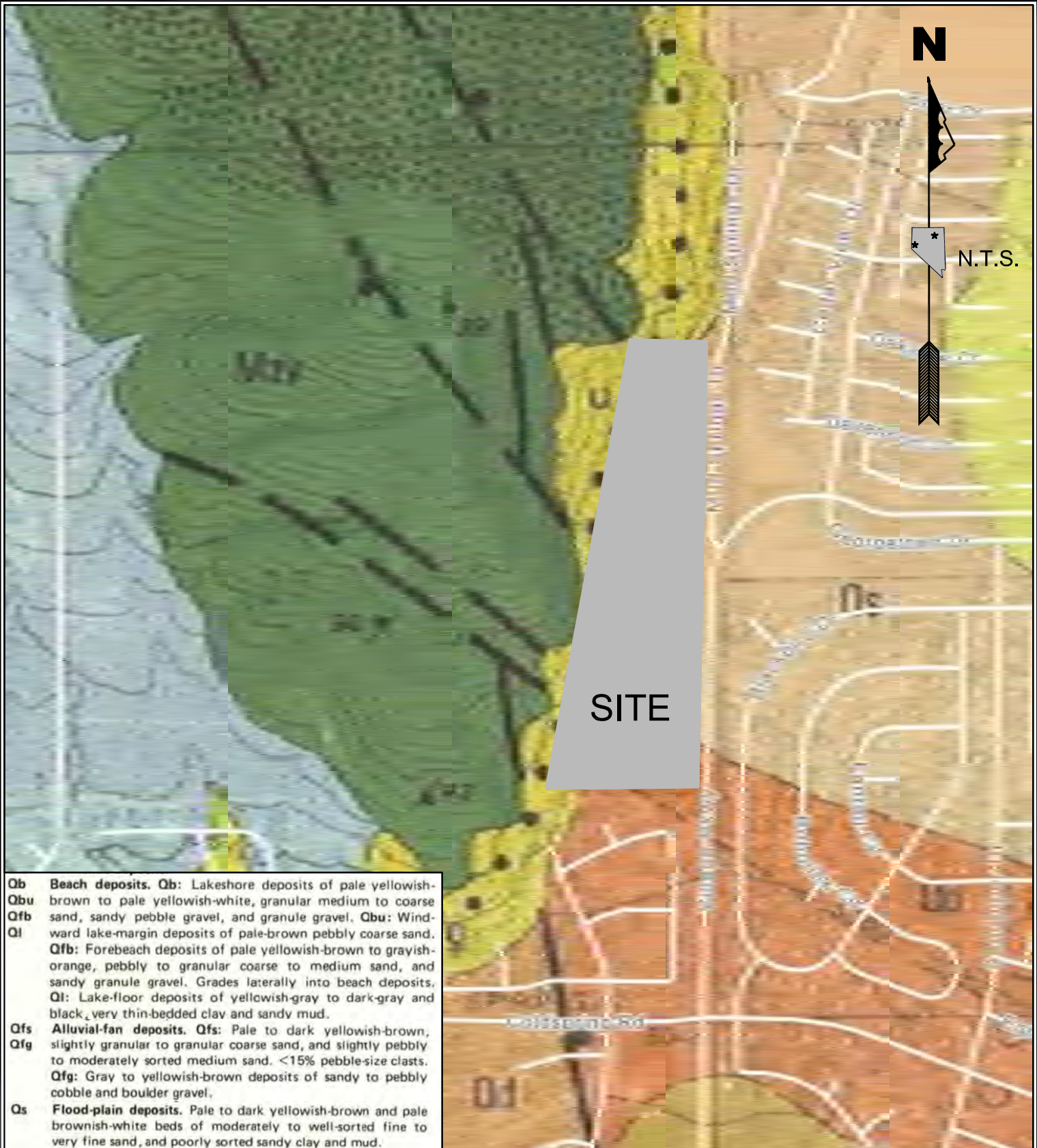
SITE MAP FOR  
 VILLAGE PARKWAY TOWNHOMES  
 RENO, NV

JOB NO.: 31097  
 APPR BY: JRP  
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SHEET  
 2  
 OF  
 25





**Qb Beach deposits.** Qb: Lakeshore deposits of pale yellowish-brown to pale yellowish-white, granular medium to coarse sand, sandy pebble gravel, and granule gravel. **Qbu**: Windward lake-margin deposits of pale-brown pebbly coarse sand. **Qfb**: Forebeach deposits of pale yellowish-brown to grayish-orange, pebbly to granular coarse to medium sand, and sandy granule gravel. Grades laterally into beach deposits. **Ql**: Lake-floor deposits of yellowish-gray to dark-gray and black, very thin-bedded clay and sandy mud.

**Qfs Alluvial-fan deposits.** Qfs: Pale to dark yellowish-brown, slightly granular to granular coarse sand, and slightly pebbly to moderately sorted medium sand. <15% pebble-size clasts. **Qfg**: Gray to yellowish-brown deposits of sandy to pebbly cobble and boulder gravel.

**Qs Flood-plain deposits.** Pale to dark yellowish-brown and pale brownish-white beds of moderately to well-sorted fine to very fine sand, and poorly sorted sandy clay and mud.

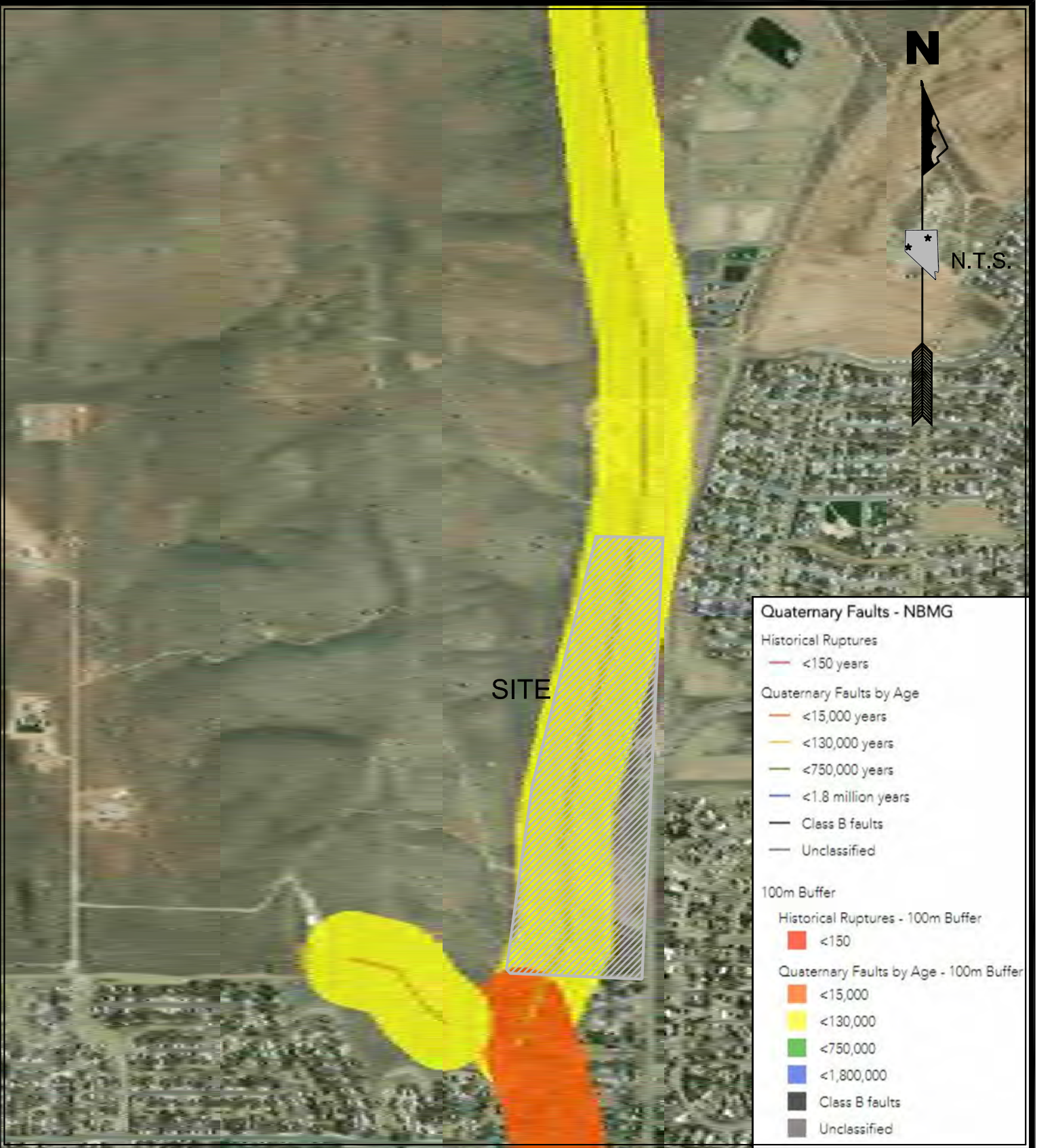
**GEOLOGIC MAP FOR  
 VILLAGE PARKWAY TOWNHOMES  
 RENO, NV**

JOB NO.: 31097  
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SHEET  
 3  
 OF  
 25





**FAULT MAP FOR  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV**

JOB NO.: 31097  
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SHEET  
4  
OF  
25



LOG OF TP-1

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION
				2	
				4	
NP	12.6	2.8		6	
				8	
				10	
				12	
				14	

MATERIAL TYPE

SM 0-1' BSG: SILTY SANDS  
SILTY SANDS. SPARSE VEGETATION

SM 1-3' BSG: SILTY SANDS  
SILTY SANDS. ESTIMATED 70% SANDS, 30% NON PLASTIC FINES. SLIGHTLY CEMENTED. DRY. LIGHT TAN. SULFATE SAMPLE. <0.01% RESULT.

SM 3-9.5' BSG: SILTY SANDS  
SILTY SANDS. 85% SANDS, 15% NON PLASTIC FINES. SLIGHTLY CEMENTED. DRY.

BOH @ 9.5' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 1**

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SHEET  
**5**  
 OF  
**25**

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF TP-2

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
				0		SM 0-1' BSG: SILTY SANDS SILTY SANDS. MINOR ORGANICS (ROOTS) SURFACE GRASS AND SHRUBS
				2		SM W/GRAVEL 1-9' BSG: SILTY SANDS WITH GRAVEL SILTY SANDS. 25% SANDS, 40% FINES, 35% GRAVELS TO 3" MINUS. CEMENTED. DRY. DENSE. TAN.
4.3	37.9	2.8		4		
				6		
				8		
				10		
				12		
				14		

BOH @ 9' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 2**

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SHEET  
**6**  
 OF  
**25**

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF TP-3

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
1.4	17.6	4.0		2		SM
				4		SM w/GRAVEL
				6		
				8		
				10		
				12		
				14		

0-4' BSG: SILTY SANDS.  
SILTY SANDS. MINOR VEGETATION AT SURFACE.  
80% SANDS, 20% FINES.  
TAN.

4-10' BSG: SILTY SANDS WITH GRAVEL  
SILTY SANDS. ESTIMATED 70% SANDS,  
15% FINES, 15% GRAVELS TO 3/4".  
DRY. LIGHT TAN. LENSES OF CEMENTATION.  
MEDIUM DENSE TO LOOSE.

BOH @ 10' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
VILLAGE PARKWAY TOWNHOMES  
TEST PIT 3

JOB #: 31097  
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SHEET  
7  
OF  
25

LOG OF TP-4

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION
				2	
				4	X
				6	
NP	4.2	2.2		8	X
				10	
				12	
				14	

SM 0-3' BSG: SILTY SAND  
 SILTY SANDS. SLIGHT ORGANICS IN FIRST 12".  
 BROWN. MOIST. NON-PLASTIC FINES.

SM  
W/GRAVEL 3-7' BSG: SILTY SAND WITH GRAVEL  
 SILTY SANDS. ESTIMATED 60% SANDS,  
 20% NON-PLASTIC FINES, 20% GRAVELS  
 TO 1". DENSE.

SW 7-11.5' BSG: WELL GRADED SAND  
 SANDS. 85% SANDS, 5% NON-PLASTIC  
 FINES, 10% GRAVELS TO 1/2".  
 LIGHT BROWN. MOIST. LOOSE.

BOH @ 11.5' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 4**

JOB #: 31097  
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SHEET  
8  
OF  
25

LOG OF TP-5

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION
2.9	4.4	4.0		2	
				4	
				6	
				8	
				10	
				12	
				14	

PT

0-1' BSG: ORGANICS  
SILTY SANDS. ROOTS AND ORGANICS.  
GRASSES AND SHRUBS.

SW

1-3.5' BSG: WELL GRADED SANDS  
SANDS. 85% SANDS, 5% FINES,  
10% GRAVELS.  
DENSE. SLIGHTLY MOIST.

SM

3.5-9.5' BSG: SILTY SANDS  
INCREASE IN AMOUNT OF FINES.  
ESTIMATED 75% SANDS, 20% FINES,  
5% GRAVELS.  
DRY. LENSES OF CEMENTATION.  
MEDIUM DENSE TO LOOSE.

BOH @ 9.5' BSG. NO GROUNDWATER.

TEST PIT LOG  
VILLAGE PARKWAY TOWNHOMES  
TEST PIT 5

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SHEET 9  
OF 25



LOG OF TP-6

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX  
% PASSING #200  
MOISTURE CONTENT  
% OF DRY WT.  
DRY DENSITY  
(PCF)  
DEPTH (FT.)  
SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	DESCRIPTION
				0		SM W/GRAVEL	0-1' BSG: SILTY SANDS WITH GRAVEL SILTY SANDS. BROWN. MOIST. SOME ORGANICS.
				2		SM	1-5' BSG: SILTY SANDS SILTY SANDS. ESTIMATED 60% SANDS, 25% NON-PLASTIC FINES, 15% GRAVELS.
				4	X		
				6		SM	5-10' BSG: SILTY SANDS SILTY SANDS. 60% SANDS, 35% FINES, 5% GRAVELS. PARTIALLY CEMENTED. LIGHT BROWN. MOIST.
				8	X		
				10		SM W/GRAVEL	10-13' BSG: SILTY SANDS WITH GRAVEL SILTY SANDS. ESTIMATED 55% SANDS, 25% NON-PLASTIC FINES, 15% GRAVELS. PARTIALLY CEMENTED. LIGHT BROWN. MOIST.
				12	X		
				14			

BOH @ 13' BSG. NO GROUNDWATER.

TEST PIT LOG  
VILLAGE PARKWAY TOWNHOMES  
TEST PIT 6

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SHEET  
10  
OF  
25

LOG OF TP-7

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	DESCRIPTION
				0	X	SM	0-1.5' BSG: SILTY SANDS SILTY SANDS. ESTIMATED 80% SANDS, 20% FINES. SLIGHTLY CEMENTED. BROWN. MOIST.
				2		SM	1.5-7' BSG: SILTY SANDS SILTY SANDS. CEMENTED. ESTIMATED 80% SANDS, 20% FINES. TAN. DRY. DENSE.
				4			
				6			
NP	11.4	4.4		8	X	SW-SM	7-10' BSG: WELL GRADED SAND WITH SILT SANDS. 85% SANDS, 10% NON-PLASTIC FINES, 5% GRAVELS. SLIGHTLY MOIST TO DRY. TAN SLIGHTLY DENSE.
				10			SLIGHTLY MOIST TO DRY. TAN SLIGHTLY DENSE.
				12			
				14			

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 7**

JOB #: 31097  
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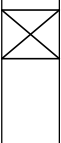





SHEET  
 11  
 OF  
 25

LOG OF TP-8

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
				2		SM
				4		SM
				6		SM
				8		
				10		
				12		
				14		

0-2' BSG: SILTY SANDS  
 SILTY SANDS. SOME MINOR ORGANICS.  
 ESTIMATED 70% SANDS, 30% FINES.  
 SLIGHTLY MOIST. BROWN.  
 SAMPLE FOR R-VALUE. R-VALUE=0

2-3.5' BSG: SILTY SANDS  
 DECREASE IN MOISTURE AT 2' BSG.  
 ESTIMATED 70% SANDS, 30% FINES.  
 MEDIUM DENSE.

3.5-12' BSG: SILTY SANDS  
 SILTY SANDS. 80% SANDS,  
 20% NON-PLASTIC FINES.  
 LENSES OF CEMENTATION. DRY.  
 TAN TO BROWN. DENSE TO LOOSE.

BOH @ 12' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 8**

JOB #: 31097  
 DRAWN BY: JRP  
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SHEET  
 12  
 OF  
 25

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF TP-9

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	DESCRIPTION
				0	X	SM	0-1.5' BSG: SILTY SANDS SILTY SANDS. ESTIMATED 70% SANDS, 30% FINES. SLIGHTLY MOIST. BROWN. SAMPLE SULFATES. RESULTS - <0.01%
				2		SM	1.5-9' BSG: SILTY SANDS SILTY SANDS. DECREASE IN MOISTURE. 55% SANDS, 45% FINES. CEMENTED. LIGHT TAN. DENSE.
6.1	43.4	7.6		4	X		
				6			
				8			
				10	X	SP-SM	9-11.5' BSG: POORLY GRADED SAND WITH SILT SANDS. ESTIMATED 85% SANDS, 10% FINES, 5% GRAVELS. LOOSE. TAN TO GRAY. SLIGHTLY MOIST.
				12			
				14			

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 9**

JOB #: 31097  
 DRAWN BY: JRP  
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SHEET  
**13**  
 OF  
**25**

LOG OF TP-10

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
				0		SM 0-1' BSG: SILTY SANDS
				2	X	SP-SM 1-10' BSG: POORLY GRADED SAND WITH SILT SANDS. 90% SANDS, 10% NON-PLASTIC FINES. TAN TO WHITE. CEMENTED. MEDIUM DENSE. DRY.
NP	10.8	1.8		4		
				6		
				8		
				10	X	SP-SM 10-11.5' BSG: POORLY GRADED SAND WITH SILT SANDS. INCREASE IN GRAVELS. ESTIMATED 80% SANDS, 10% FINES, 10% GRAVELS.
				12		
				14		

SM 0-1' BSG: SILTY SANDS.  
SILTY SANDS.  
ESTIMATED 80% SANDS, 20% FINES.  
SLIGHTLY MOIST. SLIGHTLY CEMENTED.

SP-SM 1-10' BSG: POORLY GRADED SAND WITH SILT SANDS. 90% SANDS, 10% NON-PLASTIC FINES. TAN TO WHITE. CEMENTED. MEDIUM DENSE. DRY.

SP-SM 10-11.5' BSG: POORLY GRADED SAND WITH SILT SANDS. INCREASE IN GRAVELS. ESTIMATED 80% SANDS, 10% FINES, 10% GRAVELS.

BOH @ 11.5' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 10**

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SHEET  
**14**  
 OF  
**25**



LOG OF TP-11

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	
						SM w/GRAVEL	0-1.5' BSG: SILTY SANDS WITH GRAVEL LOOSE. MOIST. BROWN. SLIGHT ORGANICS.
NP	10.8	1.8		2	X	SP-SM	1.5-6' BSG: POORLY GRADED SAND WITH SILT SANDS. 90% SANDS, 10% FINES. LOOSE. BROWN.
				4			
				6	X	SM w/GRAVEL	6-9' BSG: SILTY SANDS WITH GRAVEL INCREASE IN AMOUNT OF GRAVEL AND COARSE SANDS. ESTIMATED 65% SANDS, 15% NON-PLASTIC FINES, 20% GRAVELS. LOOSE. MOIST. BROWN.
				8			
				10			
				12			
				14			

BOH @ 9' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 11**

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 DRAWN BY: JRP  
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SHEET  
**15**  
 OF  
**25**

LOG OF TP-12

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX  
 % PASSING #200  
 MOISTURE CONTENT  
 % OF DRY WT.  
 DRY DENSITY  
 (PCF)  
 DEPTH (FT.)  
 SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	DESCRIPTION
				0-1'		SM w/GRAVEL	0-1' BSG: SILTY SANDS WITH GRAVEL LOOSE. MOIST. BROWN. SLIGHT ORGANICS.
				1-6'		SM	1-6' BSG: SILTY SANDS WITH GRAVEL SILTY SANDS. ESTIMATED 60% SANDS, 25% NON-PLASTIC FINES, 15% GRAVELS TO 1/2". LOOSE. MOIST. BROWN.
				6-10'		SP	6-10' BSG: POORLY GRADED SAND SANDS. 90% SANDS, 10% GRAVELS TO 3/4" MINUS. LOOSE. DRY. BROWN.
NP	0.5	1.5					
				10'			
				12'			
				14'			

BOH @ 10' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 12**

JOB #: 31097  
 DRAWN BY: JRP  
 CHECKED BY: JRP  
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SHEET  
 16  
 OF  
 25

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

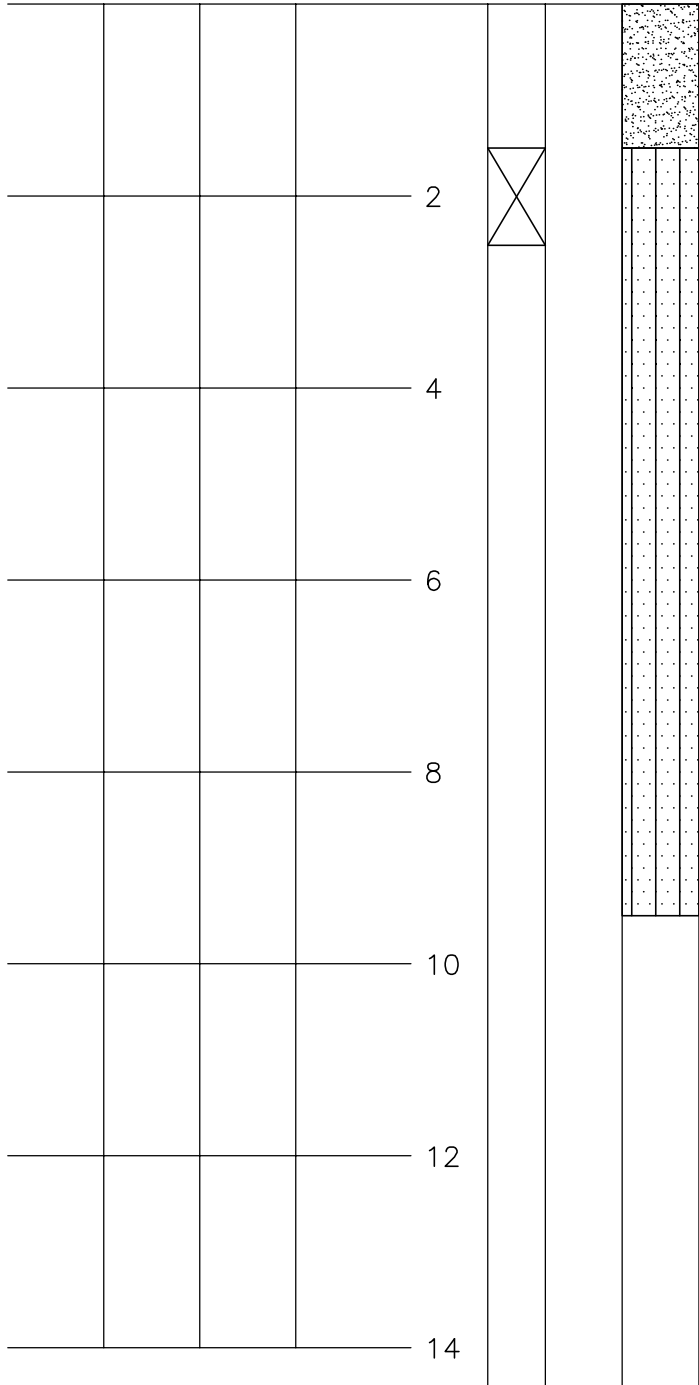
SAMPLE LOCATION

MATERIAL TYPE

LOG OF TP-13

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.



SP 0-1.5' BSG: POORLY GRADED SAND  
COARSE SANDS. MOIST. SLIGHTLY LOOSE.  
DARK BROWN. SOME ORGANICS AND ROOTS.

SM  
w/GRAVEL 1.5-9.5' BSG: SILTY SANDS WITH GRAVEL  
DECREASE IN MOISTURE.  
ESTIMATED 65% SANDS, 15% FINES,  
20% MINOR GRAVELS. SLIGHTLY MOIST.  
LOOSE.

SLIGHTLY CEMENTED AT 6' BSG.

BOH @ 9.5' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
VILLAGE PARKWAY TOWNHOMES  
TEST PIT 13

JOB #: 31097  
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SHEET  
17  
OF  
25

LOG OF TP-14

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
				0		SM W/GRAVEL
				2		SM W/GRAVEL
				4		
0.6	13.3	3.6		6		SM W/GRAVEL
				8		
				10		
				12		
				14		

0-1' BSG: SILTY SANDS WITH GRAVEL  
BROWN. MOIST. SLIGHTLY ORGANIC.

1-6' BSG: SILTY SANDS WITH GRAVEL  
SILTY SANDS. 65% SANDS, 20% NON-PLASTIC  
FINES, 15% GRAVELS TO 1".  
PARTIALLY CEMENTED. BROWN. MOIST.

6-10' SBG: SILTY SANDS WITH GRAVEL  
SILTY SANDS. 70% SANDS, 15% NON-PLASTIC  
FINES, 15% GRAVELS TO 3/4".  
PARTIALLY CEMENTED. MOIST./ BROWN.

BOH @ 10' BSG. NO GROUNDWATER.

**TEST PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**TEST PIT 14**

JOB #: 31097  
 DRAWN BY: JRP  
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SHEET  
 18  
 OF  
 25

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF IF-1

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE
				2		SM w/GRAVEL 0-10' BSG: SILTY SANDS WITH GRAVEL LENSES OF CEMENTATION. GRAVELS TO 1". SOME LOW PLASTICITY FINES.
				4		
				6		
				8		
				10		
				12		
				14		

0-10' BSG: SILTY SANDS WITH GRAVEL  
LENSES OF CEMENTATION. GRAVELS TO 1".  
SOME LOW PLASTICITY FINES.

BOH @ 10' BSG. NO GROUNDWATER.  
INFILTRATION RATE @ 10'=2MIN/INCH

**INFILTRATION PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**INFILTRATION PIT 1**

JOB #: 31097  
 DRAWN BY: JRP  
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SHEET  
**19**  
 OF  
**25**



PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF IF-2

EQUIPMENT: LINK BELT EXC.

DATE: 1-19-21 ELEV.

				2			
				4			
				6			
				8			
				10			
				12			
				14			

SC  
 0-2.5' BSG: CLAYEY SANDS  
 SOME SURFACE ORGANICS.  
 ESTIMATED 75% SANDS, 15% SLIGHTLY PLASTIC  
 FINES, 10% GRAVELS.

SM  
 2.5-6' BSG: SILTY SANDS  
 ESTIMATED 75% SANDS, 20% FINES,  
 5% MINOR GRAVELS.

BOH @ 6' BSG. NO GROUNDWATER.  
 INFILTRATION RATE @ 6'=7MIN/INCH

**INFILTRATION PIT LOG**  
**VILLAGE PARKWAY TOWNHOMES**  
**INFILTRATION PIT 2**

JOB #: 31097  
 DRAWN BY: JRP  
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 OF  
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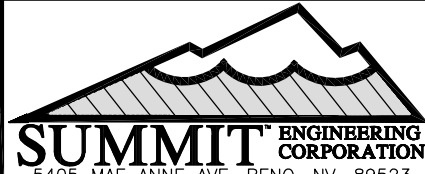
		MAJOR DIVISIONS	GRAPHIC SYMBOL	GROUP SYMBOL	TYPICAL NAMES		
COARSE GRAINED SOILS LESS THAN 50% PASSING No. 200 SIEVE	<b>GRAVELS</b>  LESS THAN 50% COARSE FRACTION PASSES THE No.4 SIEVE	CLEAN GRAVELS WITH LITTLE OR NO FINES		GW	WELL GRADED GRAVELS, GRAVEL/SAND MIXTURE		
		GRAVELS WITH OVER 12% FINES		GP	POORLY GRADED GRAVELS, GRAVEL/SAND MIXTURE		
		<b>SANDS</b>  MORE THAN 50% COARSE FRACTION PASSES THE No.4 SIEVE	CLEAN SANDS WITH LITTLE OR NO FINES		GM	SILTY GRAVEL, POORLY GRADED GRAVEL/SAND/SILT MIXTURE	
			SANDS WITH OVER 12% FINES		GC	CLAYEY GRAVEL, POORLY GRADED GRAVEL/SAND/CLAY MIXTURE	
	FINE GRAINED SOILS MORE THAN 50% PASSING No. 200 SIEVE	<b>SANDS</b>  MORE THAN 50% COARSE FRACTION PASSES THE No.4 SIEVE	CLEAN SANDS WITH LITTLE OR NO FINES		SW	WELL GRADED SANDS, GRAVELLY SANDS	
			SANDS WITH OVER 12% FINES		SP	POORLY GRADED SANDS, GRAVELLY SANDS	
		<b>SILTS AND CLAYS</b>  LIQUID LIMIT LESS THAN 50	SANDS WITH OVER 12% FINES		SM	SILTY SANDS, POORLY GRADED SAND/CLAY MIXTURES	
			SANDS WITH OVER 12% FINES		SC	CLAYEY SAND, POORLY GRADED SAND/CLAY MIXTURES	
			<b>SILTS AND CLAYS</b>  LIQUID LIMIT GREATER THAN 50			ML	INORGANIC SILTS & VERY FINE SANDS OF LOW PLASTICITY
						CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, LEAN CLAYS
<b>SILTS AND CLAYS</b>  LIQUID LIMIT GREATER THAN 50			OL	ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY			
			MH	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SANDY OR SILTY SOILS			
<b>ORGANIC RICH SOILS</b>			CH	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS			
			OH	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS			
<b>OTHER SOILS</b>			PT	TOPSOIL, PEAT, ORGANIC RICH SOILS			
			F	FILL MATERIALS			

## UNIFIED SOIL CLASSIFICATION SYSTEM

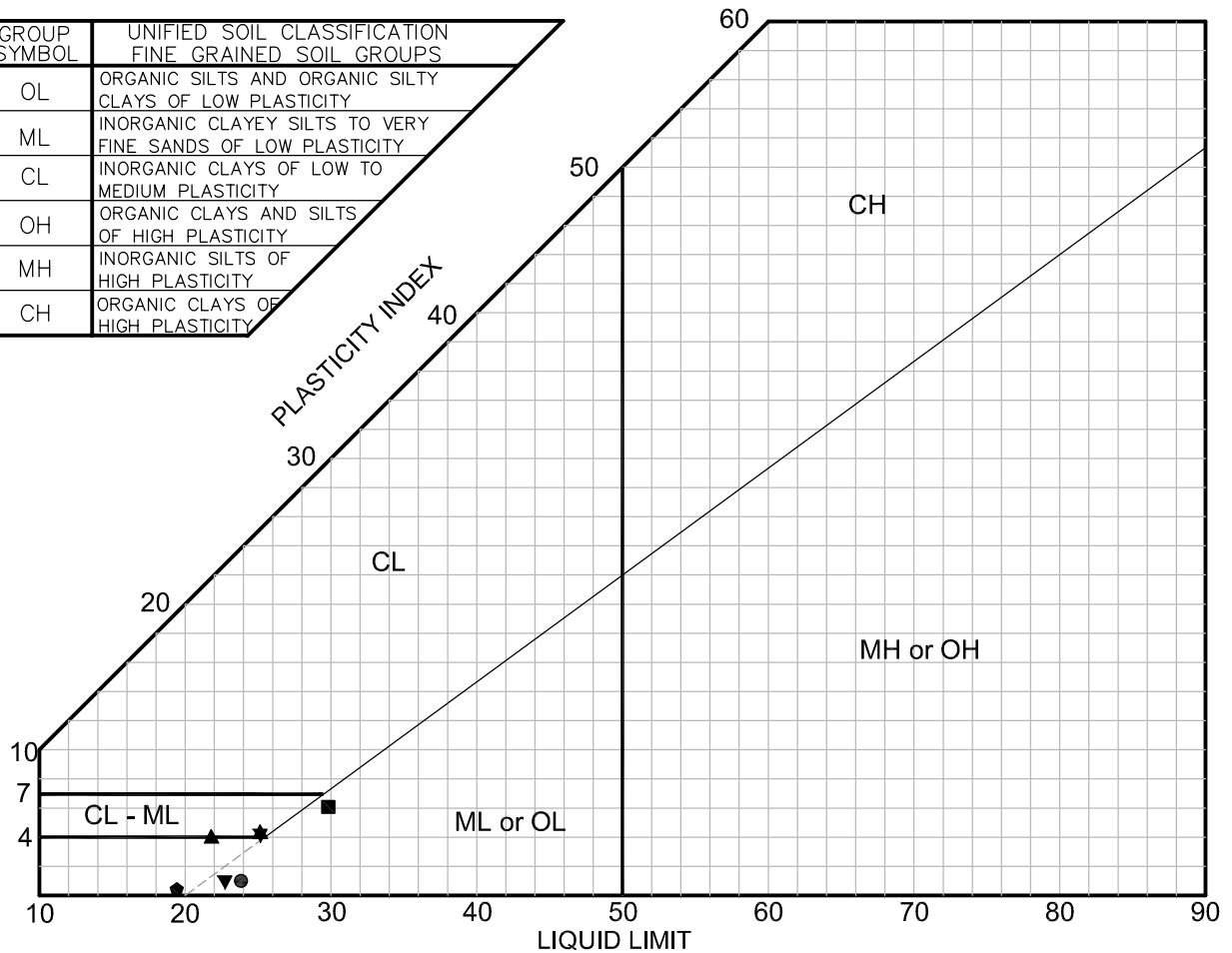
UNDISTURBED SAMPLE	BULK SAMPLE	NO RECOVERY	WATER LEVEL AT TIME OF DRILLING
			STATIC WATER LEVEL AFTER DRILLING

<b>SOIL KEY</b> VILLAGE PARKWAY TOWNHOMES RENO, NV	JOB NO.: 31097		SHEET 21
	APPR: JRP		OF
	DRAWN BY: JRP		
Copyright SUMMIT ENG 2021		5405 MAE ANNE AVE. RENO, NV. 89523	

SAMPLE LOCATION	SAMPLE DEPTH	% PASSING 3"	% PASSING #4	% PASSING #40	% PASSING #200	LIQUID LIMIT	PLASTICTY INDEX	USCS	MATERIAL TYPE
TP-1	5.0-6.0'	100	98	56	12.6	-	NP	SM	NATIVE
TP-2	3.0-4.0'	88	66	45	37.9	21.9	4.3	SM	NATIVE
TP-3	2.5-3.5'	100	99	64	19.6	22.3	1.4	SM	NATIVE
TP-4	7.5-8.5'	100	88	11	4.2	-	NP	SW	NATIVE
TP-5	2.0-3.0'	100	92	27	4.4	24.5	4.9	SW	NATIVE
TP-6	6.5-7.5'	100	92	66	37.0	23.7	1.4	SM	NATIVE
TP-7	7.0-7.5'	100	97	35	11.4	-	NP	SW-SM	NATIVE
TP-8	6.0-6.5'	100	98	56	20.8	-	NP	SM	NATIVE
TP-9	4.5-5.5'	100	100	87	43.4	29.8	6.1	SM	NATIVE
TP-11	2.0-3.0'	100	100	64	10.8	-	NP	SP-SM	NATIVE
TP-12	6.0-7.0'	100	90	3	0.6	-	NP	SP	NATIVE
TP-14	6.5-7.5'	100	83	35	13.3	19.3	0.4	SM	NATIVE

<b>SIEVE ANALYSIS</b> <b>VILLAGE PARKWAY TOWNHOMES</b> <b>RENO, NV</b>	JOB NO: 31097		SHEET 22
	APPR BY: JRP		OF
	DRAWN BY: JEB		25
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<small>N:\DWGS\J31097_VillageParkwayTownhomes\Geotech\ACAD\22_SIEVE.DWG ~ 11:35 AM * 05-FEB-2021</small>		<small>SUMMIT ENGINEERING CORPORATION 5405 MAE ANNE AVE. RENO, NV. 89523</small>	

GROUP SYMBOL	UNIFIED SOIL CLASSIFICATION FINE GRAINED SOIL GROUPS
OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
ML	INORGANIC CLAYEY SILTS TO VERY FINE SANDS OF LOW PLASTICITY
CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY
OH	ORGANIC CLAYS AND SILTS OF HIGH PLASTICITY
MH	INORGANIC SILTS OF HIGH PLASTICITY
CH	ORGANIC CLAYS OF HIGH PLASTICITY



TEST SYMBOL	SAMPLE LOCATION	SAMPLE DEPTH	% PASSING #200 SIEVE	LIQUID LIMIT	PLASTICITY INDEX	CLASSIFICATION
▲	TP-2	3-4'	37.9	21.9	4.3	SM
▼	TP-3	2.5-3.5'	19.6	22.3	1.4	SM
★	TP-5	2-3'	4.4	24.5	4.9	SW
●	TP-6	6.5-7.5'	37.0	23.7	1.4	SM
■	TP-9	4.5-5'	43.4	29.8	6.1	SM
◆	TP-14	6.5-7.5'	13.3	19.3	0.4	SM

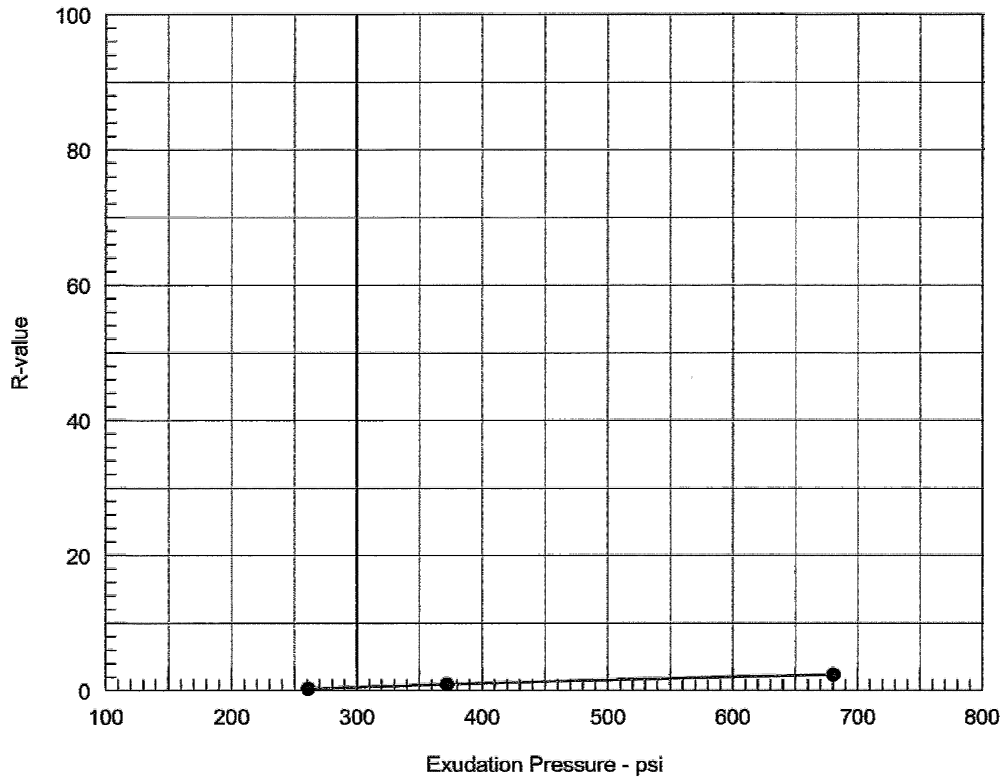
PLASTICITY INDEX  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV

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# R-VALUE TEST REPORT



**Resistance R-Value and Expansion Pressure - ASTM D2844**

No.	Compact. Pressure psi	Density pcf	Moist. %	Expansion Pressure psi	Horizontal Press. psi @ 160 psi	Sample Height in.	Exud. Pressure psi	R Value	R Value Corr.
1	75	103.9	24.3	0.00	153	2.60	681	2	2
2	50	99.1	26.1	0.00	157	2.50	372	1	1
3	49	103.8	27.9	0.00	159	2.50	261	0	0

Test Results	Material Description
R-value at 300 psi exudation pressure = 0	SITE SOIL
<b>Project No.:</b> 1146 <b>Project:</b> WOODLAND VILLAGE- VILLAGE PARKWAY TOWNHOMES <b>Location:</b> WOODLAND VILLAGE SITE <b>Sample Number:</b> 35043 <b>Date:</b> 1/26/2021	<b>Tested by:</b> M. PONTONI <b>Checked by:</b> S. VINEIS <b>Remarks:</b> RECEIVED 1/21/2021



**Figure 1A**

**RESISTANCE VALUE  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV**

JOB NO: 31097  
 APPR BY: JRP  
 BY: JRP  
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 OF 25





Silver State Labs-Reno  
1135 Financial Blvd  
Reno, NV 89502  
(775) 857-2400 FAX: (888) 398-7002  
www.ssalabs.com

# Analytical Report

Workorder#: 21010927  
Date Reported: 2/4/2021

**Client:** Summit Engineering  
**Project Name:** 31097/ WVTH TP 9 0-1 Sulfate  
**PO #:** 11354

**Sampled By:** Joe Pursel

**Laboratory Accreditation Number:** NV015/CA2990

Laboratory ID	Client Sample ID	Date/Time Sampled	Date Received
21010927-01	WVTH TP 9 0-1 Sulfate	01/19/2021 12:00	1/21/2021

Parameter	Method	Result	Units	PQL	Analyst	Date/Time Analyzed	Data Flag
Sodium	ASTM D2791	< 0.01	%	0.01	AC	02/03/2021 9:53	
Sodium Sulfate as Na <sub>2</sub> SO <sub>4</sub>	Calculation	< 0.01	%	0.01	AC	02/03/2021 9:56	
Sulfate	SM4500 SO <sub>4</sub> E	< 0.01	%	0.01	AC	02/03/2021 9:52	

**Laboratory Accreditation Number:** NV015/CA2990

Laboratory ID	Client Sample ID	Date/Time Sampled	Date Received
21010927-02	WVTH TP 1 2-3 Sulfate	01/19/2021 12:30	1/21/2021

Parameter	Method	Result	Units	PQL	Analyst	Date/Time Analyzed	Data Flag
Sodium	ASTM D2791	< 0.01	%	0.01	AC	02/03/2021 9:53	
Sodium Sulfate as Na <sub>2</sub> SO <sub>4</sub>	Calculation	< 0.01	%	0.01	AC	02/03/2021 9:56	
Sulfate	SM4500 SO <sub>4</sub> E	< 0.01	%	0.01	AC	02/03/2021 9:52	

Original

<b>SULFATE RESULTS</b> <b>VILLAGE PARKWAY TOWNHOMES</b> <b>RENO, NV</b>	JOB NO: 31097	 <b>SUMMIT</b> ENGINEERING CORPORATION 5405 MAE ANNE AVE. RENO, NV. 89523	SHEET 25
	APPR BY: JRP		OF 25
	BY: JRP		
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March 5, 2021

Mr. Robert Lissner  
Woodland Village North, LLC  
4790 Caughlin Parkway, #519  
Reno, NV 89519

Job No. 31097

RE: Geotechnical Investigation Addendum #1  
Village Parkway Townhomes  
Woodland Village  
Reno, NV

Dear Mr. Lissner:

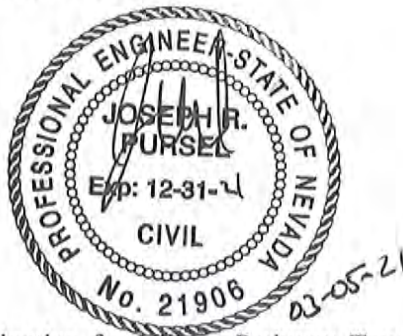
Summit Engineering Corporation is pleased to present to you this addendum to the report for the proposed housing project, Village Parkway Townhomes, in Woodland Village Development, in Reno, Nevada. Previously, Summit had provided a report dated February 5, 2021 (Summit File 31097), for the proposed housing development. This addendum is being issued to address and include additional infiltration testing that was performed on-site after the initial exploration.

**All previous recommendations from the report prepared by Summit Engineering Corporation dated February 5, 2021 remain valid and in place. This Addendum adds the additional infiltration test and results. An infiltration rate of 3 min/inch should be used in storm drain design for this area.**

If you have any questions, please contact our office.

Sincerely,  
**SUMMIT ENGINEERING CORPORATION**

Joseph R. Pursel, P.E.  
Geotechnical Division Manager



Reference: Geotechnical Investigation for Village Parkway Townhomes, Woodland Village, Reno Nevada. File No. 31097. Dated February 5, 2021.

CC: Robert Gelu, P.E., Summit Engineering



SITE



COLD SPRINGS MIDDLE SCHOOL

N



N.T.S.

VILLAGE PKWY

US 395

VICINITY MAP FOR  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV

JOB NO.: 31097 ADD.1

APPR BY: JRP

DRAWN BY: JRP

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SHEET  
1

OF  
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**SITE MAP FOR  
VILLAGE PARKWAY TOWNHOMES  
RENO, NV**

JOB NO.: 31097 ADD.1  
 APPR BY: JRP  
 DRAWN BY: JRP  
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SHEET  
2  
 OF  
3

PLASTICITY INDEX

% PASSING #200

MOISTURE CONTENT  
% OF DRY WT.

DRY DENSITY  
(PCF)

DEPTH (FT.)

SAMPLE LOCATION

MATERIAL TYPE

LOG OF IF-3

EQUIPMENT: YANMAR Vi055

DATE: 2-19-21 ELEV.

PLASTICITY INDEX	% PASSING #200	MOISTURE CONTENT % OF DRY WT.	DRY DENSITY (PCF)	DEPTH (FT.)	SAMPLE LOCATION	MATERIAL TYPE	DESCRIPTION
						SC	0-1.5' BSG: CLAYEY SANDS CLAYEY SANDS, BROWN, VERY MOIST, SOFT, SLIGHTLY ORGANIC. ESTIMATED 15% GRAVELS. MEDIUM PLASTIC.
				2		SM W/GRAVEL	1.5-3.5' BSG: SILTY SANDS WITH GRAVEL SILTY SANDS. SEMI-MOIST. LIGHT BROWN. ESTIMATED 20% NON-PLASTIC FINES, 20% GRAVELS TO 1/2".
				4		ML	3.5-9' BSG: SILTS SILT. PARTIALLY CEMENTED. LIGHT BROWN TO BROWN. DENSE. ESTIMATED 50-60% FINES. MOIST.
				6			
				8			
				10		SM	9-11' BSG: SILTY SANDS SILTY SANDS. BROWN, MOIST, LOOSE. 85% SANDS, 15% NON-PLASTIC FINES.
NP	13.8	9.3			X		INFILTRATION RATE @ 10' BSG=3 MIN/INCH  BOTTOM EXPLORATION @ 11' BSG.
				12			
				14			

**INFILTRATION PIT LOG  
VILLAGE PARKWAY TOWNHOMES  
INFILTRATION PIT 3**

JOB #: 31097 ADD.1  
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SHEET  
**3**  
OF  
**3**







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### Grading Analysis (ASTM C-136)

JOB NAME:	<b>Woodland Village Town Homes</b>	WET WEIGHT (g):	<b>3033.9</b>
JOB NUMBER:	<b>31097</b>	DRY WEIGHT (g):	<b>2775.2</b>
LAB NUMBER:	<b>2533 IF 10-11</b>	PERCENT MOISTURE:	<b>9.3%</b>
DATE:	<b>2/23/2021</b>	WASH WEIGHT(g):	<b>2101.6</b>
TECHNICIAN:	<b>PM</b>	SOAK TIME (min):	<b>30.0</b>
SAMPLE DESCRIPTION:	<b>Silty Sands</b>	CC:	1.25
		CU:	9.62
PI: <u>          </u> <u>          </u> <u>          </u>	SOIL CLASSIFICATION: <u>          </u> <u>          </u>	% PASSING #4:	<b>100</b>
LL: <u>          </u> <u>          </u> <u>          </u>	SOIL NAME: <u>          </u> <u>          </u>	% PASSING #200:	<b>13.8</b>

SIEVE	WEIGHT RETAINED		% RETAINED		% PASSING	SPECS
	INDIVIDUAL	CUMULATIVE	INDIVIDUAL	CUMULATIVE		
3"					100	
2"					100	
1 1/2"					100	
1"					100	
3/4"					100	
1/2"		0.0		0	100	
3/8"		0.0		0	100	
#4		3.2		0.2	100	
#8		42.2		2.0	98	
#10		62.4		3.0	97	
#16		255.6		12.2	88	
#30		708.0		33.7	66	
#40		951.6		45.3	55	
#50		1151.4		54.8	45	
#100		1580.9		75.2	25	
#200		1811.0		86.2	13.8	
PAN		1842.3				

NOTES:



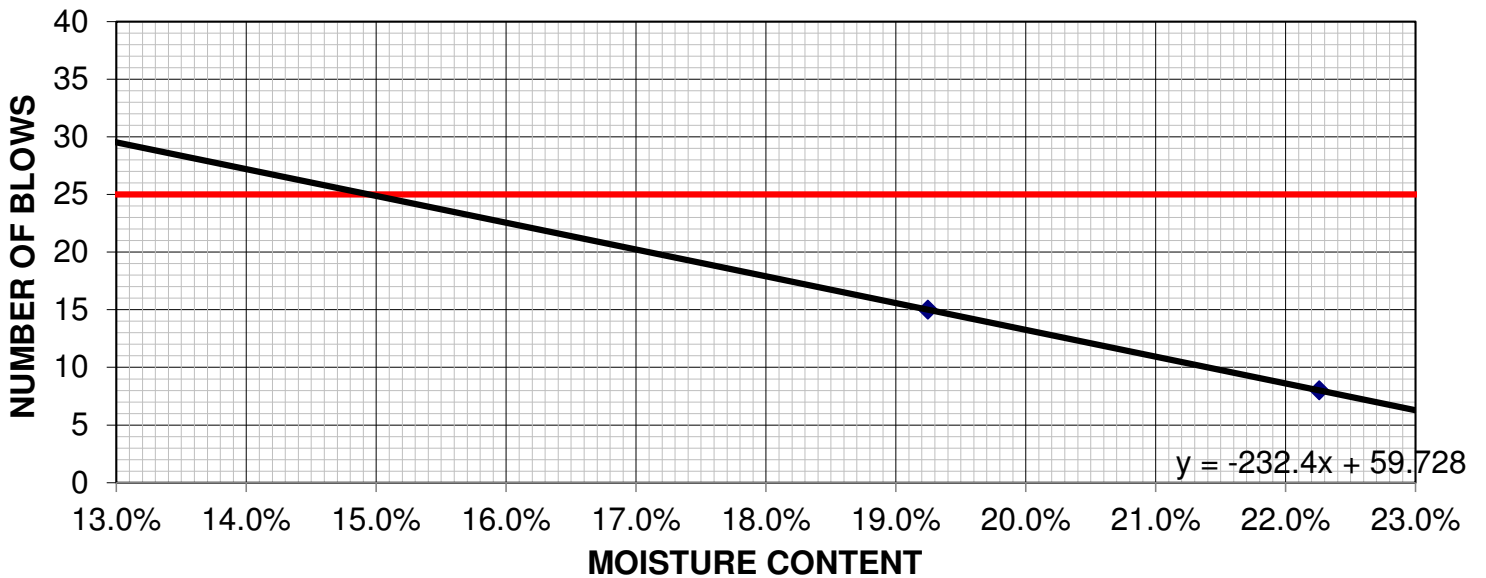
JOB NAME: Woodland Village Town Homes  
 JOB NUMBER: 31097  
 DATE: 2/23/2021  
 TESTED BY: MC  
 LAB NUMBER: 2533 IF 10-11  
 SAMPLE DESCRIPTION: Silty Sands

**Liquid and Plastic Limit (ASTM D 4318)**

LIQUID LIMIT: 15.0  
 PLASTIC LIMIT: 20.6  
 PLASTICITY INDEX: -5.6

DETERMINATION	PLASTIC LIMIT				LIQUID LIMIT / NUMBER OF BLOWS		
	1	2	3	4	15	8	
TARE NO.	T	X			B	G1	
GROSS WET WEIGHT	9.26	9.72			9.88	10.65	
GROSS DRY WEIGHT	8.34	8.71			8.91	9.27	
TARE WEIGHT	3.88	3.82			3.87	3.07	
NET DRY WEIGHT	4.46	4.89			0.00	5.04	6.20
WEIGHT OF WATER	0.92	1.01			0.00	0.97	1.38
% MOISTURE	20.63%	20.65%			#DIV/0!	19.25%	22.26%

**LIQUID LIMIT**



REMARKS: \_\_\_\_\_

VILLAGE PARKWAY  
AND  
VILLAGE CENTER  
RESIDENTIAL  
PROJECTS

TRAFFIC STUDY

NOVEMBER 2020



Prepared by:  
Solaegui Engineers, Ltd.  
715 H Street  
Sparks, Nevada 89431  
(775) 358-1004

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# VILLAGE PARKWAY AND VILLAGE CENTER RESIDENTIAL PROJECTS

## TRAFFIC STUDY

### EXECUTIVE SUMMARY

The proposed Village Parkway and Village Center Residential developments will be located in the Cold Springs area of Washoe County, Nevada. The Village Parkway Residential site is generally located west of Village Parkway and north of Cold Springs Drive on undeveloped land. The Village Center Residential site is generally located east of Village Parkway and north of Village Center Drive on mostly undeveloped land. Community center and restaurant buildings exist on the Village Center Residential site. The purpose of this study is to address the project's impact upon the adjacent street network. The following intersections have been identified for traffic capacity analysis:

1. Village Parkway/White Lake Parkway
2. Village Parkway/Cold Springs Drive
3. Village Parkway/Project Access
4. Village Parkway/New Forest Drive/Georgetown Drive
5. Village Parkway/Village Center Drive
6. Village Parkway/Rockland Drive
7. Village Parkway/North Driveway
8. Village Center Drive/East Driveway
9. Crystal Canyon Boulevard/Aquamarine Drive

The traffic study includes analysis of the AM and PM peak hours for the existing, existing plus project, 2030 base, 2030 base plus project, 2040 base, and 2040 base plus project scenarios. The White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections have been identified for updated traffic signal warrant analysis.

The proposed Village Parkway Residential development will include the construction of a total of 428 attached dwelling units with access provided from one proposed roadway intersecting Village Parkway. The Village Parkway Residential development is anticipated to generate 3,348 average daily trips with 207 trips occurring during the AM peak hour and 241 trips occurring during the PM peak hour.

The proposed Village Center Residential development will include the construction of a total of 111 attached dwelling units with access provided from multiple driveways on Village Parkway and Village Center Drive. The Village Center Residential development is anticipated to generate 851 average daily trips with 61 trips occurring during the AM peak hour and 71 trips occurring during the PM peak hour.

Traffic generated by the Village Parkway and Village Center Residential developments will have some impact on the adjacent street network. The following recommendations are made to mitigate project traffic impacts.

It is recommended that any required signing, striping, or traffic control improvements comply with Washoe County requirements.

It is recommended that the Village Parkway/Project Access intersection be designed as a three-leg intersection with stop sign control at the west approach. It is recommended that the intersection contain an exclusive left turn lane with a minimum of 340 feet of storage/deceleration length at the south approach.

It is recommended that the Village Parkway/Rockland Drive-Project Driveway intersection be improved as a four-leg intersection with stop sign control at the east project driveway and west Rockland Drive approaches. It is recommended that the existing lane markings at the west Rockland Drive approach be modified to show a shared left turn-through lane and an exclusive right turn lane. It is recommended that the north Village Parkway approach be modified to contain a left turn lane with a minimum of 100 feet of storage length.

It is recommended that pedestrian crosswalks be installed at the new east leg of the Village Parkway/Rockland Drive-Project Access intersection and at the east leg of the Village Parkway/North Driveway intersection.

# INTRODUCTION

## STUDY AREA

The proposed Village Parkway and Village Center Residential developments will be located in the Cold Springs area of Washoe County, Nevada. The Village Parkway Residential site is generally located west of Village Parkway and north of Cold Springs Drive. The Village Center Residential site is generally located east of Village Parkway and north of Village Center Drive. Figure 1 shows the approximate location of the two sites. The purpose of this study is to address the project's impact upon the adjacent street network. The following intersections have been identified for traffic capacity analysis:

1. Village Parkway/White Lake Parkway
2. Village Parkway/Cold Springs Drive
3. Village Parkway/Project Access
4. Village Parkway/New Forest Drive/Georgetown Drive
5. Village Parkway/Village Center Drive
6. Village Parkway/Rockland Drive
7. Village Parkway/North Driveway
8. Village Center Drive/East Driveway
9. Crystal Canyon Boulevard/Aquamarine Drive

This traffic study includes analysis of the AM and PM peak hours for the existing, existing plus project, 2030 base, 2030 base plus project, 2040 base, and 2040 base plus project scenarios. The White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections have been identified for updated traffic signal warrant analysis.

## EXISTING AND PROPOSED LAND USES

Both sites are mostly undeveloped land with existing community center and restaurant buildings on the Village Center Residential site. These buildings will remain with development of the projects. Land adjacent to the Village Parkway Residential site consists of single family dwelling units to the east and south and undeveloped land to the north and west. Land adjacent to the Village Center site consists of single family dwelling units to the north, south and west and a middle school and neighborhood park to the east.

The proposed Village Parkway Residential development will include the construction of a total of 428 attached dwelling units with access provided from one proposed roadway intersecting Village Parkway.

The proposed Village Center Residential development will include the construction of a total of 111 attached dwelling units with access provided from multiple driveways on Village Parkway and Village Center Drive.



**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS  
VICINITY MAP  
FIGURE 1**

## EXISTING AND PROPOSED ROADWAYS AND INTERSECTIONS

Village Parkway is a two-lane roadway with one through lane in each direction within the project study area. The speed limit is generally posted for 45 miles per hour west of White Lake Parkway, 35 miles per hour between White Lake Parkway and New Forest Drive, and 25 miles per hour east and north of New Forest Drive. Roadway improvements west of White Lake Parkway generally include graded shoulders with striped edgelines and a striped centerline. The remaining segment of Village Parkway contains curb, gutter, sidewalk and a bike lane on both sides of the street with a striped centerline. A raised center median exists between Rockland Drive and Village Center Drive.

White Lake Parkway is a two-lane roadway with one through lane in each direction east of Village Parkway. The speed limit is posted for 35 miles per hour. Roadway improvements generally include graded shoulders with striped bike lanes and a striped centerline. Some curb, gutter, and sidewalk improvements exist just east of Village Parkway.

Cold Springs Drive is a two-lane roadway with one through lane in each direction east and west of Village Parkway. The speed limit is posted for 25 miles per hour. Roadway improvements west of Village Parkway generally include curb and gutter on both sides of the street, sidewalk on the south side of the street, and a striped centerline. Curb, gutter, sidewalk and striping improvements do not exist on Cold Springs Drive east of Village Parkway.

New Forest Drive is a two-lane roadway with one through lane in each direction north of Village Parkway. The speed limit is posted for 25 miles per hour. Roadway improvements generally include curb, gutter, and sidewalk on both sides of the street with some centerline striping.

Georgetown Drive is a two-lane roadway with one through lane in each direction south of Village Parkway. Georgetown Drive aligns with New Forest Drive at the intersection with Village Parkway. The speed limit is posted for 25 miles per hour. Roadway improvements generally include curb, gutter, and sidewalk on both sides of the street.

Rockland Drive is a two-lane roadway with one through lane in each direction west of Village Parkway. The speed limit is posted for 25 miles per hour. Roadway improvements generally include curb, gutter, and sidewalk on both sides of the street.

Village Center Drive is a two-lane roadway with one through lane in each direction east of Village Parkway. The speed limit is not posted but assumed to be 25 miles per hour. Roadway improvements include curb and gutter on both sides of the street, a sidewalk on the south side of the street, and a striped centerline. Village Center Drive becomes Aquamarine Drive east of Jutewood Court.

Aquamarine Drive is a two-lane roadway with one through lane in each direction east of Jutewood Court. The speed limit is posted for 25 miles per hour. Roadway improvements include curb, gutter, and sidewalk on both sides of the street.



Crystal Canyon Boulevard is a two-lane roadway with one through lane in each direction north and south of Aquamarine Drive. The speed limit is posted for 25 miles per hour near Aquamarine Drive. Roadway improvements generally include curb and gutter on both sides of the street, sidewalk in some areas, and a striped centerline.

The Village Parkway/White Lake Parkway intersection is an unsignalized three-leg intersection with stop sign control at the east White Lake Parkway approach. The north approach contains one left turn lane and one through lane. The south approach contains one through lane and one right turn lane. The east approach contains one shared left turn-right turn lane. A striped crosswalk exists at the north leg.

The Village Parkway/Cold Springs Drive intersection is an unsignalized four-leg intersection with stop sign control at the east and west Cold Springs Drive approaches. The north and south approaches each contain one left turn lane and one shared through-right turn lane. The east and west approaches each contain one shared left turn-through-right turn lane. Striped crosswalks exist at the north and south legs.

The Village Parkway/Project Access intersection does not currently exist but is anticipated to be constructed as an unsignalized three-leg intersection with stop sign control at the west project access approach. The intersection will be analyzed with one shared through-right turn lane at the north approach, one shared left turn-through lane at the south approach, and one shared left turn-right turn lane at the west approach.

The Village Parkway/New Forest Drive-Georgetown Drive intersection is an unsignalized four-leg intersection with stop sign control at the north New Forest Drive and south Georgetown Drive approaches. The north, east, and west approaches each contain one left turn lane and one shared through-right turn lane. The south approach contains one shared left turn-through-right turn lane. Striped crosswalks exist at the north, south, east, and west legs.

The Village Parkway/Village Center Drive intersection is an unsignalized three-leg intersection with stop sign control at the east Village Center Drive approach. The north approach contains one left turn lane and one through lane. The south approach contains one shared through-right turn lane. The east approach contains one left turn lane and one right turn lane. Striped crosswalks do not exist at the intersection.

The Village Parkway/Rockland Drive intersection is an unsignalized three-leg intersection with stop sign control at the west Rockland Drive approach. The north approach contains one shared through-right turn lane. The south approach contains one left turn lane and one through lane. The west approach contains one left turn lane and one right turn lane. Striped crosswalks exist at all legs. With construction of the Village Center Residential development the intersection will be improved as a four-leg intersection with stop sign control at the east and west approaches. The four-leg intersection will be analyzed with one left turn lane and one shared through-right turn lane at the north and south approaches, one shared left turn-through lane and one right turn lane at the west approach, and one shared left turn-through-right turn lane at the east approach.

The Village Parkway/North Driveway intersection is an unsignalized three-leg intersection with stop sign control at the east approach. The north approach contains one left turn lane and one through lane. The south approach contains one shared through-right turn lane. The west approach appears to contain one shared left turn-right turn lane. The driveway currently provides access to the community center parking lot. With development of the Village Center development the driveway will continue to serve the community center as well as the new residential units.

The Village Center Drive/East Driveway intersection is an unsignalized three-leg intersection with stop sign control at the north approach. The west approach contains one shared left turn-through lane. The east approach contains one shared through-right turn lane. The north approach contains one shared left turn-right turn lane. The driveway currently provides access to the restaurant and neighborhood park parking lot. With development of the Village Center development the driveway will continue to serve the restaurant and park as well as the new residential units.

The Crystal Canyon Boulevard/Aquamarine Drive intersection is an unsignalized four-leg intersection with stop sign control at the east and west Aquamarine Drive approaches. The north, south, east, and west approaches each contain one shared left turn-through-right turn lane. Striped crosswalks exist at the north, east, and west legs.

## TRIP GENERATION

In order to assess the magnitude of project traffic impacts on the key roadways and intersections, the project dwelling units had to be reviewed in order to correspond to land use categories listed in the Tenth Edition of *ITE Trip Generation* (2018). The Village Parkway development will include a total of 428 attached dwelling units and the Village Center development will include a total of 111 attached dwelling units. Both projects are anticipated to contain single family and multifamily dwellings.

*ITE Trip Generation* generally states that multifamily housing consists of apartments, townhouses or condominiums located within the same building with at least three other dwelling units. It is estimated that approximately 385 dwelling units within the Village Parkway development and 100 dwelling units within the Village Center development are anticipated to be in buildings with at least three other units which meets the multifamily definition. Trip generation for these dwelling units was therefore calculated based on trip generation equations for *ITE Trip Generation* Land Use 220: Multifamily Housing (Low-Rise).

The remaining 43 dwelling units within the Village Parkway development and 11 dwelling units within the Village Center development are anticipated to be in buildings with less than three other units which does not meet the multifamily definition. Trip generation for these dwelling units was therefore calculated based on trip generation equations for *ITE Trip Generation* Land Use 210: Single Family Detached Housing.

Trip generation was calculated for the weekday peak hours occurring between 7:00 AM and 9:00 AM and 4:00 PM and 6:00 PM which correspond to the peak hours of adjacent street traffic.

Table 1 shows a summary of the average daily traffic (ADT) volumes and peak hour traffic volumes generated by the two projects. The trip generation worksheets are included in the Appendix.

TABLE 1 TRIP GENERATION							
LAND USE/VARIABLE	ADT	AM PEAK HOUR			PM PEAK HOUR		
		IN	OUT	TOTAL	IN	OUT	TOTAL
Village Parkway Residential							
Single Family (43 DU)	478	9	26	35	28	17	45
Low-Rise Multifamily (385 DU)	<u>2,870</u>	<u>39</u>	<u>133</u>	<u>172</u>	<u>123</u>	<u>73</u>	<u>196</u>
Total	3,348	48	159	207	151	90	241
Village Center Residential							
Single Family (11 DU)	136	3	10	13	7	5	12
Low-Rise Multifamily (100 DU)	<u>715</u>	<u>11</u>	<u>37</u>	<u>48</u>	<u>37</u>	<u>22</u>	<u>59</u>
Total	851	14	47	61	44	27	71
Grand Total	4,199	62	206	268	195	117	312

## TRIP DISTRIBUTION AND ASSIGNMENT

The distribution of the project traffic to the key intersections was based on existing peak hour traffic patterns and the locations of attractions and productions. Figure 2 shows the anticipated trip distribution percentages for both projects. The peak hour trips shown in Table 1 were subsequently assigned to the key intersections based on the trip distribution. Figure 3 shows the trip assignment at the key intersections for the AM and PM peak hours.

## EXISTING AND PROJECTED TRAFFIC VOLUMES

Figure 4 shows the existing traffic volumes at the key intersections during the AM and PM peak hours. The existing peak hour traffic volumes were obtained from weekday traffic counts conducted in September and October of 2020. It should be noted that the September and October 2020 traffic counts were conducted during the COVID-19 pandemic which may have resulted in reduced traffic on the area streets. The existing traffic counts at the Village Parkway intersections with White Lake Parkway and Rockland Drive were subsequently compared with 2019 preCOVID-19 traffic volumes at these same intersections. A comparison of the total intersection volumes indicates that the September/October 2020 traffic volumes are higher than the 2019 preCOVID-19 traffic volumes during the AM peak hour and almost equal during the PM peak hour. This comparison indicates that the existing September/October 2020 traffic counts do not require adjustments. However, in order to ensure conservative results the highest turning movement volumes from the 2019 and 2020 counts were utilized at the Village Parkway intersections with White Lake Parkway and Rockland Drive and appropriate adjustments were then made at the adjacent intersections.

Figure 5 shows the existing plus project traffic volumes at the key intersections during the AM and PM peak hours. The existing plus project volumes were obtained by adding the trip assignment volumes shown on Figure 3 to the existing traffic volumes shown on Figure 4.

Figure 6 shows the 2030 base traffic volumes at the key intersections during the AM and PM peak hours. The 2030 base traffic volumes were obtained by adding traffic generated by the approved but unbuilt dwelling units within Woodland Village and traffic generated by Cold Springs Elementary School, which is currently under construction, to the existing traffic volumes. Peak hour traffic volumes generated by the unbuilt Woodland Village dwelling units were obtained from the Woodland Village Traffic Signal Warrant Study letter dated January 15, 2020. Peak hour traffic volumes generated by the school were obtained from the Cold Springs Elementary School Traffic Study dated March 2019. Woodland Village and Cold Springs Elementary School are both anticipated to buildout by 2030.

Figure 7 shows the 2030 base plus project traffic volumes at the key intersections during the AM and PM peak hours. The 2030 base plus project traffic volumes were obtained by adding the trip assignment volumes shown on Figure 3 to the 2030 base traffic volumes shown on Figure 6.

Figure 8 shows the 2040 base traffic volumes at the key intersections during the AM and PM peak hours. The 2040 base traffic volumes were also obtained by adding traffic generated by the approved but unbuilt dwelling units within Woodland Village and traffic generated by Cold Springs Elementary School, which is currently under construction, to the existing traffic volumes. Woodland Village and Cold Springs Elementary School are both anticipated to buildout by 2030 and therefore the 2030 and 2040 base traffic volumes are identical.

Figure 9 shows the 2040 base plus project traffic volumes at the key intersections during the AM and PM peak hours. The 2040 base plus project traffic volumes were obtained by adding the trip assignment volumes shown on Figure 3 to the 2040 base traffic volumes shown on Figure 8. Again, the 2030 base plus project and 2040 base plus project traffic volumes are identical.

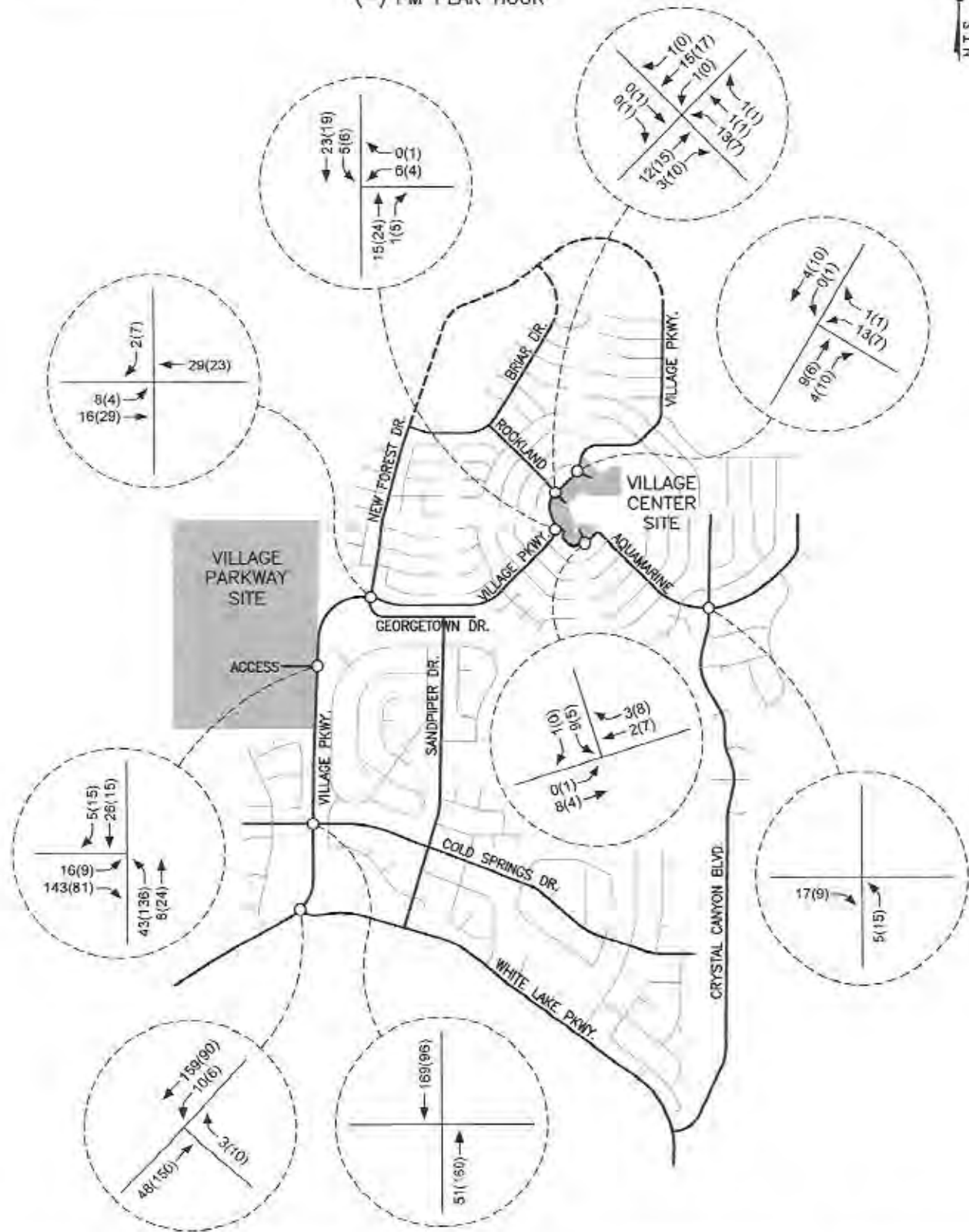




**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**TRIP DISTRIBUTION**  
**FIGURE 2**

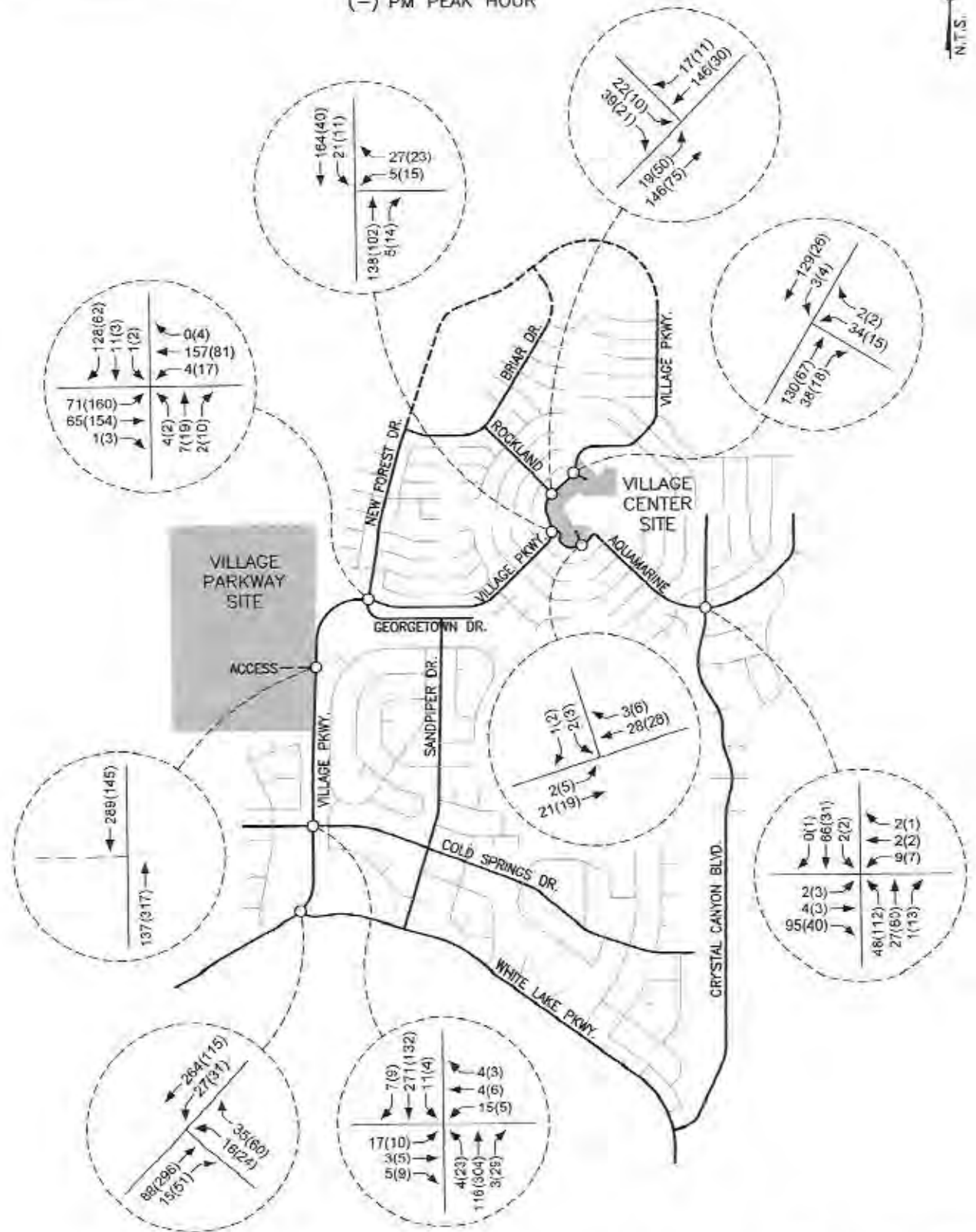


**LEGEND**  
 - AM PEAK HOUR  
 (-) PM PEAK HOUR



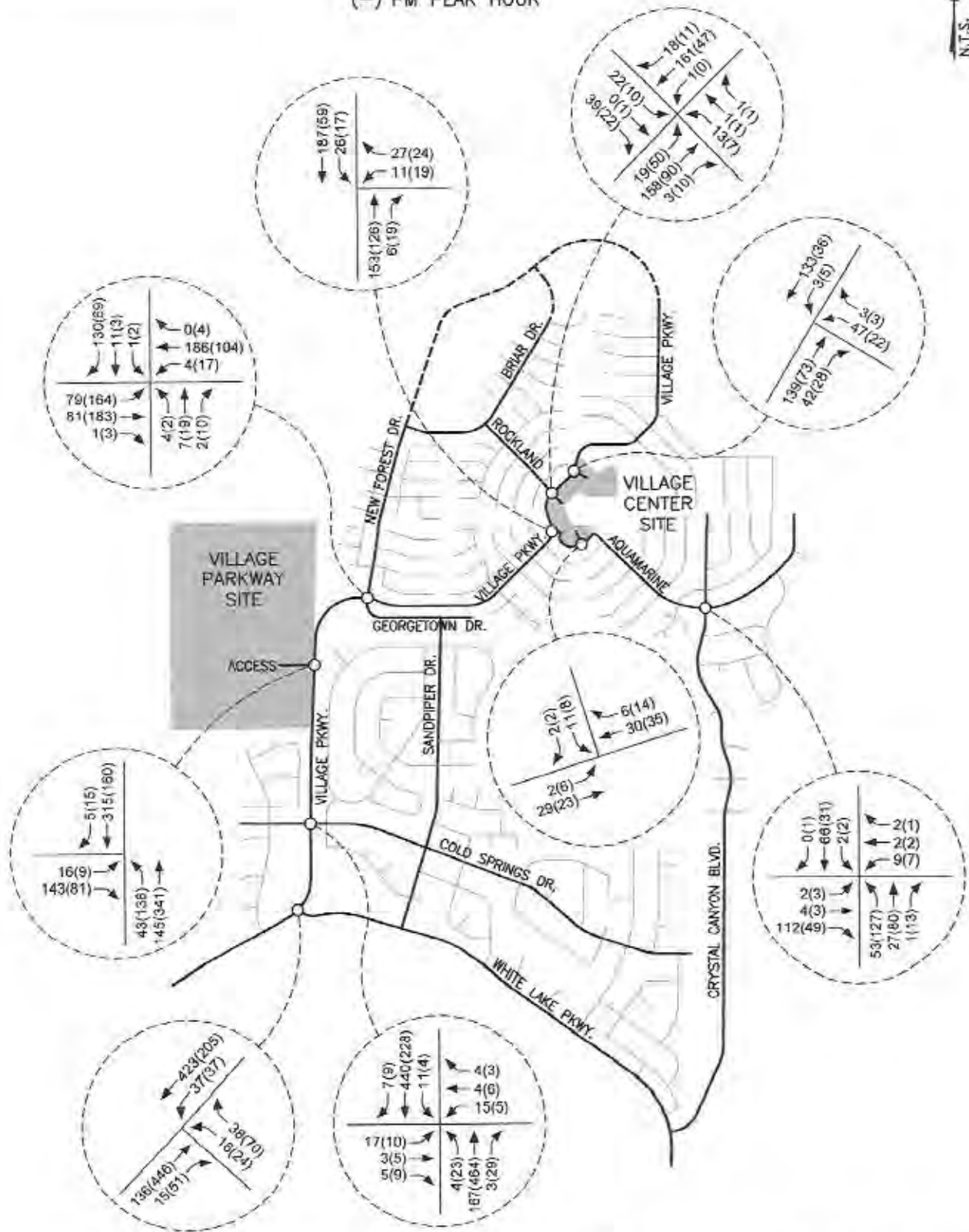
**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS  
 TRIP ASSIGNMENT  
 FIGURE 3**

**LEGEND**  
 - AM PEAK HOUR  
 (-) PM PEAK HOUR



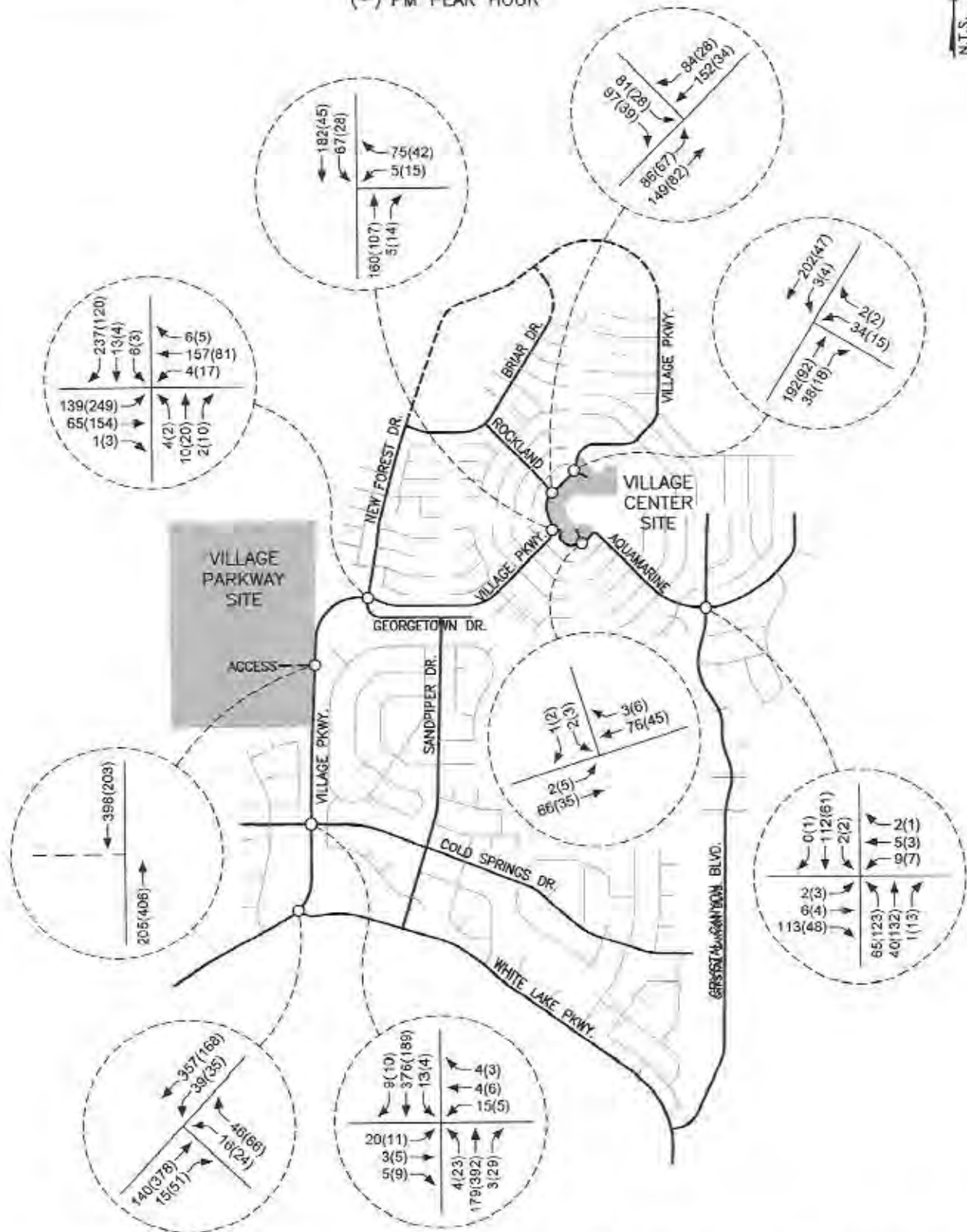
**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**EXISTING TRAFFIC VOLUMES**  
**FIGURE 4**

**LEGEND**  
 — AM PEAK HOUR  
 (—) PM PEAK HOUR



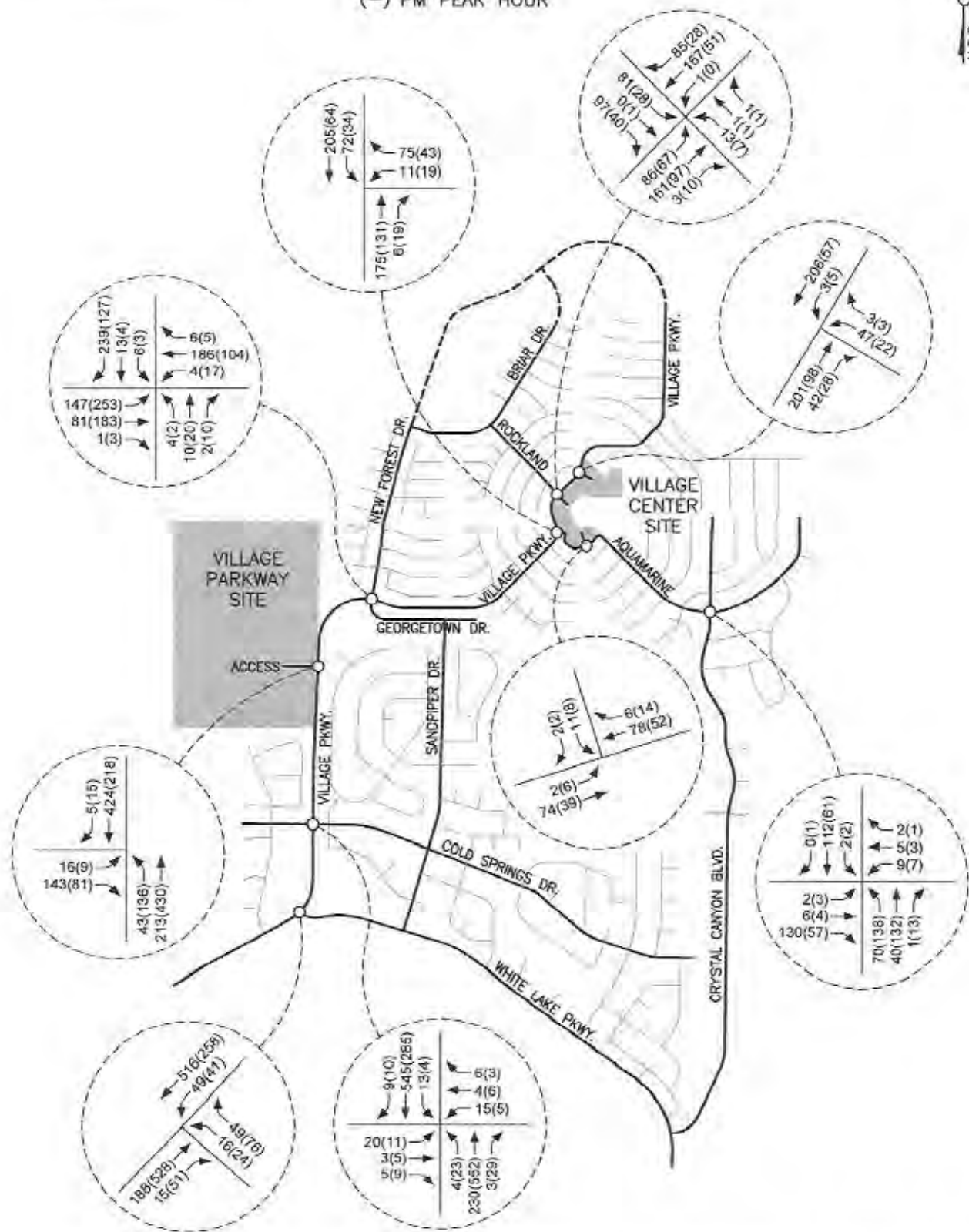
**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**EXISTING PLUS PROJECT TRAFFIC VOLUMES**  
**FIGURE 5**

**LEGEND**  
 - AM PEAK HOUR  
 (-) PM PEAK HOUR



**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**2030 BASE TRAFFIC VOLUMES**  
**FIGURE 6**

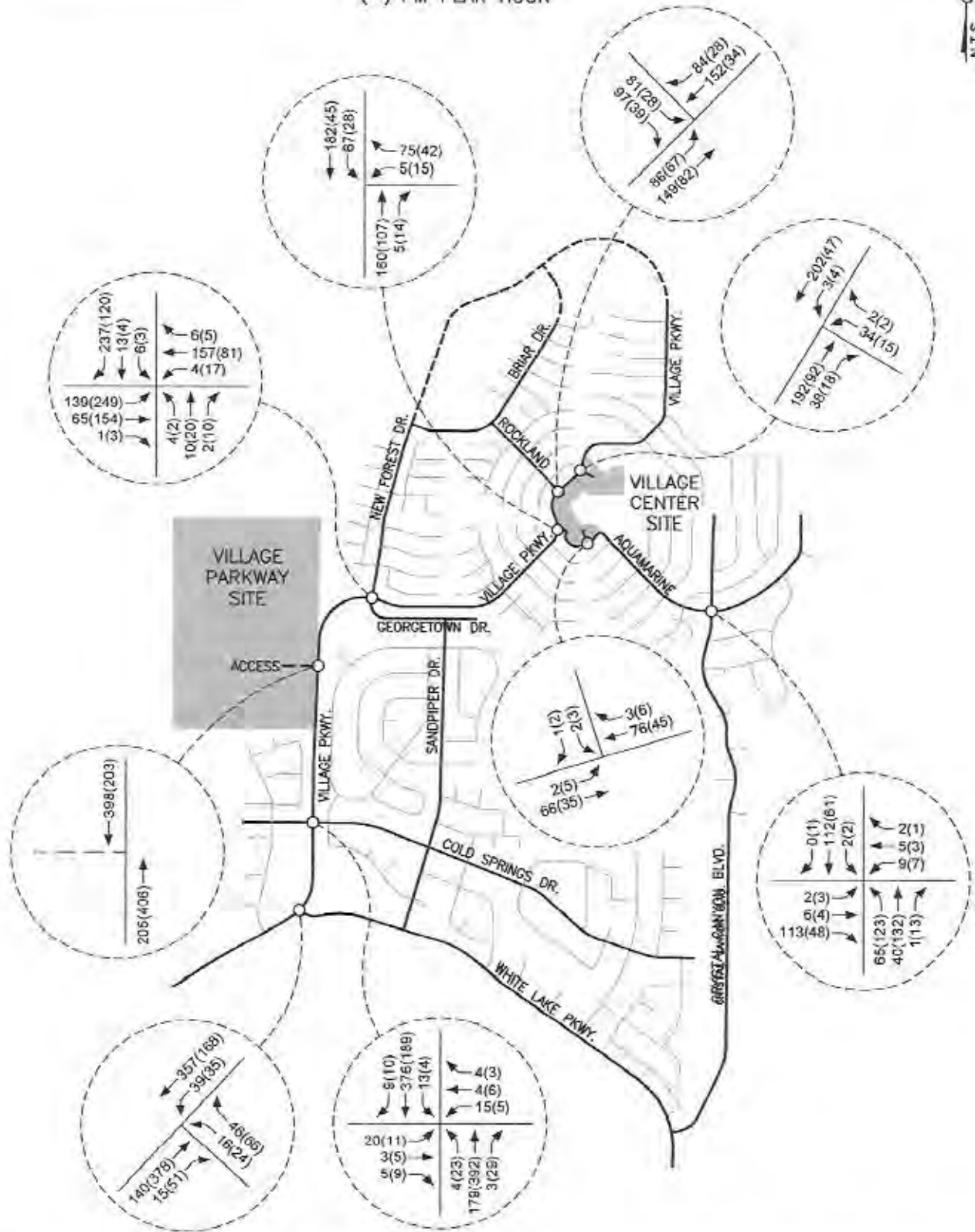
**LEGEND**  
 — AM PEAK HOUR  
 (—) PM PEAK HOUR



**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**2030 BASE PLUS PROJECT TRAFFIC VOLUMES**  
**FIGURE 7**

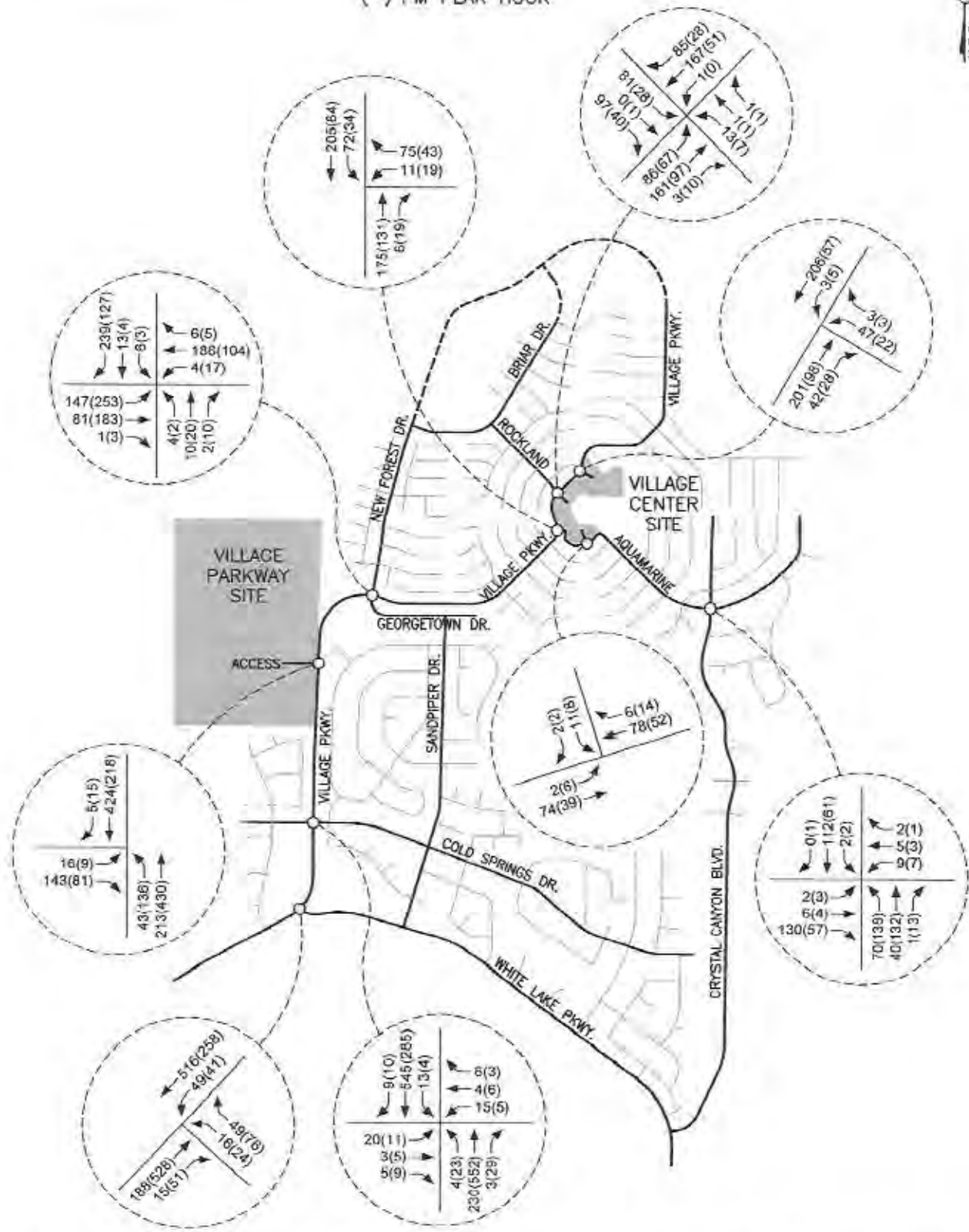


**LEGEND**  
 — AM PEAK HOUR  
 (—) PM PEAK HOUR



**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**2040 BASE TRAFFIC VOLUMES**  
**FIGURE 8**

**LEGEND**  
 — AM PEAK HOUR  
 (—) PM PEAK HOUR



**VILLAGE PARKWAY & VILLAGE CENTER RESIDENTIAL PROJECTS**  
**2040 BASE PLUS PROJECT TRAFFIC VOLUMES**  
**FIGURE 9**

## INTERSECTION CAPACITY ANALYSIS

The key intersections were analyzed for capacity based on procedures presented in the *Highway Capacity Manual (6th Edition)*, prepared by the Transportation Research Board, for unsignalized stop-controlled intersections. The latest version of the Highway Capacity computer software was used to analyze the intersections.

The result of capacity analysis is a level of service (LOS) rating for each unsignalized intersection minor movement. Level of service is a qualitative measure of traffic operating conditions where a letter grade "A" through "F", corresponding to progressively worsening traffic operation, is assigned to the unsignalized intersection minor movement.

The *Highway Capacity Manual* defines level of service for one or two-way stop controlled intersections in terms of computed or measured control delay for each minor movement. Level of service is not defined for the intersection as a whole. The level of service criteria for unsignalized intersections is shown in Table 2.

LEVEL OF SERVICE	DELAY RANGE (SEC/VEH)
A	$\leq 10$
B	$>10$ and $\leq 15$
C	$>15$ and $\leq 25$
D	$>25$ and $\leq 35$
E	$>35$ and $\leq 50$
F	$>50$

The RTC's 2040 Regional Transportation Plan indicates that level of service standards used for assessing the need for street and highway improvements at a planning level are LOS D for all regional roadway facilities projected to carry less than 27,000 ADT and LOS E for all regional roadway facilities projected to carry 27,000 or more ADT. RTC's traffic forecasting model indicates that all roadways at the key study intersections will carry less than 27,000 ADT indicating a policy LOS D standard. It should be noted that Washoe County's Cold Springs Area Plan states that LOS C or better is the policy level of service for roadways and LOS D or better is the policy level of service for intersections. LOS D is therefore the level of service standard for all key intersections in this traffic study.

Table 3 on the following page shows a summary of the level of service and delay results at the key intersections for the existing and existing plus project scenarios. The intersection capacity worksheets are included in the Appendix.

**TABLE 3  
INTERSECTION LEVEL OF SERVICE AND DELAY RESULTS  
EXISTING AND EXISTING PLUS PROJECT SCENARIOS**

INTERSECTION	EXISTING		EXISTING + PROJECT	
	AM	PM	AM	PM
Village/White Lake (Stop at East) WB Left-Right SB Left	B10.0 A7.5	B11.7 A8.2	B11.1 A7.6	B14.4 A8.7
Village/Cold Springs (Stop East/West) EB Left-Thru-Right WB Left-Thru-Right NB Left SB Left	B12.2 B12.1 A7.9 A7.5	B12.3 B13.2 A7.6 A8.0	C15.6 C15.2 A8.4 A7.6	C15.8 C17.2 A7.8 A8.5
Village/Project Access (Stop at West) EB Left-Right NB Left	N/A N/A	N/A N/A	B12.5 A8.1	B10.9 A7.9
Village/New Forest (Stop North & South) EB Left WB Left NB Left-Thru-Right SB Left-Thru SB Right	A7.8 A7.4 B12.9 B12.3 B10.2	A7.7 A7.6 B14.5 C16.6 A9.0	A7.9 A7.4 B13.9 B13.3 B10.5	A7.8 A7.7 C15.5 C18.0 A9.2
Village/Village Center (Stop at East) WB Left WB Right SB Left	B11.7 A9.4 A7.7	A9.6 A9.0 A7.5	B12.4 A9.5 A7.7	B10.1 A9.1 A7.6
Village/Rockland (Stop at West) EB Left EB Right NB Left Village/Rockland-Project Driveway (Stop at East & West) EB Left-Thru EB Right WB Left-Thru-Right NB Left SB Left	B12.4 A9.9 A7.8 N/A N/A N/A N/A N/A	B10.2 A8.7 A7.4 N/A N/A N/A N/A N/A	N/A N/A N/A B13.7 B10.1 B14.2 A7.9 A7.8	N/A N/A N/A B10.8 A8.8 B10.9 A7.5 A7.5
Village/North Dwy (Stop at East) WB Left-Right SB Left	B11.2 A7.7	A9.2 A7.4	B11.6 A7.7	A9.4 A7.4
Village Center/East Dwy (Stop at North) EB Left SB Left-Right	A7.3 A8.7	A7.3 A8.7	A7.3 A8.9	A7.3 A8.9
Crystal Canyon/Aquamarine (Stop East & West) EB Left-Thru-Right WB Left-Thru-Right NB Left SB Left	A9.3 B10.9 A7.5 A7.3	A9.2 B12.1 A7.5 A7.4	A9.4 B11.2 A7.5 A7.3	A9.2 B12.6 A7.5 A7.4

Table 4 shows a summary of the level of service and delay results at the key intersections for the 2030 base, 2030 base plus project, 2040 base, and 2040 base plus project scenarios. The intersection capacity worksheets are included in the Appendix.

TABLE 4 INTERSECTION LEVEL OF SERVICE AND DELAY RESULTS 2030 AND 2040 SCENARIOS								
INTERSECTION	2030 BASE		2030 BASE + PROJECT		2040 BASE		2040 BASE + PROJECT	
	AM	PM	AM	PM	AM	PM	AM	PM
Village/White Lake (Stop at East) WB Left-Right SB Left	B10.7 A7.6	B13.0 A8.4	B12.1 A7.8	C16.6 A9.0	B10.7 A7.6	B13.0 A8.4	B12.1 A7.8	C16.6 A9.0
Village/Cold Springs (Stop East/West) EB Left-Thru-Right WB Left-Thru-Right NB Left SB Left	B14.9 B14.1 A8.2 A7.7	B14.2 C15.2 A7.7 A8.3	C19.8 C18.2 A8.8 A7.8	C19.0 C20.5 A8.0 A8.8	B14.9 B14.1 A8.2 A7.7	B14.2 C15.2 A7.7 A8.3	C19.8 C18.2 A8.8 A7.8	C19.0 C20.5 A8.0 A8.8
Village/Project Access (Stop at West) EB Left-Right NB Left	N/A N/A	N/A N/A	B14.7 A8.5	B11.9 A8.1	N/A N/A	N/A N/A	B14.7 A8.5	B11.9 A8.1
Village/New Forest (Stop North & South) EB Left WB Left NB Left-Thru-Right SB Left-Thru SB Right	A8.0 A7.4 C17.0 C15.2 B11.4	A7.9 A7.6 C18.7 C22.3 A9.4	A8.1 A7.4 C18.7 C16.6 B11.9	A8.0 A7.7 C20.3 C24.6 A9.6	A8.0 A7.4 C17.0 C15.2 B11.4	A7.9 A7.6 C18.7 C22.3 A9.4	A8.1 A7.4 C18.7 C16.6 B11.9	A8.0 A7.7 C20.3 C24.6 A9.6
Village/Village Center (Stop at East) WB Left WB Right SB Left	B13.9 B10.0 A7.9	B10.0 A9.1 A7.5	B15.0 B10.1 A7.9	B10.5 A9.3 A7.6	B13.9 B10.0 A7.9	B10.0 A9.1 A7.5	B15.0 B10.1 A7.9	B10.5 A9.3 A7.6
Village/Rockland (Stop at West) EB Left EB Right NB Left	C19.9 B11.0 A8.3	B10.8 A8.8 A7.5	N/A N/A N/A	N/A N/A N/A	C19.9 B11.0 A8.3	B10.8 A8.8 A7.5	N/A N/A N/A	N/A N/A N/A
Village/Rockland/Dwy (Stop at East/West) EB Left-Thru EB Right WB Left-Thru-Right NB Left SB Left	N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A	C24.8 B11.2 C22.2 A8.4 A7.8	B11.7 A8.9 B11.7 A7.6 A7.5	N/A N/A N/A N/A N/A	N/A N/A N/A N/A N/A	C24.8 B11.2 C22.2 A8.4 A7.8	B11.7 A8.9 B11.7 A7.6 A7.5
Village/North Dwy (Stop at East) WB Left-Right SB Left	B13.0 A7.9	A9.5 A7.5	B13.6 A7.9	A9.7 A7.5	B13.0 A7.9	A9.5 A7.5	B13.6 A7.9	A9.7 A7.5



TABLE 4 (CONTINUED)  
INTERSECTION LEVEL OF SERVICE AND DELAY RESULTS  
2030 AND 2040 SCENARIOS

INTERSECTION	2030 BASE		2030 BASE + PROJECT		2040 BASE		2040 BASE + PROJECT	
	AM	PM	AM	PM	AM	PM	AM	PM
Village Center/East Dwy (Stop at North)								
EB Left	A7.4	A7.3	A7.4	A7.4	A7.4	A7.3	A7.4	A7.4
SB Left-Right	A9.3	A8.9	A9.5	A9.1	A9.3	A8.9	A9.5	A9.1
Crystal Can./Aquamarine (Stop East/West)								
EB Left-Thru-Right	A9.9	A9.6	B10.0	A9.6	A9.9	A9.6	B10.0	A9.6
WB Left-Thru-Right	B12.2	B13.7	B12.6	B14.3	B12.2	B13.7	B12.6	B14.3
NB Left	A7.6	A7.6	A7.6	A7.6	A7.6	A7.6	A7.6	A7.6
SB Left	A7.3	A7.5	A7.3	A7.5	A7.3	A7.5	A7.3	A7.5

Village Parkway/White Lake Parkway Intersection

The Village Parkway/White Lake Parkway intersection was analyzed as an unsignalized three-leg intersection with stop control at the east approach for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM and PM peak hours. For the existing plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements operate at LOS B or better during the AM peak hour and LOS C or better during the PM peak hour. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Parkway/White Lake Parkway intersection.

Village Parkway/Cold Springs Drive Intersection

The Village Parkway/Cold Springs Drive intersection was analyzed as an unsignalized four-leg intersection with stop control at the east and west approaches for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM and PM peak hours. For the existing plus project traffic volumes the intersection minor movements operate at LOS C or better during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS B or better during the AM peak hour and LOS C or better during the PM peak hour. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements operate at LOS C or better during the AM and PM peak hours. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Parkway/Cold Springs Drive intersection.

### Village Parkway/Project Access Intersection

The Village Parkway/Project Access intersection was analyzed as an unsignalized three-leg intersection with stop control at the west approach for the existing plus project, 2030 base plus project, and 2040 base plus project scenarios. For the existing plus project traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. The intersection was analyzed with single lanes at all approaches for each scenario. The Village Parkway/Project Access intersection meets Washoe County's policy LOS D standard for all with project scenarios.

The need for an exclusive left turn lane on Village Parkway at the project access intersection was reviewed based on AASHTO guidelines for left turn lanes on two-lane roadways. Table 9-23 of the AASHTO publication lists traffic volumes and operating speeds which necessitate the need for left turn lanes. An exclusive left turn lane is warranted based on the existing plus project traffic volumes. Storage requirements were subsequently reviewed for the left turn lane based on the AASHTO criteria of providing storage for an average two minute period. Approximately 125 feet of storage length is required based on the projected left turn volumes. A minimum deceleration length (including taper) of 215 feet is also required for the left turn lane based on the 35 mile per hour speed limit on Village Parkway for a total length of 340 feet. The need for an exclusive right turn lane on Village Parkway at the project access was also reviewed based on RTC's access management standards. The standards indicate that right turn deceleration lanes are needed on moderate access control arterials (Village Parkway) if the right turn ingress movement serves more than 60 vehicles per hour. The anticipated right turn ingress volume is below the 60 vehicle per hour threshold so a right turn lane is not warranted.

It is recommended that the Village Parkway/Project Access intersection be designed as a three-leg intersection with stop sign control at the west approach and contain an exclusive left turn lane with a minimum of 340 feet of storage/deceleration length at the south approach.

### Village Parkway/New Forest Drive-Georgetown Drive Intersection

The Village Parkway/New Forest Drive-Georgetown Drive intersection was analyzed as an unsignalized four-leg intersection with stop control at the north and south approaches for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM peak hour and LOS C or better during the PM peak hour. For the existing plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM peak hour and LOS C or better during the PM peak hour. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS C or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements operate at LOS C or better during the AM and PM peak hours. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Parkway/New Forest Drive-Georgetown Drive intersection.

### Village Parkway/Village Center Drive Intersection

The Village Parkway/Village Center Drive intersection was analyzed as an unsignalized three-leg intersection with stop control at the east approach for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM peak hour and LOS A during the PM peak hour. For the existing plus project traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM and PM peak hours. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Parkway/Village Center Drive intersection.

### Village Parkway/Rockland Drive-Project Driveway Intersection

The Village Parkway/Rockland Drive intersection was analyzed as an unsignalized three-leg intersection with stop control at the west approach for the existing, 2030 base, and 2040 base scenarios. The intersection minor movements currently operate at LOS B or better during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS C or better during the AM peak hour and LOS B or better during the PM peak hour. The three-leg intersection was analyzed with the existing approach lanes. The existing three-leg intersection meets Washoe County's policy LOS D standard.

The Village Parkway/Rockland Drive-Project Driveway intersection was analyzed as an unsignalized four-leg intersection with stop control at the east and west approaches for the existing plus project, 2030 base plus project, and 2040 base plus project scenarios. For the existing plus project traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements operate at LOS C or better during the AM peak hour and LOS B or better during the PM peak hour. The four-leg intersection was analyzed with one left turn lane and one shared through-right turn lane at the north and south Village Parkway approaches, one shared left turn-through lane and one right turn lane at the west approach, and one shared left turn-through-right turn lane at the east approach. The four-leg intersection meets Washoe County's policy LOS D standard for all with project scenarios.

It is recommended that the Village Parkway/Rockland Drive-Project Driveway intersection be improved as a four-leg intersection with stop sign control at the east project driveway and west Rockland Drive approaches. It is recommended that the existing lane markings at the west Rockland Drive approach be modified to show a shared left turn-through lane and an exclusive right turn lane. The north approach currently contains a center two-way left turn lane. It is recommended that the north Village Parkway approach be modified to contain a typical left turn lane with a minimum of 100 feet of storage length.



### Village Parkway/North Driveway Intersection

The Village Parkway/North Driveway intersection was analyzed as an unsignalized three-leg intersection with stop control at the east approach for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM peak hour and LOS A during the PM peak hour. For the existing plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM peak hour and LOS A during the PM peak hour. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS B or better during the AM peak hour and LOS A during the PM peak hour. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM peak hour and LOS A during the PM peak hour. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Parkway/North Driveway intersection.

### Village Center Drive/East Driveway Intersection

The Village Center Drive/East Driveway intersection was analyzed as an unsignalized three-leg intersection with stop control at the north approach for all scenarios. The intersection minor movements currently operate at LOS A during the AM and PM peak hours. For the existing plus project traffic volumes the intersection minor movements continue to operate at LOS A during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS A during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements continue to operate at LOS A during the AM and PM peak hours. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Village Center Drive/East Driveway intersection.

### Crystal Canyon Boulevard/Aquamarine Drive Intersection

The Crystal Canyon Boulevard/Aquamarine Drive intersection was analyzed as an unsignalized four-leg intersection with stop control at the east and west approaches for all scenarios. The intersection minor movements currently operate at LOS B or better during the AM and PM peak hours. For the existing plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM and PM peak hours. For both the 2030 base and 2040 base traffic volumes the intersection minor movements operate at LOS B or better during the AM and PM peak hours. For both the 2030 base plus project and 2040 base plus project traffic volumes the intersection minor movements continue to operate at LOS B or better during the AM and PM peak hours. The intersection was analyzed with the existing approach lanes for all scenarios. The intersection meets Washoe County's policy LOS D standard for all study scenarios. No capacity improvements are recommended at the Crystal Canyon Boulevard/Aquamarine Drive intersection.

## SITE PLAN REVIEW

A copy of the preliminary site plans for the proposed Village Parkway and Village Center Residential developments are included with this submittal. The preliminary site plan for the Village Center development indicates that project access will be provided from existing driveways on Village Parkway and Village Center Drive and one new driveway on Village Parkway. The new driveway will align with Rockland Drive. The project driveways will connect to the on-site roadways and guest parking area. The site plan also indicates that parking will continue to be provided for the existing Woodland Village community center and restaurant buildings. The project driveways, internal streets, and parking areas are anticipated to provide good access and internal circulation.

Access to the Village Parkway site will be provided from one new roadway intersecting Village Parkway. The location of the project access intersection has not yet been determined but will be located along the project frontage south of Mud Springs Drive. Mud Springs Drive intersects the curved segment of Village Parkway and a left turn lane exists on Village Parkway at Mud Springs Drive. It is therefore suggested that the project access intersection be located so that it meets sight distance requirements and does not interfere with the existing left turn lane at the Village Parkway/Mud Springs Drive intersection. RTC's access management standards also indicate that driveways on arterials with moderate access control (Village Parkway) shall be located a minimum of 300 feet from adjacent driveways. The project access intersection should also be located to meet the 300 foot minimum spacing requirement.

## SCHOOL ZONE PEDESTRIAN SAFETY REVIEW

The project's impact on pedestrian safety within the existing school zone on Village Parkway was reviewed. The school zone begins  $\pm 50$  feet north of Rockland Drive and ends  $\pm 50$  west of Cody Court. A single midblock crosswalk located  $\pm 150$  feet north of the North Driveway exists within the Village Parkway school zone. The existing pavement markings and signs at this school zone crossing appear to conform to Manual on Uniform Traffic Control Devices (MUTCD) standards. Three additional Village Parkway crossings located adjacent to the project site exist outside the school zone limits. Two of these crossings are located at the north and south legs of the Village Parkway/Rockland Drive intersection and the third crossing is located approximately midway between Rockland Drive and Village Center Drive. The existing pavement markings and signs at these crossings also appear to conform to MUTCD standards.

School pedestrian activity was subsequently reviewed at the four Village Parkway crosswalks. Actual counts show 9 AM peak hour and 5 PM peak hour pedestrians at the midblock crossing north of the North Project Driveway, 12 AM peak hour and 3 PM peak hour pedestrians at the crossing north of Rockland Drive, 21 AM peak hour and 9 PM peak hour pedestrians at the crossing south of Rockland Drive, and 20 AM peak hour and 6 PM peak hour pedestrians at the midblock crossing between Rockland Drive and Village Center Drive. Our observations indicate good pedestrian safety at each of the crossings.



Traffic volumes were also reviewed on Village Parkway at these pedestrian crossing locations in order to compare to Washoe County street capacity thresholds. The 2040 base plus project traffic volumes show a maximum volume of 527 vehicles during the AM peak hour on Village Parkway south of Rockland Drive. This peak hour volume amounts to  $\pm 5,300$  ADT based on a typical 10% AM peak hour percentage of the ADT. Washoe County standards indicate that two-lane collector streets (Village Parkway) are designed to serve a maximum of 7,300 vehicles per day. The maximum 2040 buildout traffic volume of 5,300 ADT on Village Parkway is well below the 7,300 ADT capacity threshold of the street. It should be noted that bike lanes and sidewalks exist on both sides of Village Parkway per Washoe County collector street standards.

In summary, the existing school zone on Village Parkway as well as the existing pedestrian facilities on Village Parkway further south of the school zone appear to conform to MUTCD standard while providing safe operation based on site observations. In addition, buildout traffic volumes on Village Parkway will be lower than the design capacity of the street. It is recommended that pedestrian crosswalks be installed at the new east leg of the Village Parkway/Rockland Drive-Project Access intersection and at the east leg of the Village Parkway/North Driveway intersection.

## TRAFFIC SIGNAL WARRANT ANALYSIS

A full traffic signal warrant study was prepared for the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections in January of 2020. Traffic Signal Warrants 1 through 9 as presented in the 2009 Edition of the Manual on Uniform Traffic Control Devices (MUTCD) were analyzed. The results of this study indicate that no traffic signal warrants are met at either the White Lake Parkway/Crystal Canyon Boulevard or Village Parkway/White Lake Parkway intersections for either the existing or existing plus unbuilt Woodland Village traffic volumes.

Traffic Signal Warrants 1 through 3 as presented in the 2009 Edition of the Manual on Uniform Traffic Control Devices (MUTCD) were subsequently re-evaluated at the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections based on additional traffic volumes generated by the proposed Village Parkway and Village Center Residential developments as well as trips generated by the Cold Springs Elementary School.

The results of the updated warrant analysis indicate that traffic signal warrants 1, 2, and 3 are still not met at the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections. The updated warrant analysis is included in the Appendix.

## RECOMMENDATIONS

Traffic generated by the Village Parkway and Village Center Residential developments will have some impact on the adjacent street network. The following recommendations are made to mitigate project traffic impacts.

It is recommended that any required signing, striping, or traffic control improvements comply with Washoe County requirements.

It is recommended that the Village Parkway/Project Access intersection be designed as a three-leg intersection with stop sign control at the west approach. It is recommended that the intersection contain an exclusive left turn lane with a minimum of 340 feet of storage/deceleration length at the south approach.

It is recommended that the Village Parkway/Rockland Drive-Project Driveway intersection be improved as a four-leg intersection with stop sign control at the east project driveway and west Rockland Drive approaches. It is recommended that the existing lane markings at the west Rockland Drive approach be modified to show a shared left turn-through lane and an exclusive right turn lane. It is recommended that the north Village Parkway approach be modified to contain a left turn lane with a minimum of 100 feet of storage length.

It is recommended that pedestrian crosswalks be installed at the new east leg of the Village Parkway/Rockland Drive-Project Access intersection and at the east leg of the Village Parkway/North Driveway intersection.

# APPENDIX

# Single-Family Detached Housing (210)

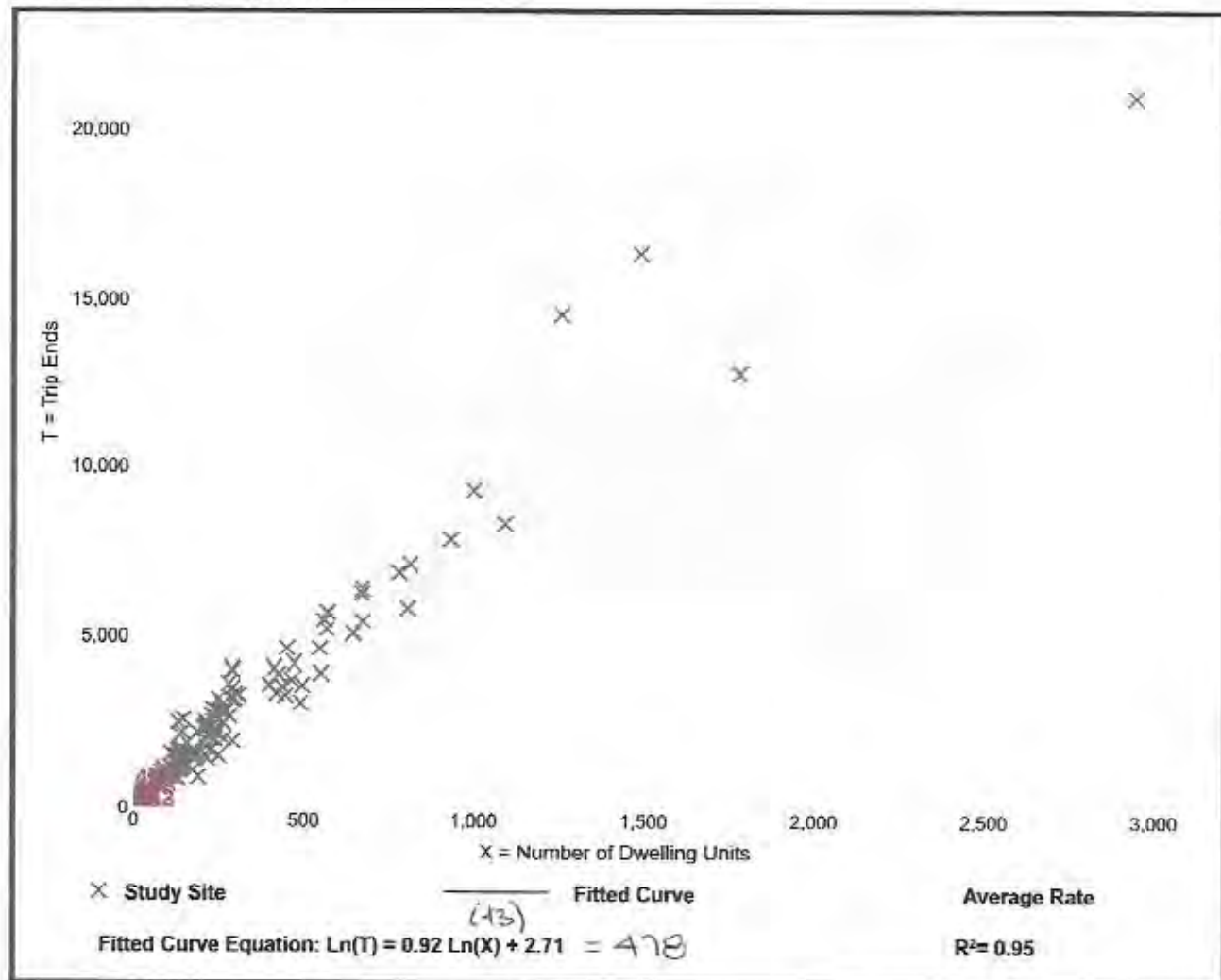
Vehicle Trip Ends vs: Dwelling Units  
On a: Weekday

Setting/Location: General Urban/Suburban  
Number of Studies: 159  
Avg. Num. of Dwelling Units: 264  
Directional Distribution: 50% entering, 50% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
9.44	4.81 - 19.39	2.10

## Data Plot and Equation



# Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,  
One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

Number of Studies: 173

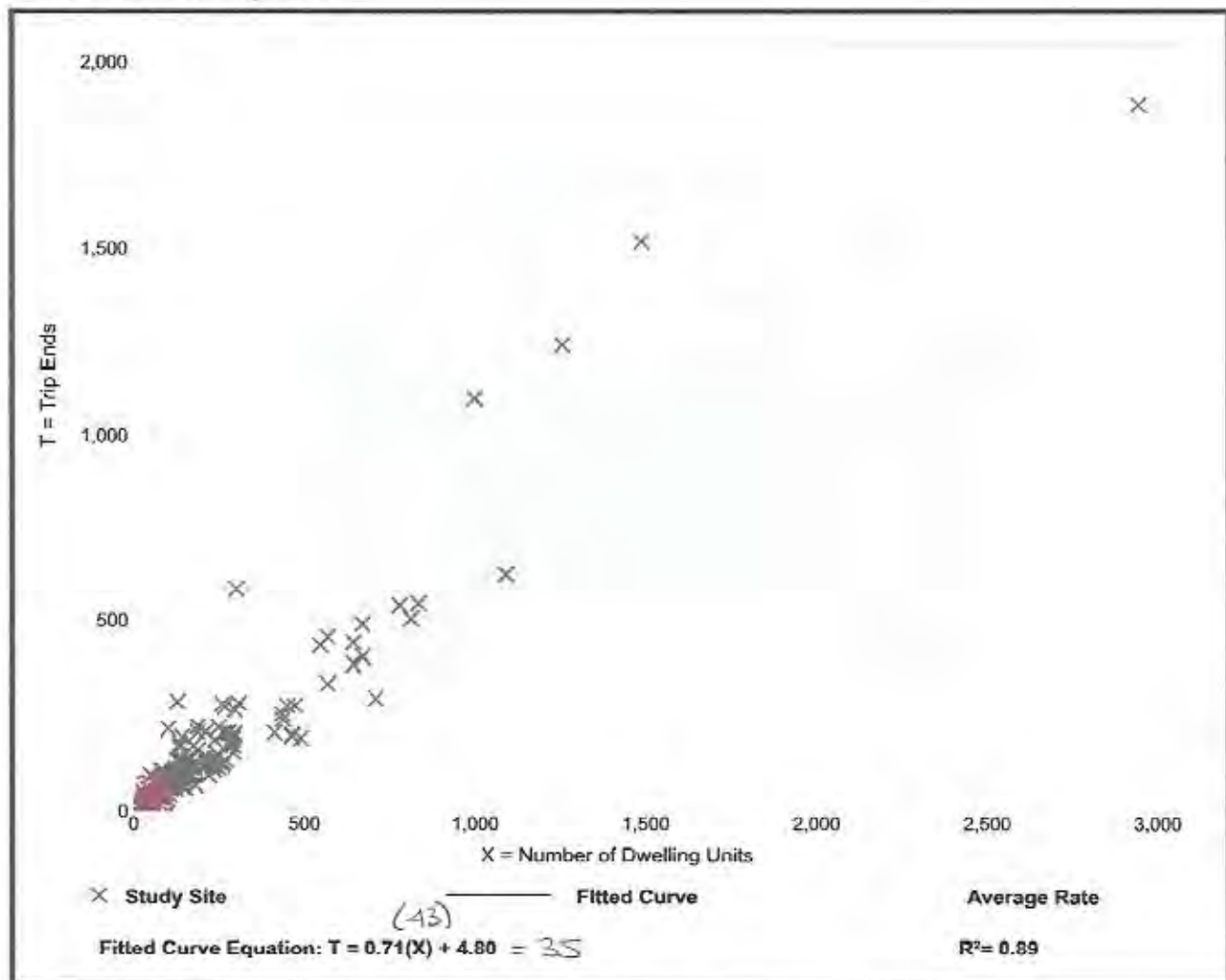
Avg. Num. of Dwelling Units: 219

Directional Distribution: 25% entering, 75% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.74	0.33 - 2.27	0.27

## Data Plot and Equation





# Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,  
One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 190

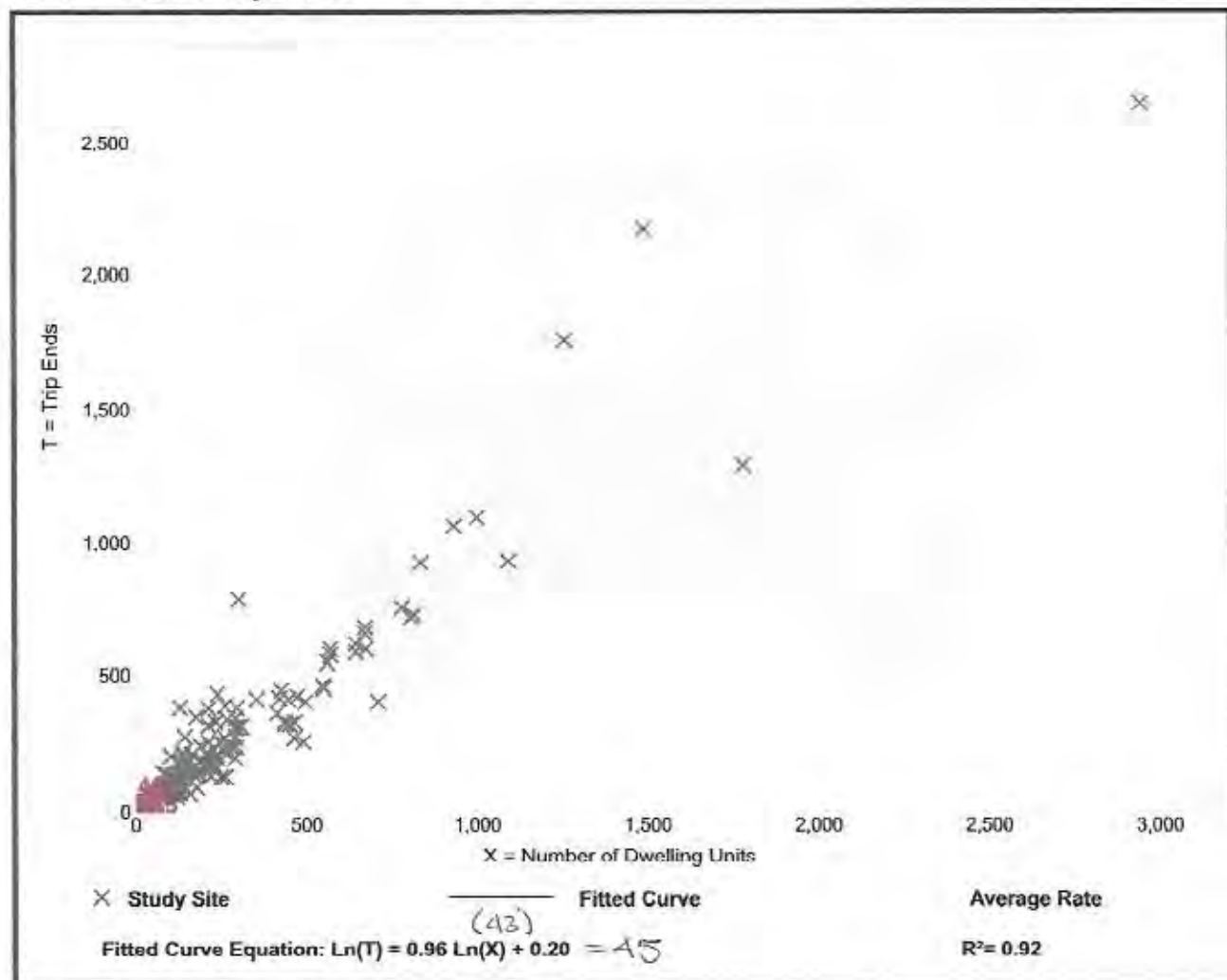
Avg. Num. of Dwelling Units: 242

Directional Distribution: 63% entering, 37% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.99	0.44 - 2.98	0.31

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

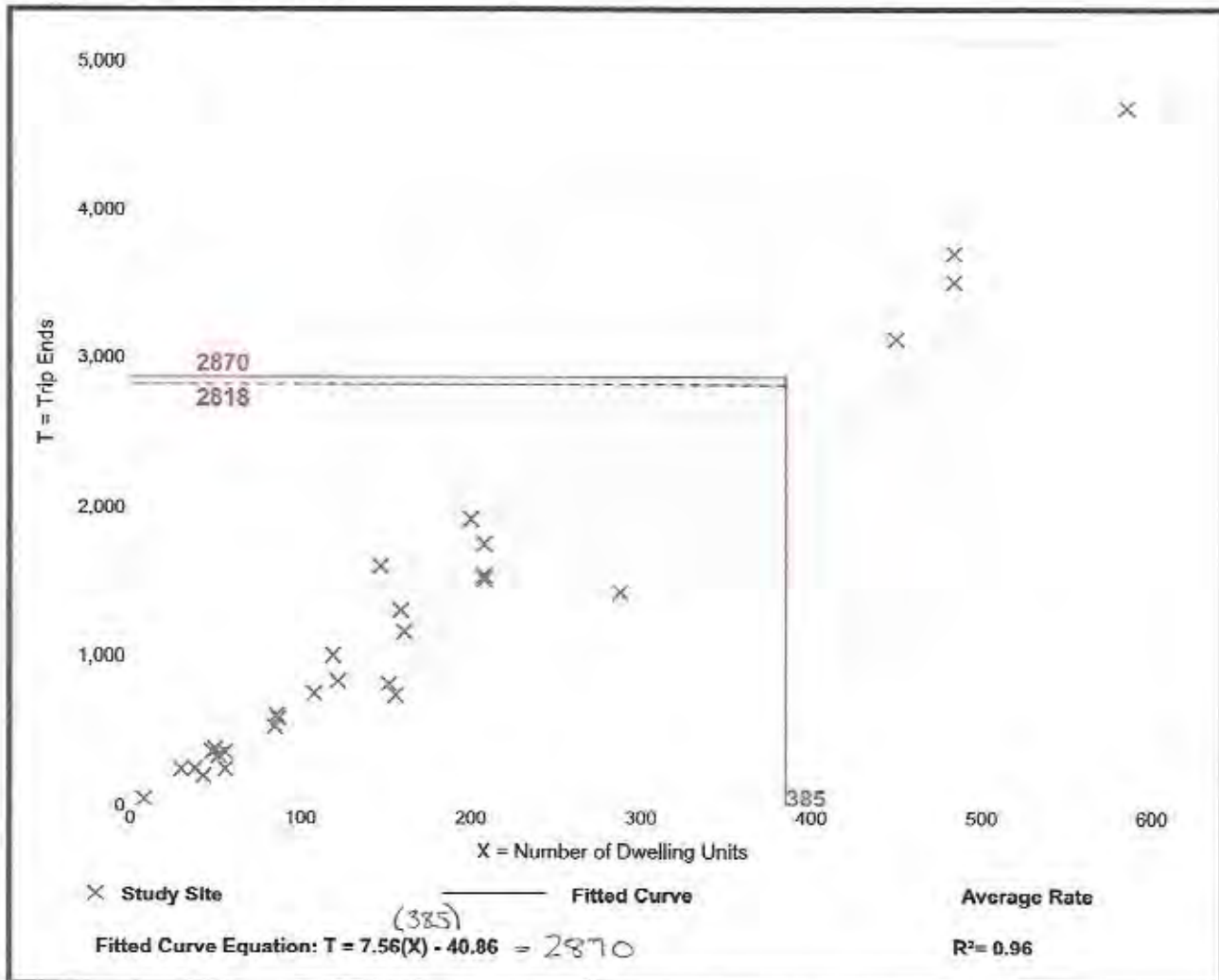
Vehicle Trip Ends vs: Dwelling Units  
On a: Weekday

Setting/Location: General Urban/Suburban  
Number of Studies: 29  
Avg. Num. of Dwelling Units: 168  
Directional Distribution: 50% entering, 50% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
7.32	4.45 - 10.97	1.31

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

Number of Studies: 42

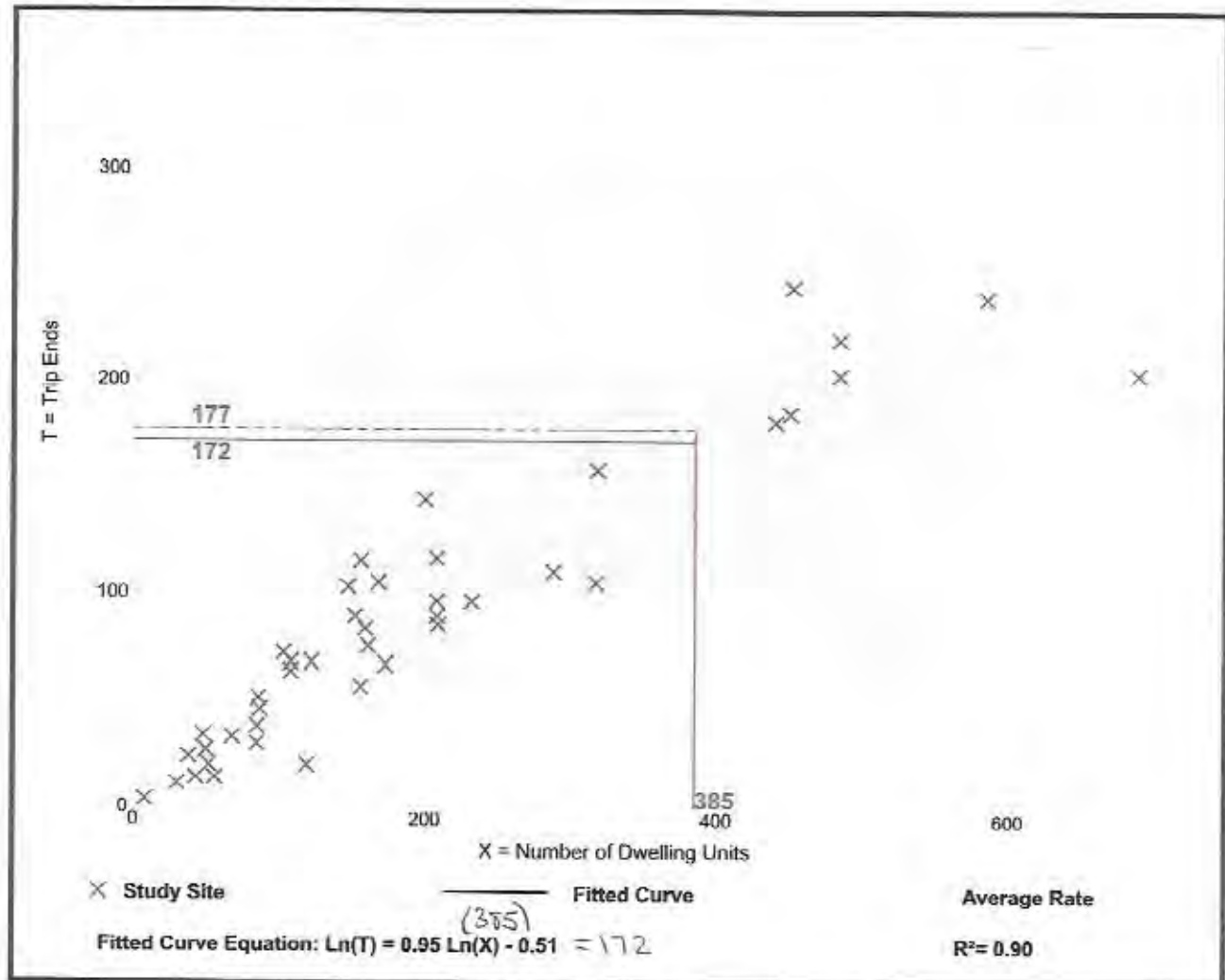
Avg. Num. of Dwelling Units: 199

Directional Distribution: 23% entering, 77% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.46	0.18 - 0.74	0.12

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 50

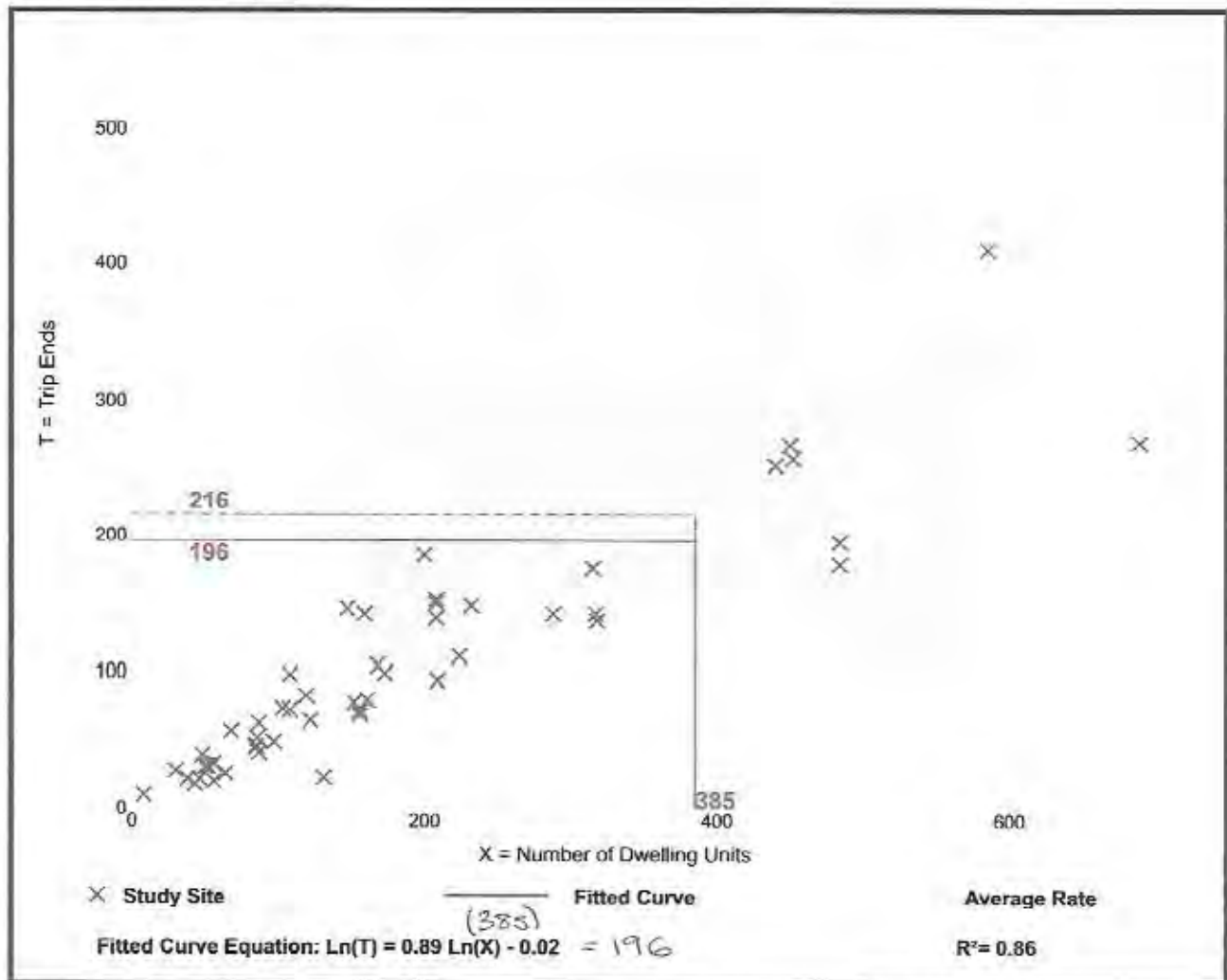
Avg. Num. of Dwelling Units: 187

Directional Distribution: 63% entering, 37% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.56	0.18 - 1.25	0.16

## Data Plot and Equation



# Single-Family Detached Housing (210)

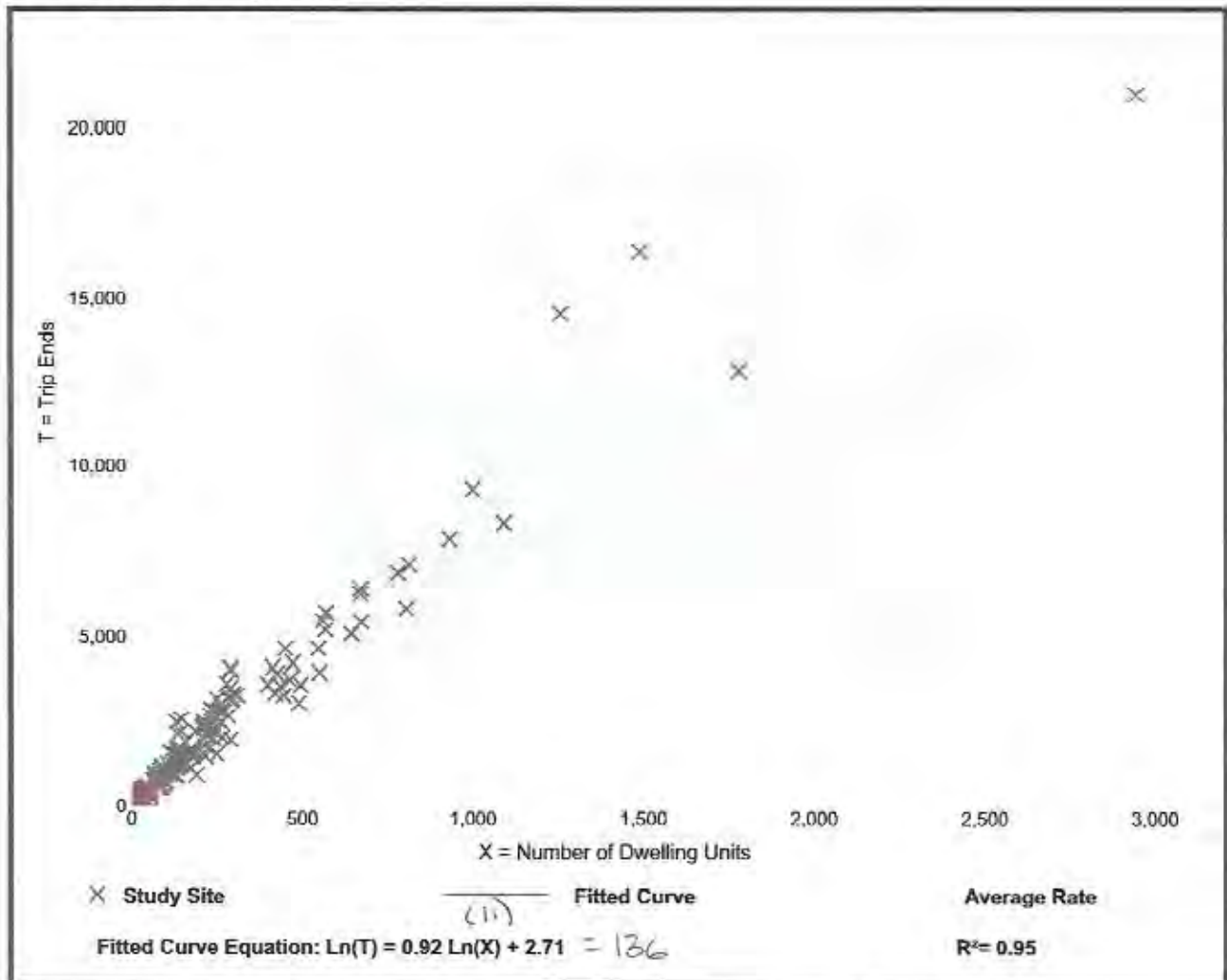
Vehicle Trip Ends vs: Dwelling Units  
On a: Weekday

Setting/Location: General Urban/Suburban  
Number of Studies: 159  
Avg. Num. of Dwelling Units: 264  
Directional Distribution: 50% entering, 50% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
9.44	4.81 - 19.39	2.10

## Data Plot and Equation





# Single-Family Detached Housing (210)

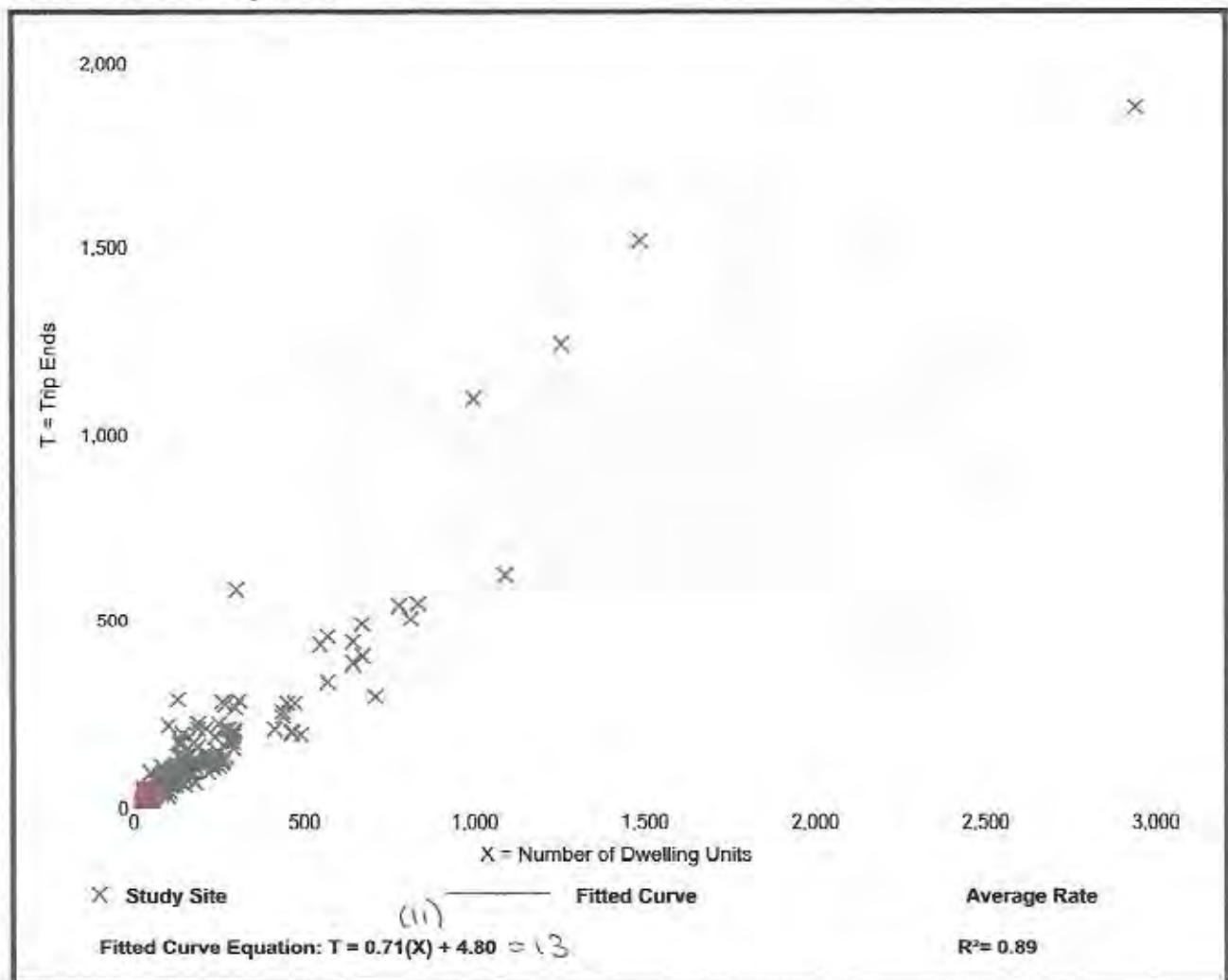
Vehicle Trip Ends vs: Dwelling Units  
 On a: Weekday,  
 Peak Hour of Adjacent Street Traffic,  
 One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban  
 Number of Studies: 173  
 Avg. Num. of Dwelling Units: 219  
 Directional Distribution: 25% entering, 75% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.74	0.33 - 2.27	0.27

## Data Plot and Equation



# Single-Family Detached Housing (210)

Vehicle Trip Ends vs: Dwelling Units

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 190

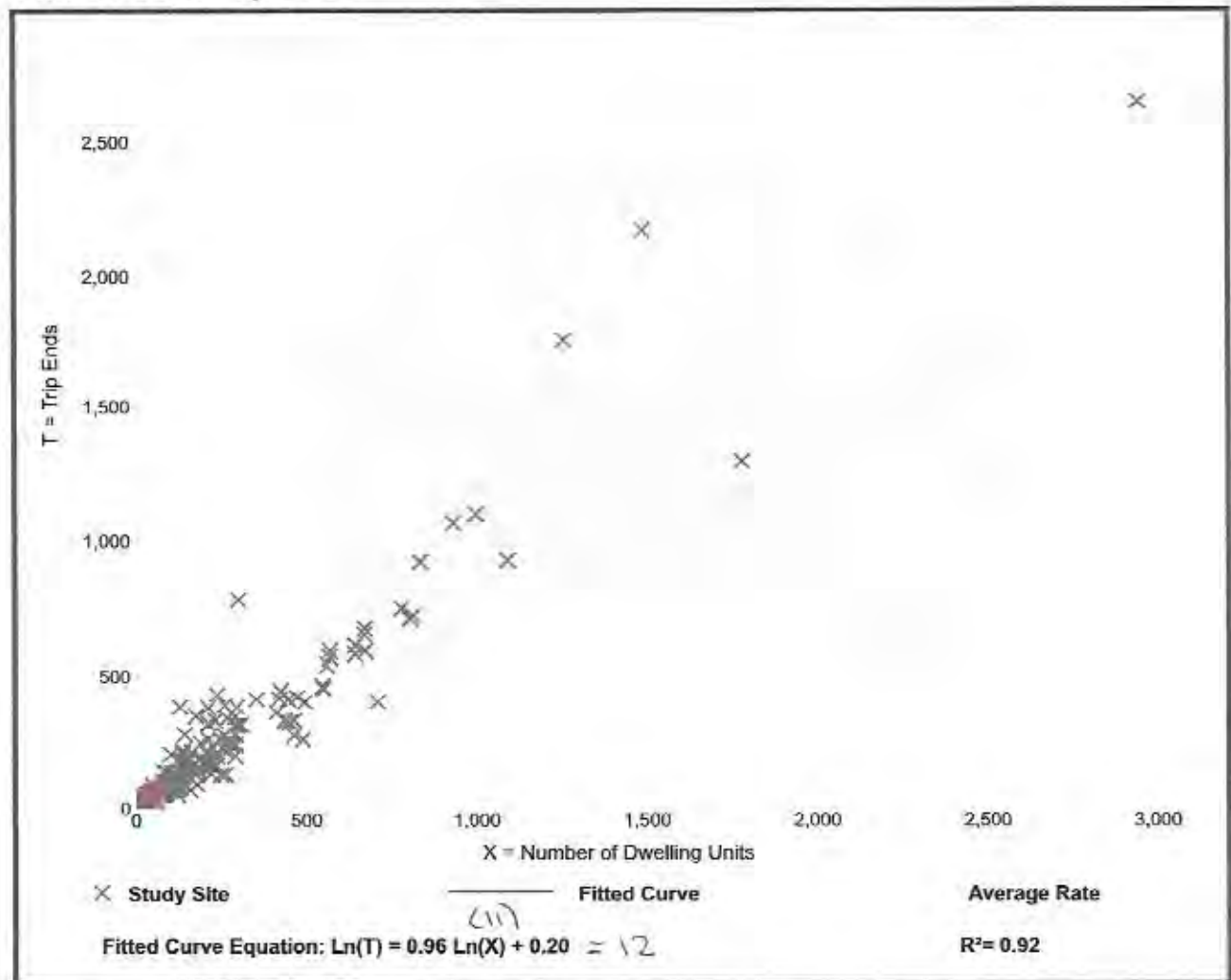
Avg. Num. of Dwelling Units: 242

Directional Distribution: 63% entering, 37% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.99	0.44 - 2.98	0.31

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

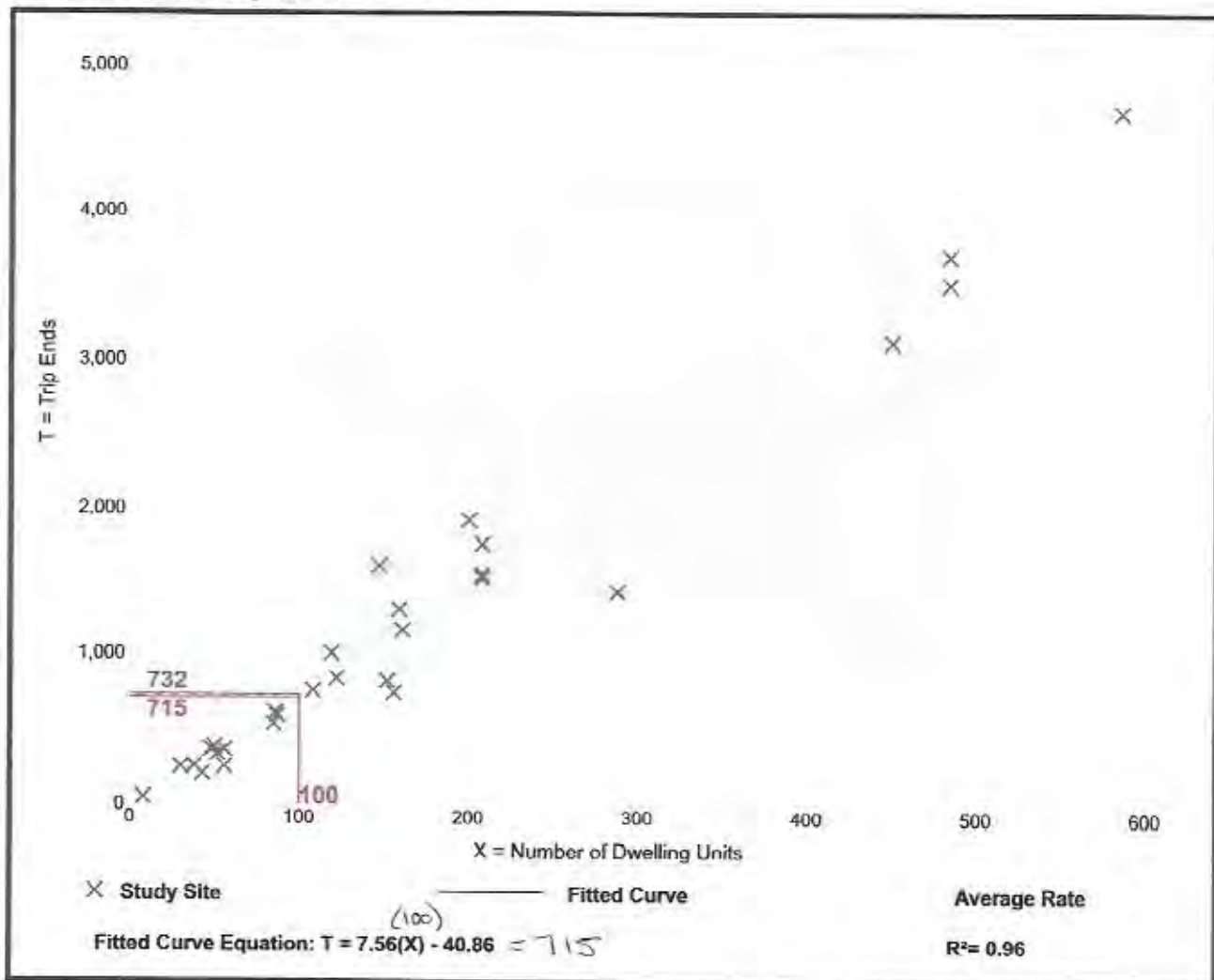
Vehicle Trip Ends vs: Dwelling Units  
On a: Weekday

Setting/Location: General Urban/Suburban  
Number of Studies: 29  
Avg. Num. of Dwelling Units: 168  
Directional Distribution: 50% entering, 50% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
7.32	4.45 - 10.97	1.31

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units  
 On a: Weekday,  
 Peak Hour of Adjacent Street Traffic,  
 One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

Number of Studies: 42

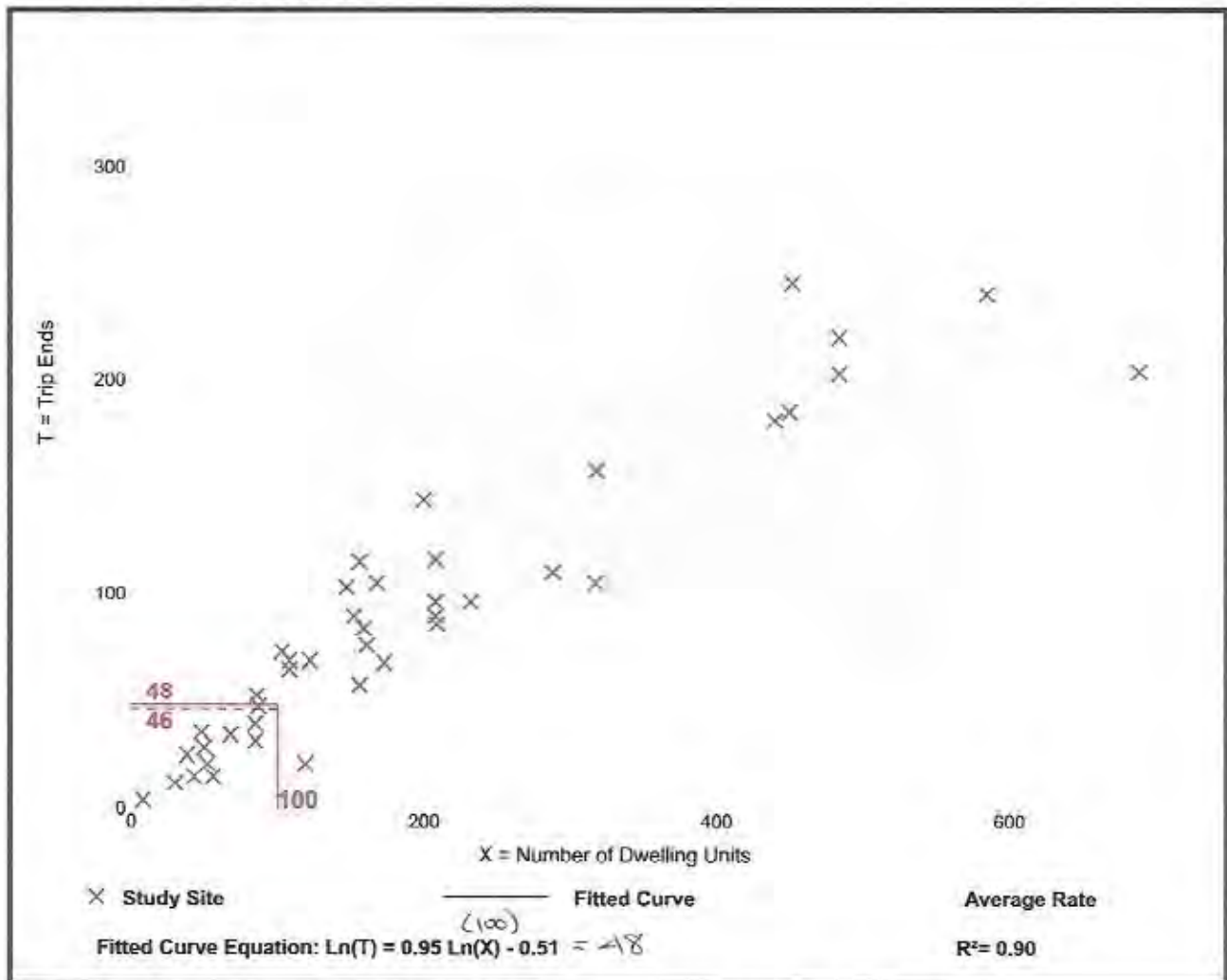
Avg. Num. of Dwelling Units: 199

Directional Distribution: 23% entering, 77% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.46	0.18 - 0.74	0.12

## Data Plot and Equation



# Multifamily Housing (Low-Rise) (220)

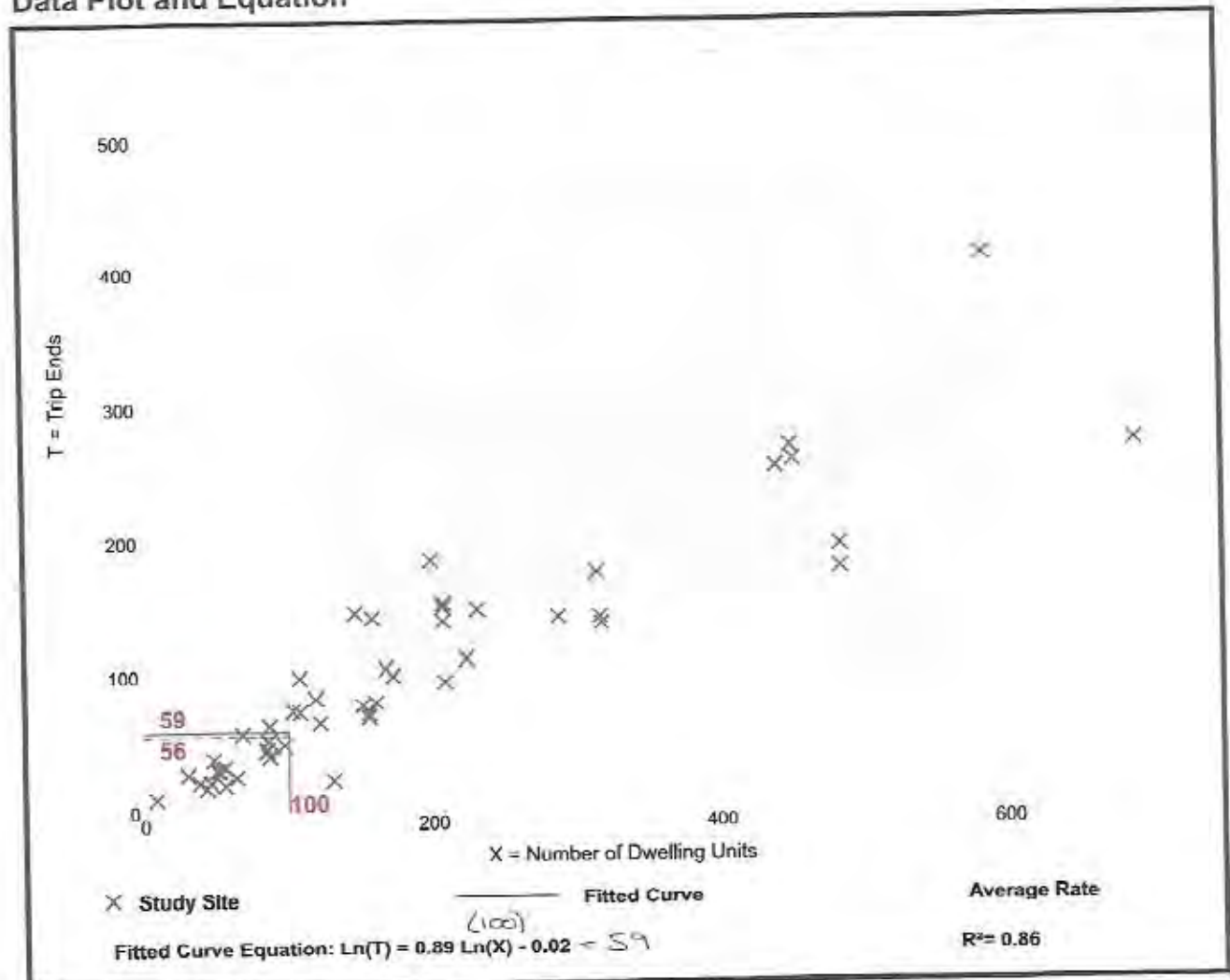
Vehicle Trip Ends vs: Dwelling Units  
 On a: Weekday,  
 Peak Hour of Adjacent Street Traffic,  
 One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban  
 Number of Studies: 50  
 Avg. Num. of Dwelling Units: 187  
 Directional Distribution: 63% entering, 37% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.56	0.18 - 1.25	0.16

## Data Plot and Equation





# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9		0	0	1	1	0	1	1	0
Number of Lanes		0	0	0		0	1	0		0	0	1	1				
Configuration							LR				T	R		L	T		
Volume (veh/h)						16		35			88	15		27	264		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)							0										
Right Turn Channelized											No						
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								57								30
Capacity, c (veh/h)								780								1475
v/c Ratio								0.07								0.02
95% Queue Length, Q <sub>95</sub> (veh)								0.2								0.1
Control Delay (s/veh)								10.0								7.5
Level of Service (LOS)								A								A
Approach Delay (s/veh)								10.0								0.7
Approach LOS								A								



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9		0	0	1	1	0	1	1	0
Number of Lanes		0	0	0		0	1	0		0	0	1	1	0			0
Configuration							LR					T	R		L	T	
Volume (veh/h)						24		60			296	51			31	115	
Percent Heavy Vehicles (%)						2		2							2		
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2									4.1
Critical Headway (sec)						6.42		6.22									4.12
Base Follow-Up Headway (sec)						3.5		3.3									2.2
Follow-Up Headway (sec)						3.52		3.32									2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								93									34
Capacity, c (veh/h)								634									1173
v/c Ratio								0.15									0.03
95% Queue Length, Q <sub>95</sub> (veh)								0.5									0.1
Control Delay (s/veh)								11.7									8.2
Level of Service (LOS)								B									A
Approach Delay (s/veh)								11.7									1.7
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement									1U	1	2	3	4U	4	5	6
Priority		10	11	12		7	8	9						1	1	0
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0
Configuration							LR				T	R		L	T	
Volume (veh/h)						16		38			136	15		37	423	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized											No					
Median Type   Storage						Undivided										

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								60								41
Capacity, c (veh/h)								648								1410
v/c Ratio								0.09								0.03
95% Queue Length, Q <sub>95</sub> (veh)								0.3								0.1
Control Delay (s/veh)								11.1								7.6
Level of Service (LOS)								B								A
Approach Delay (s/veh)								11.1								0.6
Approach LOS								B								



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						24		70			446	51		37	205		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2									4.1
Critical Headway (sec)						6.42		6.22									4.12
Base Follow-Up Headway (sec)						3.5		3.3									2.2
Follow-Up Headway (sec)						3.52		3.32									2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								104									41
Capacity, c (veh/h)								487									1018
v/c Ratio								0.21									0.04
95% Queue Length, Q <sub>95</sub> (veh)								0.8									0.1
Control Delay (s/veh)								14.4									8.7
Level of Service (LOS)								B									A
Approach Delay (s/veh)								14.4									1.3
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement									1U	1	2	3	4U	4	5	6
Priority		10	11	12		7	8	9						1	1	0
Number of Lanes		0	0	0		0	1	0		0	1	1		0	1	0
Configuration							LR				T	R		L	T	
Volume (veh/h)						16		46			140	15		39	357	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized											No					
Median Type   Storage							Undivided									

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

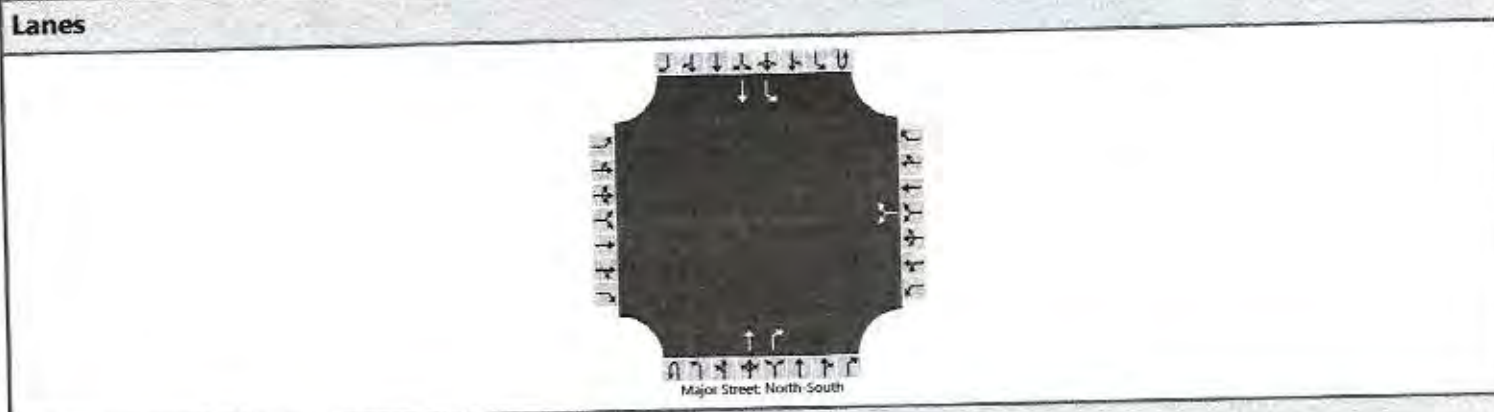
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								69								43
Capacity, c (veh/h)								695								1405
v/c Ratio								0.10								0.03
95% Queue Length, Q <sub>95</sub> (veh)								0.3								0.1
Control Delay (s/veh)								10.7								7.6
Level of Service (LOS)								B								A
Approach Delay (s/veh)								10.7								0.8
Approach LOS								B								



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						24		66			378	51		35	168		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1	
Critical Headway (sec)						6.42		6.22								4.12	
Base Follow-Up Headway (sec)						3.5		3.3								2.2	
Follow-Up Headway (sec)						3.52		3.32								2.22	

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								100								39	
Capacity, c (veh/h)								548								1086	
v/c Ratio								0.18								0.04	
95% Queue Length, Q <sub>95</sub> (veh)								0.7								0.1	
Control Delay (s/veh)								13.0								8.4	
Level of Service (LOS)								B								A	
Approach Delay (s/veh)								13.0								1.5	
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						16		49			188	15		49	516		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2									4.1
Critical Headway (sec)						6.42		6.22									4.12
Base Follow-Up Headway (sec)						3.5		3.3									2.2
Follow-Up Headway (sec)						3.52		3.32									2.22

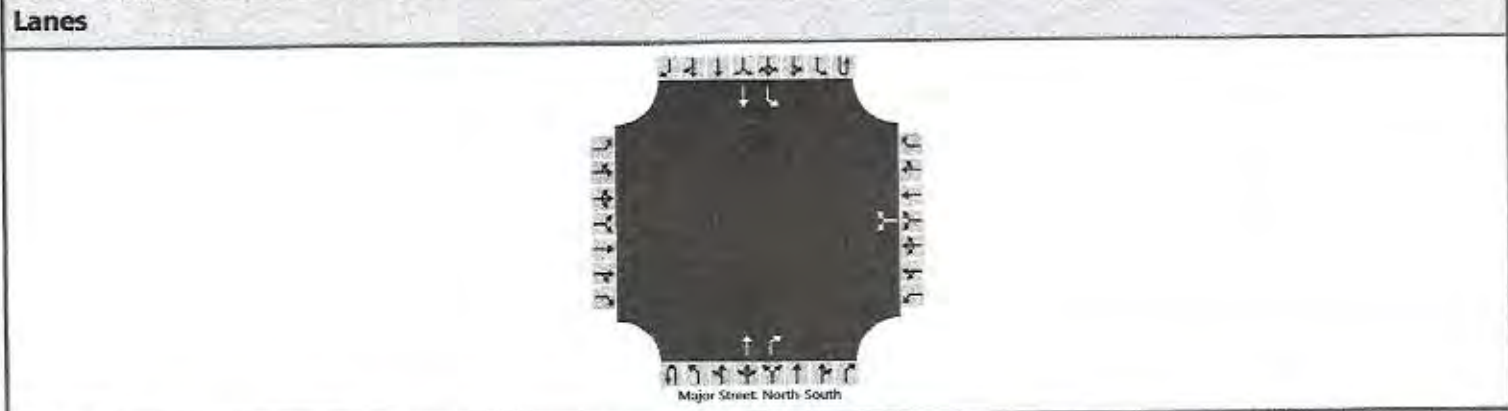
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								72									54
Capacity, c (veh/h)								579									1343
v/c Ratio								0.12									0.04
95% Queue Length, Q <sub>95</sub> (veh)								0.4									0.1
Control Delay (s/veh)								12.1									7.8
Level of Service (LOS)								B									A
Approach Delay (s/veh)								12.1									0.7
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	40	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						24		76			528	51		41	258		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized										No							
Median Type   Storage					Undivided												

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)							111								46	
Capacity, c (veh/h)							420								941	
v/c Ratio							0.26								0.05	
95% Queue Length, Q <sub>95</sub> (veh)							1.1								0.2	
Control Delay (s/veh)							16.6								9.0	
Level of Service (LOS)							C								A	
Approach Delay (s/veh)							16.6								1.2	
Approach LOS							C									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						16		46			140	15		39	357		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2									4.1
Critical Headway (sec)						6.42		6.22									4.12
Base Follow-Up Headway (sec)						3.5		3.3									2.2
Follow-Up Headway (sec)						3.52		3.32									2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								69									43
Capacity, c (veh/h)								695									1405
v/c Ratio								0.10									0.03
95% Queue Length, Q <sub>95</sub> (veh)								0.3									0.1
Control Delay (s/veh)								10.7									7.6
Level of Service (LOS)								B									A
Approach Delay (s/veh)								10.7									0.8
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0	
Configuration							LR				T	R		L	T		
Volume (veh/h)						24		66			378	51		35	168		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized											No						
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1	
Critical Headway (sec)						6.42		6.22								4.12	
Base Follow-Up Headway (sec)						3.5		3.3								2.2	
Follow-Up Headway (sec)						3.52		3.32								2.22	

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								100									39
Capacity, c (veh/h)								548									1086
v/c Ratio								0.18									0.04
95% Queue Length, Q <sub>95</sub> (veh)								0.7									0.1
Control Delay (s/veh)								13.0									8.4
Level of Service (LOS)								B									A
Approach Delay (s/veh)								13.0									1.5
Approach LOS								B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement									1U	1	2	3	4U	4	5	6
Priority		10	11	12		7	8	9						1	1	0
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0
Configuration							LR				T	R		L	T	
Volume (veh/h)						16		49			188	15		49	516	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)						0										
Right Turn Channelized											No					
Median Type   Storage					Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)								72								54
Capacity, c (veh/h)								579								1343
v/c Ratio								0.12								0.04
95% Queue Length, Q <sub>95</sub> (veh)								0.4								0.1
Control Delay (s/veh)								12.1								7.8
Level of Service (LOS)								B								A
Approach Delay (s/veh)								12.1								0.7
Approach LOS								B								



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & White Lake
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	White Lake Parkway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement									1U	1	2	3	4U	4	5	6
Priority		10	11	12		7	8	9								
Number of Lanes		0	0	0		0	1	0	0	0	1	1	0	1	1	0
Configuration							LR				T	R		L	T	
Volume (veh/h)						24		76			528	51		41	258	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)	0															
Right Turn Channelized	No															
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)					7.1	6.2									4.1		
Critical Headway (sec)					6.42	6.22									4.12		
Base Follow-Up Headway (sec)					3.5	3.3									2.2		
Follow-Up Headway (sec)					3.52	3.32									2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)					111									46		
Capacity, c (veh/h)					420									941		
v/c Ratio					0.26									0.05		
95% Queue Length, Q <sub>95</sub> (veh)					1.1									0.2		
Control Delay (s/veh)					16.6									9.0		
Level of Service (LOS)					C									A		
Approach Delay (s/veh)	16.6															
Approach LOS	C															



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		17	3	5		15	4	4		4	116	3		11	271	7	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1			
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12			
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2			
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22			

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			28				26			4				12			
Capacity, c (veh/h)			525				532			1252				1453			
v/c Ratio			0.05				0.05			0.00				0.01			
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.2			0.0				0.0			
Control Delay (s/veh)			12.2				12.1			7.9				7.5			
Level of Service (LOS)			B				B			A				A			
Approach Delay (s/veh)		12.2				12.1				0.3				0.3			
Approach LOS		B				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9									
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		10	5	9		5	6	3		23	304	29		4	132	9	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			27				16			26					4		
Capacity, c (vch/h)			521				457			1423					1189		
v/c Ratio			0.05				0.03			0.02					0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1			0.1					0.0		
Control Delay (s/veh)			12.3				13.2			7.6					8.0		
Level of Service (LOS)			B				B			A					A		
Approach Delay (s/veh)		12.3				13.2				0.5				0.2			
Approach LOS		B				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3		4	5	6	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		17	3	5		15	4	4		4	167	3		11	440	7	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1			
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12			
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2			
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22			

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			28				26			4					12		
Capacity, c (veh/h)			369				378			1067					1385		
v/c Ratio			0.08				0.07			0.00					0.01		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.2			0.0					0.0		
Control Delay (s/veh)			15.6				15.2			8.4					7.6		
Level of Service (LOS)			C				C			A					A		
Approach Delay (s/veh)		15.6				15.2				0.2				0.2			
Approach LOS		C				C											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3		4	5	6	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		10	5	9		5	6	3		23	464	29		4	228	9	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1					4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12					4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2					2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22					2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			27				16			26					4		
Capacity, c (veh/h)			360				310			1301					1022		
v/c Ratio			0.07				0.05			0.02					0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.2			0.1					0.0		
Control Delay (s/veh)			15.8				17.2			7.8					8.5		
Level of Service (LOS)			C				C			A					A		
Approach Delay (s/veh)		15.8				17.2				0.3				0.1			
Approach LOS		C				C				A				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	1	0		0	1	0		0	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		20	3	5		15	4	6		4	179	3		13	376	9	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

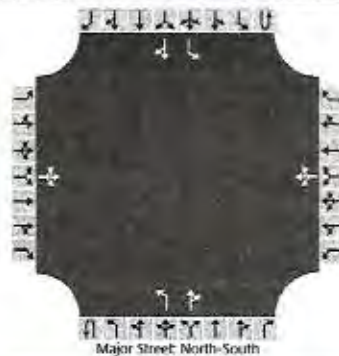
Flow Rate, v (veh/h)			31				28				4				14		
Capacity, c (veh/h)			394				423				1132				1370		
v/c Ratio			0.08				0.07				0.00				0.01		
95% Queue Length, Q <sub>95</sub> (veh)			0.3				0.2				0.0				0.0		
Control Delay (s/veh)			14.9				14.1				8.2				7.7		
Level of Service (LOS)			B				B				A				A		
Approach Delay (s/veh)		14.9				14.1				0.2				0.3			
Approach LOS		B				B				A				A			



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Cold Springs		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Cold Springs Drive		
Analysis Year	2030			North/South Street	Village Parkway		
Time Analyzed	PM Base			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound					
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R		
Movement																		
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6		
Number of Lanes		0	1	0		0	1	0		0	1	1	0		0	1	1	0
Configuration			LTR				LTR			L		TR			L		TR	
Volume (veh/h)		11	5	9		5	6	3		23	392	29			4	189	10	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2					2			
Proportion Time Blocked																		
Percent Grade (%)		0				0												
Right Turn Channelized																		
Median Type   Storage		Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1					4.1			
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12					4.12			
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2					2.2			
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22					2.22			

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			28				16				26					4		
Capacity, c (veh/h)			418				367				1348					1094		
v/c Ratio			0.07				0.04				0.02					0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1				0.1					0.0		
Control Delay (s/veh)			14.2				15.2				7.7					8.3		
Level of Service (LOS)			B				C				A					A		
Approach Delay (s/veh)		14.2				15.2				0.4				0.2				
Approach LOS		B				C												



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement									1U	1	2	3	4U	4	5	6
Priority		10	11	12		7	8	9		1	1	0	0	1	1	0
Number of Lanes		0	1	0		0	1	0		0	1	1		0		
Configuration			LTR				LTR			L		TR		L		TR
Volume (veh/h)		20	3	5		15	4	6		4	230	3		13	545	9
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized																
Median Type   Storage		Undivided														

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			31				28			4					14		
Capacity, c (veh/h)			274				301			964					1306		
v/c Ratio			0.11				0.09			0.00					0.01		
95% Queue Length, Q <sub>95</sub> (veh)			0.4				0.3			0.0					0.0		
Control Delay (s/veh)			19.8				18.2			8.8					7.8		
Level of Service (LOS)			C				C			A					A		
Approach Delay (s/veh)		19.8				18.2				0.1				0.2			
Approach LOS		C				C											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9		1	1	0		1	1	0	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		11	5	9		5	6	3		23	552	29		4	285	10	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			28			16			26					4			
Capacity, c (veh/h)			285			247			1232					940			
v/c Ratio			0.10			0.06			0.02					0.00			
95% Queue Length, Q <sub>95</sub> (veh)			0.3			0.2			0.1					0.0			
Control Delay (s/veh)			19.0			20.5			8.0					8.8			
Level of Service (LOS)			C			C			A					A			
Approach Delay (s/veh)		19.0				20.5				0.3				0.1			
Approach LOS		C				C				A				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9						1	1	0	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		20	3	5		15	4	6		4	179	3		13	376	9	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

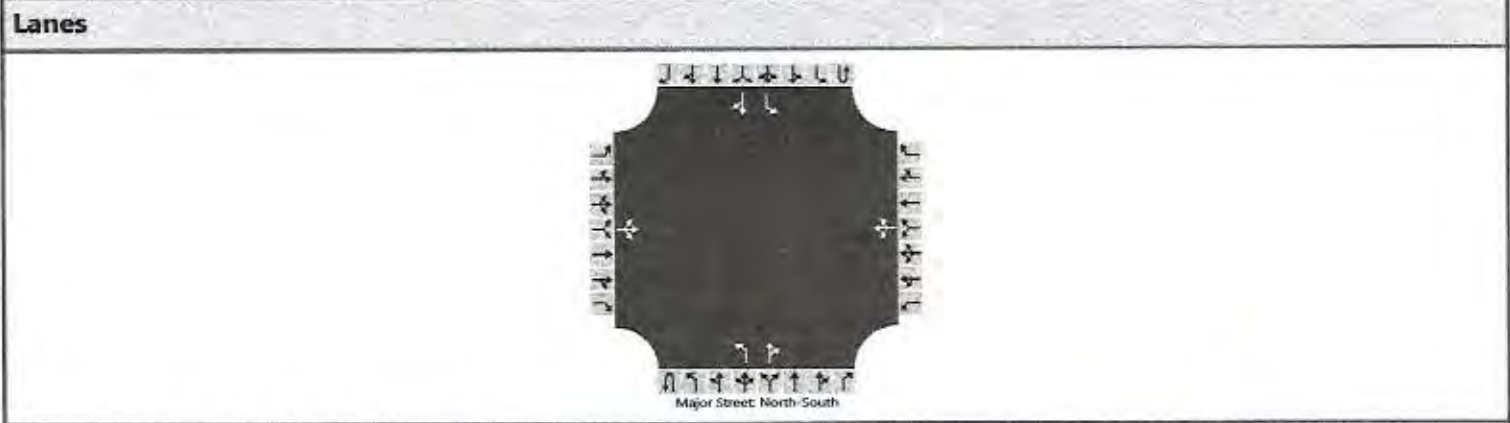
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			31				28				4					14	
Capacity, c (veh/h)			394				423				1132					1370	
v/c Ratio			0.08				0.07				0.00					0.01	
95% Queue Length, Q <sub>95</sub> (veh)			0.3				0.2				0.0					0.0	
Control Delay (s/veh)			14.9				14.1				8.2					7.7	
Level of Service (LOS)			B				B				A					A	
Approach Delay (s/veh)		14.9				14.1				0.2				0.3			
Approach LOS		B				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		11	5	9		5	6	3		23	392	29		4	189	10	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

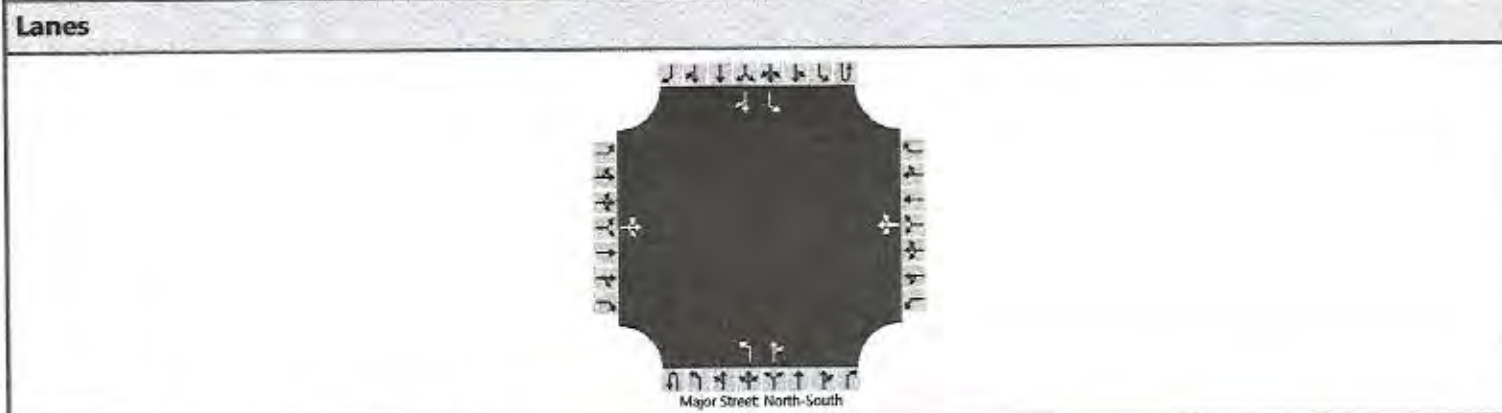
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			28				16				26				4		
Capacity, c (veh/h)			418				367				1348				1094		
v/c Ratio			0.07				0.04				0.02				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1				0.1				0.0		
Control Delay (s/veh)			14.2				15.2				7.7				8.3		
Level of Service (LOS)			B				C				A				A		
Approach Delay (s/veh)		14.2				15.2				0.4				0.2			
Approach LOS		B				C											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Cold Springs
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Cold Springs Drive
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0
Configuration			LTR				LTR			L		TR		L		TR
Volume (veh/h)		20	3	5		15	4	6		4	230	3		13	545	9
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			31				28				4				14	
Capacity, c (veh/h)			274				301				964				1306	
v/c Ratio			0.11				0.09				0.00				0.01	
95% Queue Length, Q <sub>95</sub> (veh)			0.4				0.3				0.0				0.0	
Control Delay (s/veh)			19.8				18.2				8.8				7.8	
Level of Service (LOS)			C				C				A				A	
Approach Delay (s/veh)			19.8				18.2				0.1				0.2	
Approach LOS			C				C									



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH	Intersection	Village & Cold Springs				
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County				
Date Performed	10/19/2020	East/West Street	Cold Springs Drive				
Analysis Year	2040	North/South Street	Village Parkway				
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90				
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25				
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9						1	1	0	
Number of Lanes		0	1	0		0	1	0	0	1	1	0	0	1	1	0	
Configuration			LTR				LTR			L		TR		L		TR	
Volume (veh/h)		11	5	9		5	6	3		23	552	29		4	285	10	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1					4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12					4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2					2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22					2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			28				16				26				4		
Capacity, c (veh/h)			285				247				1232				940		
v/c Ratio			0.10				0.06				0.02				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.3				0.2				0.1				0.0		
Control Delay (s/veh)			19.0				20.5				8.0				8.8		
Level of Service (LOS)			C				C				A				A		
Approach Delay (s/veh)		19.0				20.5				0.3				0.1			
Approach LOS		C				C				A				A			



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Access		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Project Access		
Analysis Year	2020			North/South Street	Village Parkway		
Time Analyzed	AM Existing + Project			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	0	0	0	0	1	0	0	0	1	0	
Configuration			LR							LT						TR	
Volume (veh/h)		16		143						43	145				315	5	
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1						
Critical Headway (sec)		6.42		6.22							4.12						
Base Follow-Up Headway (sec)		3.5		3.3							2.2						
Follow-Up Headway (sec)		3.52		3.32							2.22						

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			177								48						
Capacity, c (veh/h)			653								1203						
v/c Ratio			0.27								0.04						
95% Queue Length, Q <sub>95</sub> (veh)			1.1								0.1						
Control Delay (s/veh)			12.5								8.1						
Level of Service (LOS)			B								A						
Approach Delay (s/veh)		12.5									2.1						
Approach LOS		B									A						



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2020
Time Analyzed	PM Existing + Project
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Village & Access
Jurisdiction	Washoe County
East/West Street	Project Access
North/South Street	Village Parkway
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound					
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R		
Movement																		
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6		
Number of Lanes		0	1	0		0	0	0	0	0	1	0	0	0	1	0		
Configuration			LR								LT					TR		
Volume (veh/h)		9		81							136	341				160	15	
Percent Heavy Vehicles (%)		2		2							2							
Proportion Time Blocked																		
Percent Grade (%)		0																
Right Turn Channelized																		
Median Type   Storage		Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1						
Critical Headway (sec)		6.42		6.22							4.12						
Base Follow-Up Headway (sec)		3.5		3.3							2.2						
Follow-Up Headway (sec)		3.52		3.32							2.22						

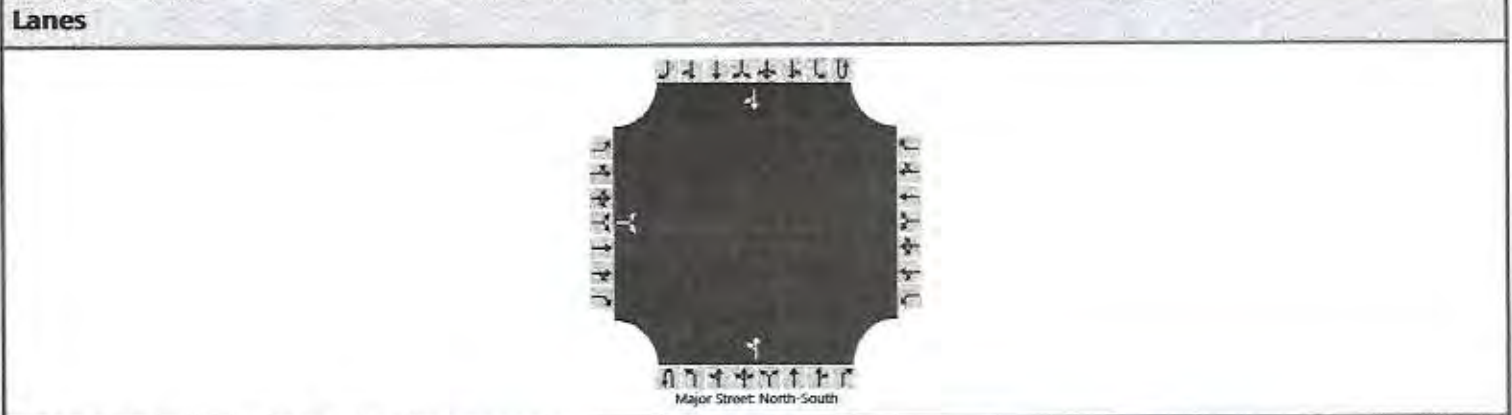
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			100								151						
Capacity, c (veh/h)			709								1379						
v/c Ratio			0.14								0.11						
95% Queue Length, Q <sub>95</sub> (veh)			0.5								0.4						
Control Delay (s/veh)			10.9								7.9						
Level of Service (LOS)			B								A						
Approach Delay (s/veh)		10.9									3.0						
Approach LOS		B									A						



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Access		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Project Access		
Analysis Year	2030			North/South Street	Village Parkway		
Time Analyzed	AM Base + Project			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	0	0		0	1	0		0	1	0	
Configuration			LR							LT						TR	
Volume (veh/h)		16		143						43	213				424	5	
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized																	
Median Type   Storage		Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1		6.2							4.1					
Critical Headway (sec)		6.42		6.22							4.12					
Base Follow-Up Headway (sec)		3.5		3.3							2.2					
Follow-Up Headway (sec)		3.52		3.32							2.22					

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			177								48							
Capacity, c (veh/h)			548								1086							
v/c Ratio			0.32								0.04							
95% Queue Length, Q <sub>95</sub> (veh)			1.4								0.1							
Control Delay (s/veh)			14.7								8.5							
Level of Service (LOS)			B								A							
Approach Delay (s/veh)		14.7									1.8							
Approach LOS		B																



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Access
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Project Access
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement									1U	1	2	3	4U	4	5	6	
Priority		10	11	12		7	8	9									
Number of Lanes		0	1	0		0	0	0	0	0	1	0	0	0	1	0	
Configuration			LR							LT						TR	
Volume (veh/h)		9		81					136	430					218	15	
Percent Heavy Vehicles (%)		2		2					2								
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2						4.1						
Critical Headway (sec)		6.42		6.22						4.12						
Base Follow-Up Headway (sec)		3.5		3.3						2.2						
Follow-Up Headway (sec)		3.52		3.32						2.22						

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			100							151							
Capacity, c (veh/h)			625							1306							
v/c Ratio			0.16							0.12							
95% Queue Length, Q <sub>95</sub> (veh)			0.6							0.4							
Control Delay (s/veh)			11.9							8.1							
Level of Service (LOS)			B							A							
Approach Delay (s/veh)		11.9								2.9							
Approach LOS		B								A							



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Access
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Project Access
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound					
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R		
Movement																		
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6		
Number of Lanes		0	1	0		0	0	0	0	0	1	0	0	0	1	0		
Configuration			LR							LT						TR		
Volume (veh/h)		16		143						43	213					424	5	
Percent Heavy Vehicles (%)		2		2						2								
Proportion Time Blocked																		
Percent Grade (%)		0																
Right Turn Channelized																		
Median Type   Storage		Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1						
Critical Headway (sec)		6.42		6.22							4.12						
Base Follow-Up Headway (sec)		3.5		3.3							2.2						
Follow-Up Headway (sec)		3.52		3.32							2.22						

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			177								48							
Capacity, c (veh/h)			548								1086							
v/c Ratio			0.32								0.04							
95% Queue Length, Q <sub>95</sub> (veh)			1.4								0.1							
Control Delay (s/veh)			14.7								8.5							
Level of Service (LOS)			B								A							
Approach Delay (s/veh)		14.7									1.8							
Approach LOS		B									A							



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	PM Base + Project
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Village & Access
Jurisdiction	Washoe County
East/West Street	Project Access
North/South Street	Village Parkway
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	40	4	5	6	
Number of Lanes		0	1	0		0	0	0		0	1	0		0	1	0	
Configuration			LR							LT						TR	
Volume (veh/h)		9		81						136	430				218	15	
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1					
Critical Headway (sec)		6.42		6.22							4.12					
Base Follow-Up Headway (sec)		3.5		3.3							2.2					
Follow-Up Headway (sec)		3.52		3.32							2.22					

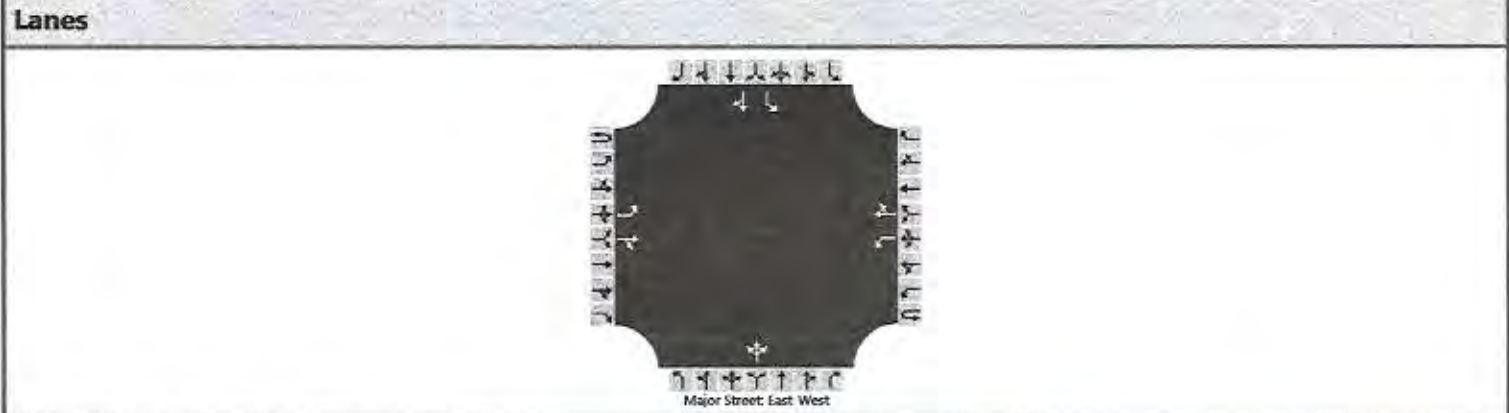
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			100								151							
Capacity, c (veh/h)			625								1306							
v/c Ratio			0.16								0.12							
95% Queue Length, Q <sub>95</sub> (veh)			0.6								0.4							
Control Delay (s/veh)			11.9								8.1							
Level of Service (LOS)			B								A							
Approach Delay (s/veh)		11.9									2.9							
Approach LOS		B									A							



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2020	North/South Street	New Forest/Georgetown
Time Analyzed	AM Existing	Peak Hour Factor	0.85
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		71	65	1		4	157	0		4	7	2		1	11	128
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		84				5				15				1		164	
Capacity, c (veh/h)		1390				1521				468				492		858	
v/c Ratio		0.06				0.00				0.03				0.00		0.19	
95% Queue Length, Q <sub>95</sub> (veh)		0.2				0.0				0.1				0.0		0.7	
Control Delay (s/veh)		7.8				7.4				12.9				12.3		10.2	
Level of Service (LOS)		A				A				B				B		B	
Approach Delay (s/veh)		4.0				0.2				12.9				10.2			
Approach LOS										B				B			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2020	North/South Street	New Forest/Georgetown
Time Analyzed	PM Existing	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6	7	8	9		10	11	12	
Priority	0	1	1	0	0	1	1	0	0	1	0		1	1	0	
Configuration		L		TR		L		TR		LTR			L		TR	
Volume (veh/h)		160	154	3		17	81	4		2	19	10		2	3	62
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		178				19					34			2		72	
Capacity, c (veh/h)		1500				1402					412			312		965	
v/c Ratio		0.12				0.01					0.08			0.01		0.07	
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0					0.3			0.0		0.2	
Control Delay (s/veh)		7.7				7.6					14.5			16.6		9.0	
Level of Service (LOS)		A				A					B			C		A	
Approach Delay (s/veh)		3.9				1.3				14.5				9.3			
Approach LOS		A				A				B				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2020	North/South Street	New Forest/Georgetown
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.85
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		79	81	1		4	186	0		4	7	2		1	11	130
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		93				5					15				1		166	
Capacity, c (veh/h)		1351				1497					419				437		821	
v/c Ratio		0.07				0.00					0.04				0.00		0.20	
95% Queue Length, Q <sub>95</sub> (veh)		0.2				0.0					0.1				0.0		0.8	
Control Delay (s/veh)		7.9				7.4					13.9				13.3		10.5	
Level of Service (LOS)		A				A					B				B		B	
Approach Delay (s/veh)		3.9				0.2					13.9				10.5			
Approach LOS		A				A					B				B			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2020	North/South Street	New Forest/Georgetown
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Priority																	
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR	
Volume (veh/h)		164	183	3		17	104	4		2	19	10		2	3	69	
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2	
Proportion Time Blocked																	
Percent Grade (%)										0				0			
Right Turn Channelized																	
Median Type   Storage	Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		182				19					34			2		80	
Capacity, c (veh/h)		1468				1365					376			278		934	
v/c Ratio		0.12				0.01					0.09			0.01		0.09	
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0					0.3			0.0		0.3	
Control Delay (s/veh)		7.8				7.7					15.5			18.0		9.2	
Level of Service (LOS)		A				A					C			C		A	
Approach Delay (s/veh)		3.7				1.0				15.5				9.5			
Approach LOS		A				A				C				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2030	North/South Street	New Forest/Georgetown
Time Analyzed	AM Base	Peak Hour Factor	0.85
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR	
Volume (veh/h)		139	65	1		4	157	6		4	10	2		6	13	237	
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2	
Proportion Time Blocked																	
Percent Grade (%)										0				0			
Right Turn Channelized																	
Median Type   Storage	Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1					7.1	6.5	6.2			7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12					7.12	6.52	6.22			7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2					3.5	4.0	3.3			3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22					3.52	4.02	3.32			3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		164				5					19				7		294
Capacity, c (veh/h)		1382				1521					318				360		854
v/c Ratio		0.12				0.00					0.06				0.02		0.34
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0					0.2				0.1		1.5
Control Delay (s/veh)		8.0				7.4					17.0				15.2		11.4
Level of Service (LOS)		A				A					C				C		B
Approach Delay (s/veh)		5.4				0.2				17.0				11.5			
Approach LOS		A				A				C				B			



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & New Forest		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Parkway		
Analysis Year	2030			North/South Street	New Forest/Georgetown		
Time Analyzed	PM Base			Peak Hour Factor	0.90		
Intersection Orientation	East-West			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0	0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		249	154	3		17	81	5		2	20	10		3	4	120
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		277				19					36			3		138	
Capacity, c (veh/h)		1498				1402					298			211		964	
v/c Ratio		0.18				0.01					0.12			0.02		0.14	
95% Queue Length, Q <sub>95</sub> (veh)		0.7				0.0					0.4			0.0		0.5	
Control Delay (s/veh)		7.9				7.6					18.7			22.3		9.4	
Level of Service (LOS)		A				A					C			C		A	
Approach Delay (s/veh)		4.9				1.3				18.7				9.7			
Approach LOS		A				A				C				A			



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2030
Time Analyzed	AM Base + Project
Intersection Orientation	East-West
Project Description	

## Site Information

Intersection	Village & New Forest
Jurisdiction	Washoe County
East/West Street	Village Parkway
North/South Street	New Forest/Georgetown
Peak Hour Factor	0.85
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		147	81	1		4	186	6		4	10	2		6	13	239
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1					7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12					7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2					3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22					3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		173				5					19				7		296	
Capacity, c (veh/h)		1343				1497					282				318		817	
v/c Ratio		0.13				0.00					0.07				0.02		0.36	
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0					0.2				0.1		1.7	
Control Delay (s/veh)		8.1				7.4					18.7				16.6		11.9	
Level of Service (LOS)		A				A					C				C		B	
Approach Delay (s/veh)		5.2				0.2					18.7				12.0			
Approach LOS		A				A					C				B			



# HCS7 Two-Way Stop-Control Report

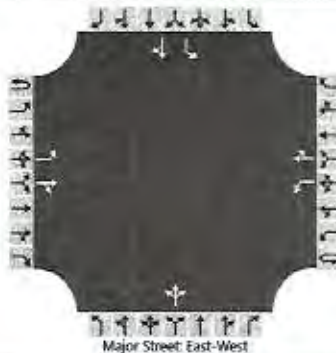
## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2030
Time Analyzed	PM Base + Project
Intersection Orientation	East-West
Project Description	

## Site Information

Intersection	Village & New Forest
Jurisdiction	Washoe County
East/West Street	Village Parkway
North/South Street	New Forest/Georgetown
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		253	183	3		17	104	5		2	20	10		3	4	127
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1					7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12					7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2					3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22					3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		281				19					36				3		146
Capacity, c (veh/h)		1466				1365					271				187		933
v/c Ratio		0.19				0.01					0.13				0.02		0.16
95% Queue Length, Q <sub>95</sub> (veh)		0.7				0.0					0.4				0.1		0.6
Control Delay (s/veh)		8.0				7.7					20.3				24.6		9.6
Level of Service (LOS)		A				A					C				C		A
Approach Delay (s/veh)		4.6				1.0				20.3				9.9			
Approach LOS		A				A				C				A			



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	AM Base
Intersection Orientation	East-West
Project Description	

## Site Information

Intersection	Village & New Forest
Jurisdiction	Washoe County
East/West Street	Village Parkway
North/South Street	New Forest/Georgetown
Peak Hour Factor	0.85
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Priority																	
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR	
Volume (veh/h)		139	65	1		4	157	6		4	10	2		6	13	237	
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2	
Proportion Time Blocked																	
Percent Grade (%)										0				0			
Right Turn Channelized																	
Median Type   Storage	Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1					7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12					7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2					3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22					3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		164				5					19				7		294	
Capacity, c (veh/h)		1382				1521					318				360		854	
v/c Ratio		0.12				0.00					0.06				0.02		0.34	
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0					0.2				0.1		1.5	
Control Delay (s/veh)		8.0				7.4					17.0				15.2		11.4	
Level of Service (LOS)		A				A					C			C			B	
Approach Delay (s/veh)		5.4				0.2					17.0				11.5			
Approach LOS		A				A					C				B			



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	PM Base
Intersection Orientation	East-West
Project Description	

## Site Information

Intersection	Village & New Forest
Jurisdiction	Washoe County
East/West Street	Village Parkway
North/South Street	New Forest/Georgetown
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Priority																	
Number of Lanes	0	1	1	0	0	1	1	0		0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR	
Volume (veh/h)		249	154	3		17	81	5		2	20	10		3	4	120	
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2	
Proportion Time Blocked																	
Percent Grade (%)										0				0			
Right Turn Channelized																	
Median Type   Storage	Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		277				19					36				3		138	
Capacity, c (veh/h)		1498				1402					298				211		964	
v/c Ratio		0.18				0.01					0.12				0.02		0.14	
95% Queue Length, Q <sub>95</sub> (veh)		0.7				0.0					0.4				0.0		0.5	
Control Delay (s/veh)		7.9				7.6					18.7				22.3		9.4	
Level of Service (LOS)		A				A					C				C		A	
Approach Delay (s/veh)		4.9				1.3					18.7				9.7			
Approach LOS		A				A					C				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & New Forest
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Parkway
Analysis Year	2040	North/South Street	New Forest/Georgetown
Time Analyzed	AM Base + Project	Peak Hour Factor	0.85
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6	7	8	9		10	11	12	
Priority	1U	1	2	3	4U	4	5	6	7	8	9		10	11	12	
Number of Lanes	0	1	1	0	0	1	1	0	0	1	0		1	1	0	
Configuration		L		TR		L		TR		LTR				L		TR
Volume (veh/h)		147	81	1		4	186	6		4	10	2		6	13	239
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)									0				0			
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		173				5				19				7		296
Capacity, c (veh/h)		1343				1497				282				318		817
v/c Ratio		0.13				0.00				0.07				0.02		0.36
95% Queue Length, Q <sub>95</sub> (veh)		0.4				0.0				0.2				0.1		1.7
Control Delay (s/veh)		8.1				7.4				18.7				16.6		11.9
Level of Service (LOS)		A				A				C				C		B
Approach Delay (s/veh)		5.2				0.2				18.7				12.0		
Approach LOS										C				B		



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & New Forest		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Parkway		
Analysis Year	2040			North/South Street	New Forest/Georgetown		
Time Analyzed	PM Base + Project			Peak Hour Factor	0.90		
Intersection Orientation	East-West			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	1	1	0	0	1	1	0	0	1	0		1	1	0	
Configuration		L		TR		L		TR			LTR			L		TR
Volume (veh/h)		253	183	3		17	104	5		2	20	10		3	4	127
Percent Heavy Vehicles (%)		2				2				2	2	2		2	2	2
Proportion Time Blocked																
Percent Grade (%)										0				0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1				4.1				7.1	6.5	6.2		7.1	6.5	6.2
Critical Headway (sec)		4.12				4.12				7.12	6.52	6.22		7.12	6.52	6.22
Base Follow-Up Headway (sec)		2.2				2.2				3.5	4.0	3.3		3.5	4.0	3.3
Follow-Up Headway (sec)		2.22				2.22				3.52	4.02	3.32		3.52	4.02	3.32

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		281				19				36				3		146
Capacity, c (veh/h)		1466				1365				271				187		933
v/c Ratio		0.19				0.01				0.13				0.02		0.16
95% Queue Length, Q <sub>95</sub> (veh)		0.7				0.0				0.4				0.1		0.6
Control Delay (s/veh)		8.0				7.7				20.3				24.6		9.6
Level of Service (LOS)		A				A				C				C		A
Approach Delay (s/veh)		4.6				1.0				20.3				9.9		
Approach LOS		A				A				C				A		



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1		0	1	0		0	1	0
Configuration						L		R				TR		L		T
Volume (veh/h)						5		27			138	5		21		164
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						7		36								28
Capacity, c (veh/h)						547		855								1383
v/c Ratio						0.01		0.04								0.02
95% Queue Length, Q <sub>95</sub> (veh)						0.0		0.1								0.1
Control Delay (s/veh)						11.7		9.4								7.7
Level of Service (LOS)						B		A								A
Approach Delay (s/veh)					9.8								0.9			
Approach LOS					A											



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Village Center		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Center Drive		
Analysis Year	2020			North/South Street	Village Parkway		
Time Analyzed	PM Existing			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L		T
Volume (veh/h)						15		23			102	14		11	40	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

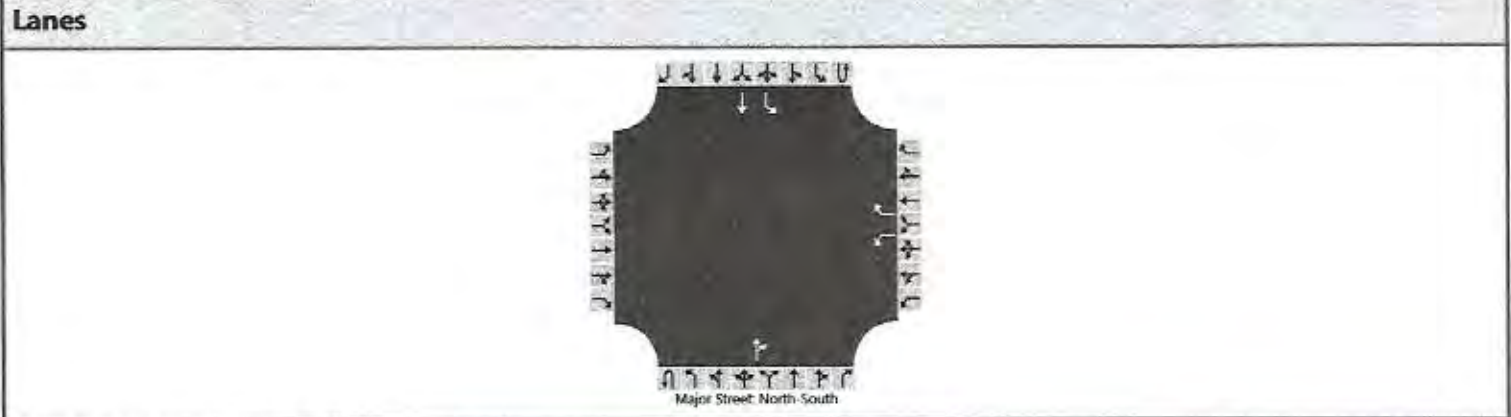
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						17		26							12	
Capacity, c (veh/h)						792		930							1457	
v/c Ratio						0.02		0.03							0.01	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.1							0.0	
Control Delay (s/veh)						9.6		9.0							7.5	
Level of Service (LOS)						A		A							A	
Approach Delay (s/veh)							9.2								1.6	
Approach LOS							A									



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Village Center		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Center Drive		
Analysis Year	2020			North/South Street	Village Parkway		
Time Analyzed	AM Existing + Project			Peak Hour Factor	0.75		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						11		27			153	6		26	187	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

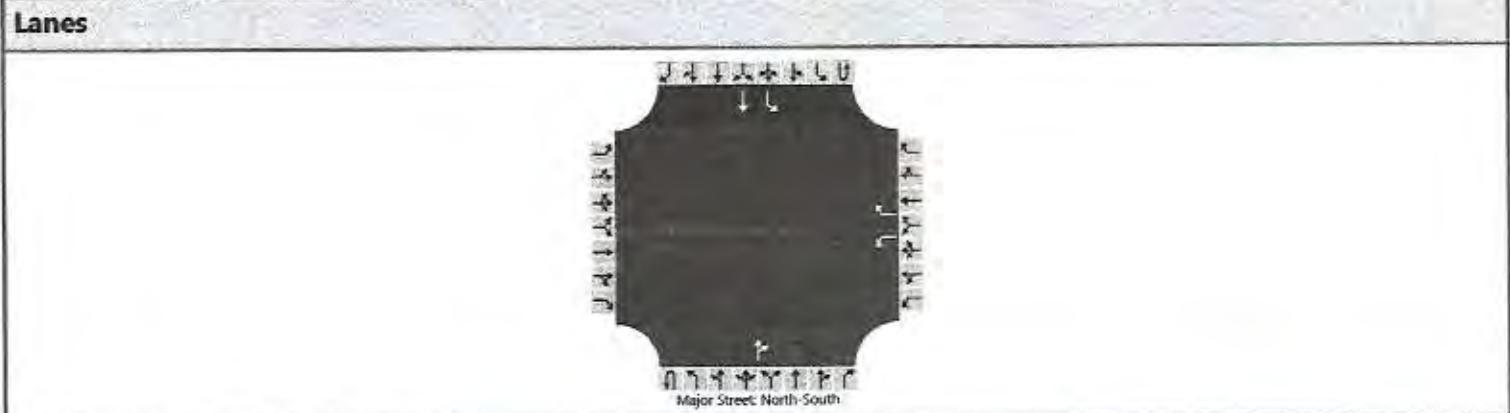
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						15		36							35	
Capacity, c (veh/h)						499		832							1358	
v/c Ratio						0.03		0.04							0.03	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.1							0.1	
Control Delay (s/veh)						12.4		9.5							7.7	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)					10.4								0.9			
Approach LOS					B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1		0	1	0		0	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						19		24			126	19		17	59	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

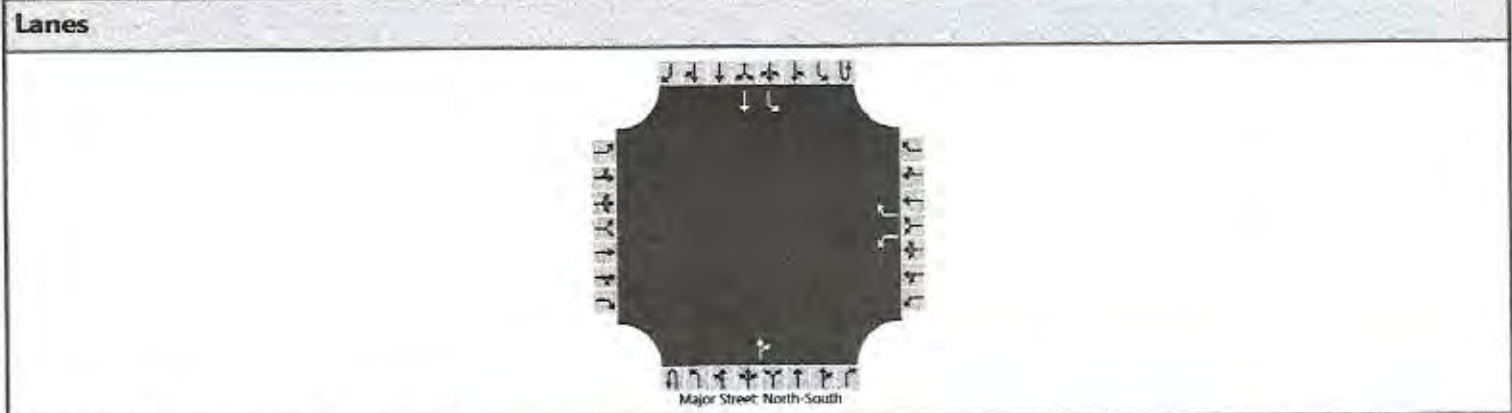
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						21		27							19	
Capacity, c (veh/h)						725		896							1418	
v/c Ratio						0.03		0.03							0.01	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.1							0.0	
Control Delay (s/veh)						10.1		9.1							7.6	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)							9.6								1.7	
Approach LOS							A									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						5		75			160	5		67	182	
Percent Heavy Vehicles (%)							2	2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						7		100							89	
Capacity, c (veh/h)						412		823							1349	
v/c Ratio						0.02		0.12							0.07	
95% Queue Length, Q <sub>95</sub> (veh)						0.0		0.4							0.2	
Control Delay (s/veh)						13.9		10.0							7.9	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)							10.2								2.1	
Approach LOS							B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						15		42			107	14		28	45	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)						0										
Right Turn Channelized						No										
Median Type   Storage					Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)					7.1	6.2							4.1			
Critical Headway (sec)					6.42	6.22							4.12			
Base Follow-Up Headway (sec)					3.5	3.3							2.2			
Follow-Up Headway (sec)					3.52	3.32							2.22			

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)					17	47							31			
Capacity, c (veh/h)					733	924							1450			
v/c Ratio					0.02	0.05							0.02			
95% Queue Length, Q <sub>95</sub> (veh)					0.1	0.2							0.1			
Control Delay (s/veh)					10.0	9.1							7.5			
Level of Service (LOS)					B	A							A			
Approach Delay (s/veh)					9.3								2.9			
Approach LOS					A								A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						11		75			175	6		72	205	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)					0											
Right Turn Channelized					No											
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

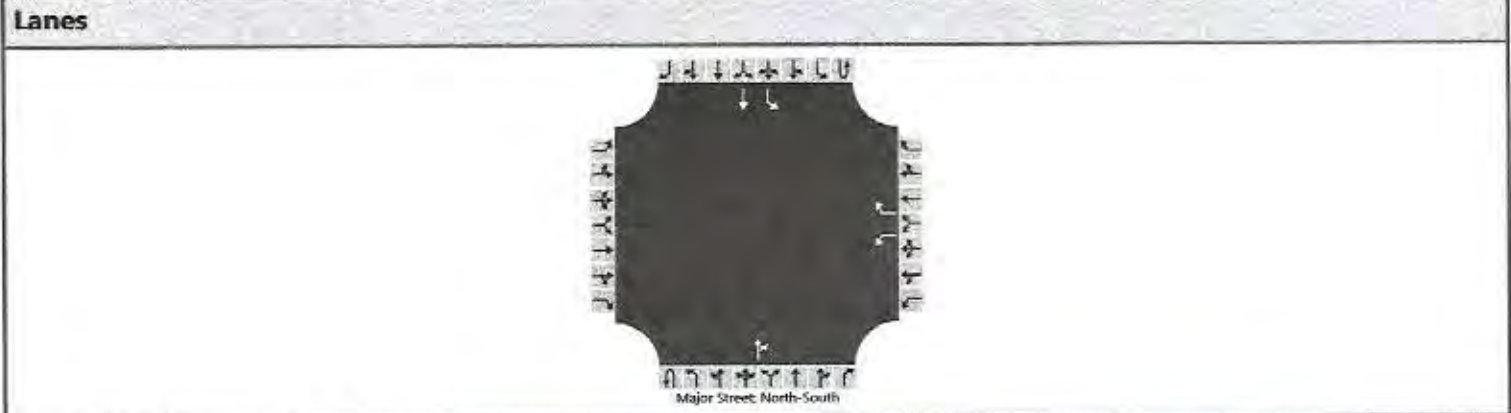
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						15		100							96	
Capacity, c (veh/h)						375		802							1325	
v/c Ratio						0.04		0.12							0.07	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.4							0.2	
Control Delay (s/veh)						15.0		10.1							7.9	
Level of Service (LOS)						B		B							A	
Approach Delay (s/veh)					10.8								2.1			
Approach LOS					B											



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Village Center		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Center Drive		
Analysis Year	2030			North/South Street	Village Parkway		
Time Analyzed	PM Base + Project			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						19		43			131	19		34	64	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						21		48							38	
Capacity, c (veh/h)						670		890							1411	
v/c Ratio						0.03		0.05							0.03	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.2							0.1	
Control Delay (s/veh)						10.5		9.3							7.6	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)							9.7								2.6	
Approach LOS							A									



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Village Center		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Center Drive		
Analysis Year	2040			North/South Street	Village Parkway		
Time Analyzed	AM Base			Peak Hour Factor	0.75		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1		0	1	0		0	1	0
Configuration						L		R				TR		L		T
Volume (veh/h)						5		75			160	5		67		182
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						7		100							89	
Capacity, c (veh/h)						412		823							1349	
v/c Ratio						0.02		0.12							0.07	
95% Queue Length, Q <sub>95</sub> (veh)						0.0		0.4							0.2	
Control Delay (s/veh)						13.9		10.0							7.9	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)							10.2									2.1
Approach LOS							B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		1	0	1		0	1	0		0	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						15		42			107	14		28	45	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2								4.1
Critical Headway (sec)						6.42		6.22								4.12
Base Follow-Up Headway (sec)						3.5		3.3								2.2
Follow-Up Headway (sec)						3.52		3.32								2.22

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						17		47								31
Capacity, c (veh/h)						733		924								1450
v/c Ratio						0.02		0.05								0.02
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.2								0.1
Control Delay (s/veh)						10.0		9.1								7.5
Level of Service (LOS)						B		A								A
Approach Delay (s/veh)					9.3								2.9			
Approach LOS					A											



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Village Center		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Village Center Drive		
Analysis Year	2040			North/South Street	Village Parkway		
Time Analyzed	AM Base + Project			Peak Hour Factor	0.75		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		1	0	1		0	1	0		0	1	1	0
Configuration						L		R				TR		L		T	
Volume (veh/h)						11		75			175	6		72		205	
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)							0										
Right Turn Channelized							No										
Median Type   Storage							Undivided										

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						15		100							96	
Capacity, c (veh/h)						375		802							1325	
v/c Ratio						0.04		0.12							0.07	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.4							0.2	
Control Delay (s/veh)						15.0		10.1							7.9	
Level of Service (LOS)						B		B							A	
Approach Delay (s/veh)							10.8									2.1
Approach LOS							B									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Village Center
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	40	4	5	6
Number of Lanes		0	0	0		1	0	1	0	0	1	0	0	1	1	0
Configuration						L		R				TR		L	T	
Volume (veh/h)						19		43			131	19		34	64	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized							No									
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						21		48							38	
Capacity, c (veh/h)						670		890							1411	
v/c Ratio						0.03		0.05							0.03	
95% Queue Length, Q <sub>95</sub> (veh)						0.1		0.2							0.1	
Control Delay (s/veh)						10.5		9.3							7.6	
Level of Service (LOS)						B		A							A	
Approach Delay (s/veh)							9.7									2.6
Approach LOS							A									



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4	5	6		
Number of Lanes		1	0	1		0	0	0	0	1	1	0	0	0	1	0	
Configuration		L		R						L	T						TR
Volume (veh/h)		22		39						19	146				146	17	
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized		No															
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2									4.1				
Critical Headway (sec)		6.42		6.22									4.12				
Base Follow-Up Headway (sec)		3.5		3.3									2.2				
Follow-Up Headway (sec)		3.52		3.32									2.22				

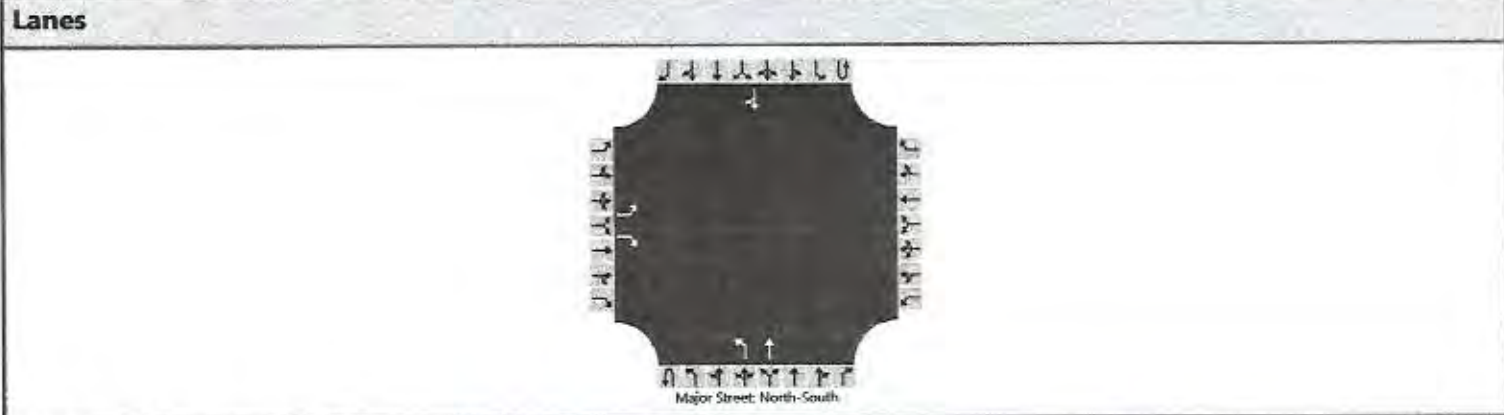
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		29		52									25				
Capacity, c (veh/h)		518		780									1304				
v/c Ratio		0.06		0.07									0.02				
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.2									0.1				
Control Delay (s/veh)		12.4		9.9									7.8				
Level of Service (LOS)		B		A									A				
Approach Delay (s/veh)		10.8											0.9				
Approach LOS		B															



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Rockland		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Rockland Drive		
Analysis Year	2020			North/South Street	Village Parkway		
Time Analyzed	PM Existing			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6
Number of Lanes		1	0	1		0	0	0	0	1	1	0	0	0	1	0
Configuration		L		R						L	T					TR
Volume (veh/h)		10		21						50	75				30	11
Percent Heavy Vehicles (%)		2		2						2						
Proportion Time Blocked																
Percent Grade (%)		0														
Right Turn Channelized		No														
Median Type   Storage		Undivided														

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1		6.2						4.1						
Critical Headway (sec)		6.42		6.22						4.12						
Base Follow-Up Headway (sec)		3.5		3.3						2.2						
Follow-Up Headway (sec)		3.52		3.32						2.22						

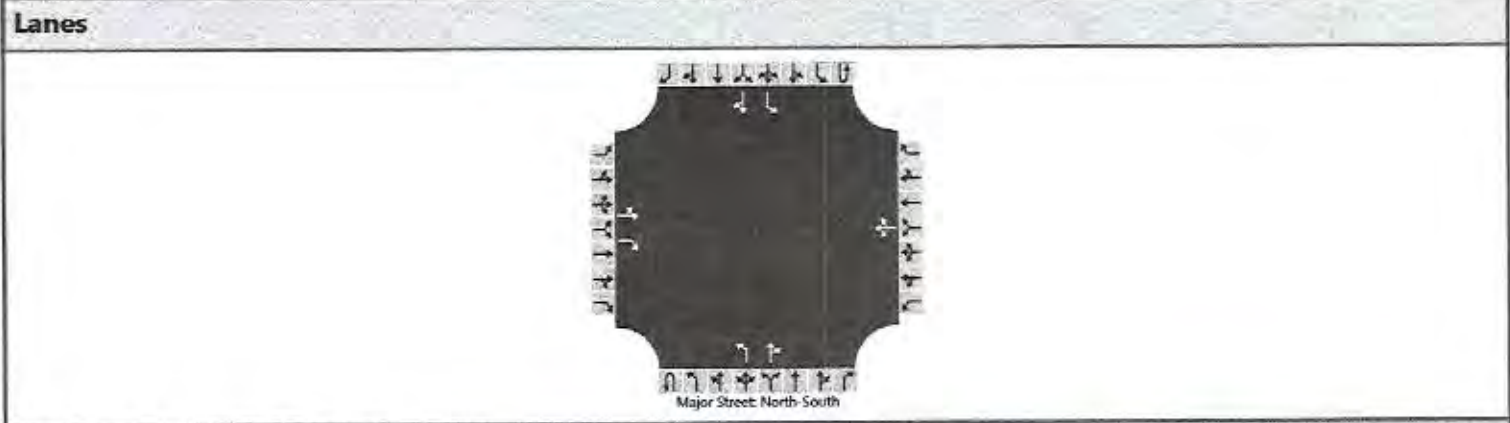
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		11		23						56							
Capacity, c (veh/h)		703		998						1535							
v/c Ratio		0.02		0.02						0.04							
95% Queue Length, $Q_{95}$ (veh)		0.0		0.1						0.1							
Control Delay (s/veh)		10.2		8.7						7.4							
Level of Service (LOS)		B		A						A							
Approach Delay (s/veh)		9.2									3.0						
Approach LOS		A									A						



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0
Configuration		LT		R			LTR			L		TR		L		TR
Volume (veh/h)		22	0	39		13	1	1		19	158	3		1	161	18
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized		No														
Median Type   Storage		Undivided														

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		29		52				20				25				1
Capacity, c (veh/h)		442		760				413				1281				1307
v/c Ratio		0.07		0.07				0.05				0.02				0.00
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.2				0.2				0.1				0.0
Control Delay (s/veh)		13.7		10.1				14.2				7.9				7.8
Level of Service (LOS)		B		B				B				A				A
Approach Delay (s/veh)		11.4				14.2				0.8				0.0		
Approach LOS		B				B										



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0	
Configuration		LT		R			LTR			L		TR		L		TR	
Volume (veh/h)		10	1	22		7	1	1		50	90	10		1	47	11	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized		No															
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		12		24			10			56				1			
Capacity, c (veh/h)		629		974			624			1510				1452			
v/c Ratio		0.02		0.03			0.02			0.04				0.00			
95% Queue Length, Q <sub>95</sub> (veh)		0.1		0.1			0.0			0.1				0.0			
Control Delay (s/veh)		10.8		8.8			10.9			7.5				7.5			
Level of Service (LOS)		B		A			B			A				A			
Approach Delay (s/veh)		9.5				10.9				2.5				0.1			
Approach LOS		A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound					
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R		
Movement																		
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6		
Number of Lanes		1	0	1		0	0	0	0	1	1	0	0	0	1	0		
Configuration		L		R						L	T						TR	
Volume (veh/h)		81		97						86	149					152	84	
Percent Heavy Vehicles (%)		2		2						2								
Proportion Time Blocked																		
Percent Grade (%)		0																
Right Turn Channelized		No																
Median Type   Storage		Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2						4.1							
Critical Headway (sec)		6.42		6.22						4.12							
Base Follow-Up Headway (sec)		3.5		3.3						2.2							
Follow-Up Headway (sec)		3.52		3.32						2.22							

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		108		129						115							
Capacity, c (veh/h)		348		729						1201							
v/c Ratio		0.31		0.18						0.10							
95% Queue Length, Q <sub>95</sub> (veh)		1.3		0.6						0.3							
Control Delay (s/veh)		19.9		11.0						8.3							
Level of Service (LOS)		C		B						A							
Approach Delay (s/veh)		15.1								3.0							
Approach LOS		C															



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Rockland		
Agency/Co.	Solægui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Rockland Drive		
Analysis Year	2030			North/South Street	Village Parkway		
Time Analyzed	PM Base			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		1	0	1		0	0	0	0	1	1	0	0	0	1	0	
Configuration		L		R						L	T						TR
Volume (veh/h)		28		39						67	82					34	28
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized		No															
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1						
Critical Headway (sec)		6.42		6.22							4.12						
Base Follow-Up Headway (sec)		3.5		3.3							2.2						
Follow-Up Headway (sec)		3.52		3.32							2.22						

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		31		43							74						
Capacity, c (veh/h)		648		992							1518						
v/c Ratio		0.05		0.04							0.05						
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.1							0.2						
Control Delay (s/veh)		10.8		8.8							7.5						
Level of Service (LOS)		B		A							A						
Approach Delay (s/veh)		9.6									3.4						
Approach LOS		A									A						



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0	
Configuration		LT		R			LTR			L		TR		L		TR	
Volume (veh/h)		81	0	97		13	1	1		86	161	3		1	167	85	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized		No															
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

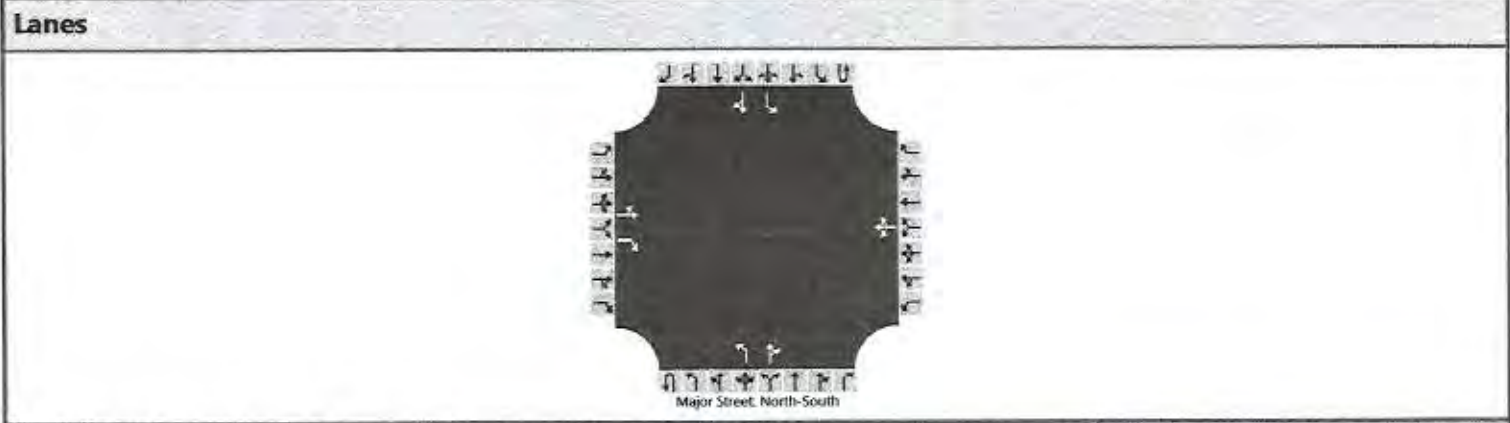
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		108		129			20			115				1			
Capacity, c (veh/h)		289		710			229			1180				1303			
v/c Ratio		0.37		0.18			0.09			0.10				0.00			
95% Queue Length, Q <sub>95</sub> (veh)		1.7		0.7			0.3			0.3				0.0			
Control Delay (s/veh)		24.8		11.2			22.2			8.4				7.8			
Level of Service (LOS)		C		B			C			A				A			
Approach Delay (s/veh)		17.4				22.2				2.9				0.0			
Approach LOS		C				C											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & Rockland
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Rockland Drive
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0	
Configuration		LT		R			LTR			L		TR		L		TR	
Volume (veh/h)		28	1	40		7	1	1		67	97	10		1	51	28	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized		No															
Median Type   Storage		Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

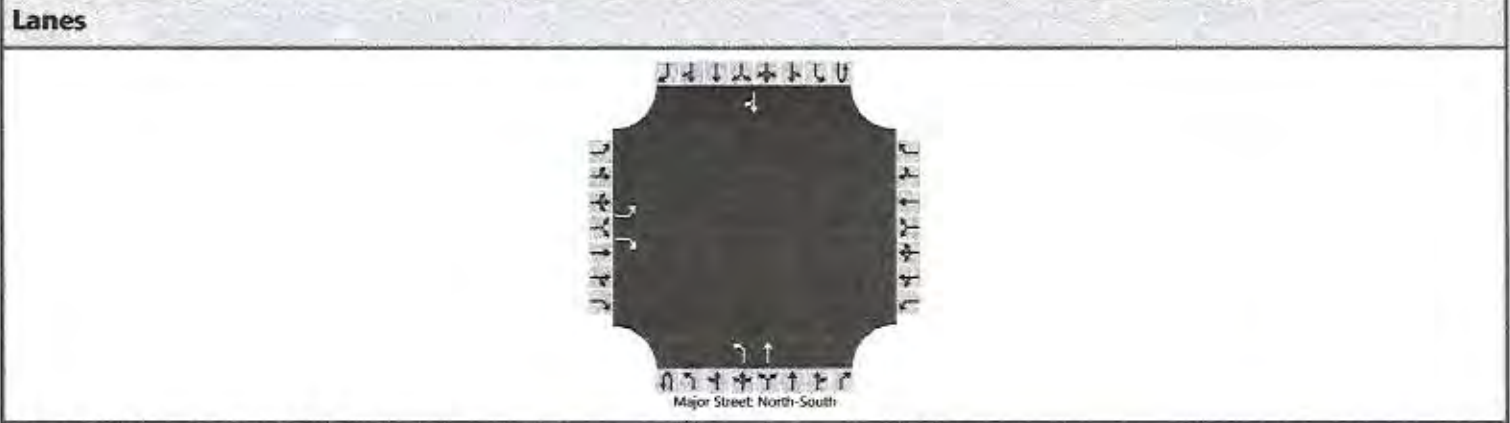
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		32		44			10			74				1			
Capacity, c (veh/h)		569		957			551			1481				1443			
v/c Ratio		0.06		0.05			0.02			0.05				0.00			
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.1			0.1			0.2				0.0			
Control Delay (s/veh)		11.7		8.9			11.7			7.6				7.5			
Level of Service (LOS)		B		A			B			A				A			
Approach Delay (s/veh)		10.1				11.7				2.9				0.1			
Approach LOS		B				B											



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Rockland		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Rockland Drive		
Analysis Year	2040			North/South Street	Village Parkway		
Time Analyzed	AM Base			Peak Hour Factor	0.75		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		1	0	1		0	0	0		1	1	0		0	1	0
Configuration		L		R						L	T					TR
Volume (veh/h)		81		97						86	149				152	84
Percent Heavy Vehicles (%)		2		2						2						
Proportion Time Blocked																
Percent Grade (%)		0														
Right Turn Channelized		No														
Median Type   Storage		Undivided														

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1		6.2							4.1					
Critical Headway (sec)		6.42		6.22							4.12					
Base Follow-Up Headway (sec)		3.5		3.3							2.2					
Follow-Up Headway (sec)		3.52		3.32							2.22					

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		108		129							115					
Capacity, c (veh/h)		348		729							1201					
v/c Ratio		0.31		0.18							0.10					
95% Queue Length, Q <sub>95</sub> (veh)		1.3		0.6							0.3					
Control Delay (s/veh)		19.9		11.0							8.3					
Level of Service (LOS)		C		B							A					
Approach Delay (s/veh)		15.1										3.0				
Approach LOS		C														



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	PM Base
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Village & Rockland
Jurisdiction	Washoe County
East/West Street	Rockland Drive
North/South Street	Village Parkway
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		1	0	1		0	0	0		1	1	0		0	1	0	
Configuration		L		R						L	T					TR	
Volume (veh/h)		28		39						67	82				34	28	
Percent Heavy Vehicles (%)		2		2						2							
Proportion Time Blocked																	
Percent Grade (%)		0															
Right Turn Channelized		No															
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1		6.2							4.1					
Critical Headway (sec)		6.42		6.22							4.12					
Base Follow-Up Headway (sec)		3.5		3.3							2.2					
Follow-Up Headway (sec)		3.52		3.32							2.22					

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		31		43							74							
Capacity, c (veh/h)		648		992							1518							
v/c Ratio		0.05		0.04							0.05							
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.1							0.2							
Control Delay (s/veh)		10.8		8.8							7.5							
Level of Service (LOS)		B		A							A							
Approach Delay (s/veh)		9.6									3.4							
Approach LOS		A									A							



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Rockland		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Rockland Drive		
Analysis Year	2040			North/South Street	Village Parkway		
Time Analyzed	AM Base + Project			Peak Hour Factor	0.75		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0
Configuration		LT		R			LTR			L		TR		L		TR
Volume (veh/h)		81	0	97		13	1	1		86	161	3		1	167	85
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized		No														
Median Type   Storage		Undivided														

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		108		129			20			115					1	
Capacity, c (veh/h)		289		710			229			1180					1303	
v/c Ratio		0.37		0.18			0.09			0.10					0.00	
95% Queue Length, Q <sub>95</sub> (veh)		1.7		0.7			0.3			0.3					0.0	
Control Delay (s/veh)		24.8		11.2			22.2			8.4					7.8	
Level of Service (LOS)		C		B			C			A					A	
Approach Delay (s/veh)		17.4				22.2				2.9				0.0		
Approach LOS		C				C										



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & Rockland		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Rockland Drive		
Analysis Year	2040			North/South Street	Village Parkway		
Time Analyzed	PM Base + Project			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	1		0	1	0	0	1	1	0	0	1	1	0
Configuration		LT		R			LTR			L		TR		L		TR
Volume (veh/h)		28	1	40		7	1	1		67	97	10		1	51	28
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized		No														
Median Type   Storage		Undivided														

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

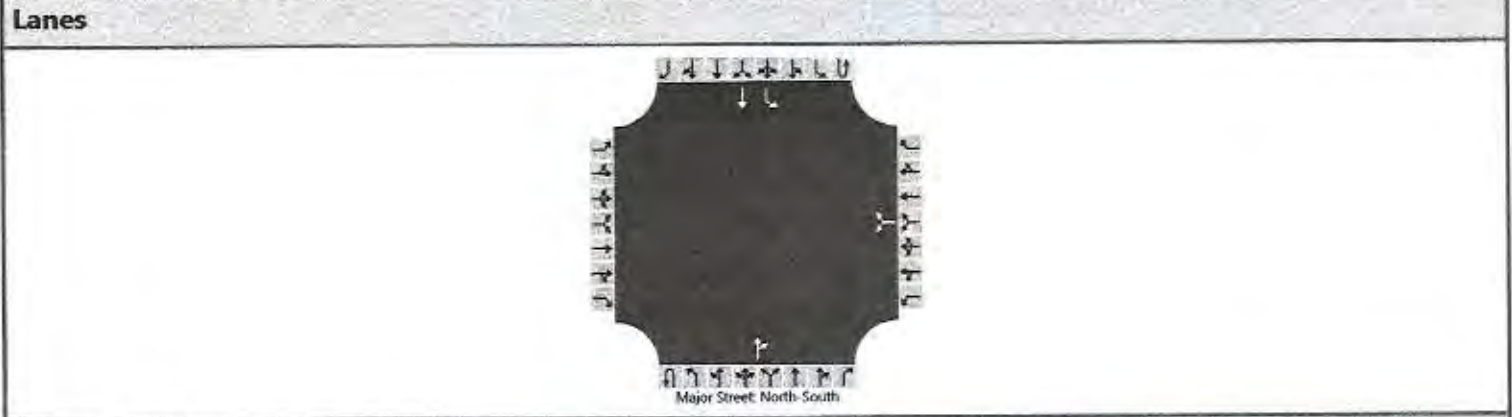
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		32		44			10			74					1	
Capacity, c (veh/h)		569		957			551			1481					1443	
v/c Ratio		0.06		0.05			0.02			0.05					0.00	
95% Queue Length, Q <sub>95</sub> (veh)		0.2		0.1			0.1			0.2					0.0	
Control Delay (s/veh)		11.7		8.9			11.7			7.6					7.5	
Level of Service (LOS)		B		A			B			A					A	
Approach Delay (s/veh)		10.1				11.7				2.9				0.1		
Approach LOS		B				B										



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0
Configuration							LR					TR		L	T	
Volume (veh/h)						34		2			130	38		3	129	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)	0															
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						40									4	
Capacity, c (veh/h)						631									1345	
v/c Ratio						0.08									0.00	
95% Queue Length, Q <sub>95</sub> (veh)						0.2									0.0	
Control Delay (s/veh)						11.2									7.7	
Level of Service (LOS)						B									A	
Approach Delay (s/veh)	11.2								0.2							
Approach LOS	B															



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Village & North Driveway		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	North Driveway		
Analysis Year	2020			North/South Street	Village Parkway		
Time Analyzed	PM Existing			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4	5	6		
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						15		2			67	18		4	26		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1		
Critical Headway (sec)						6.42		6.22							4.12		
Base Follow-Up Headway (sec)						3.5		3.3							2.2		
Follow-Up Headway (sec)						3.52		3.32							2.22		

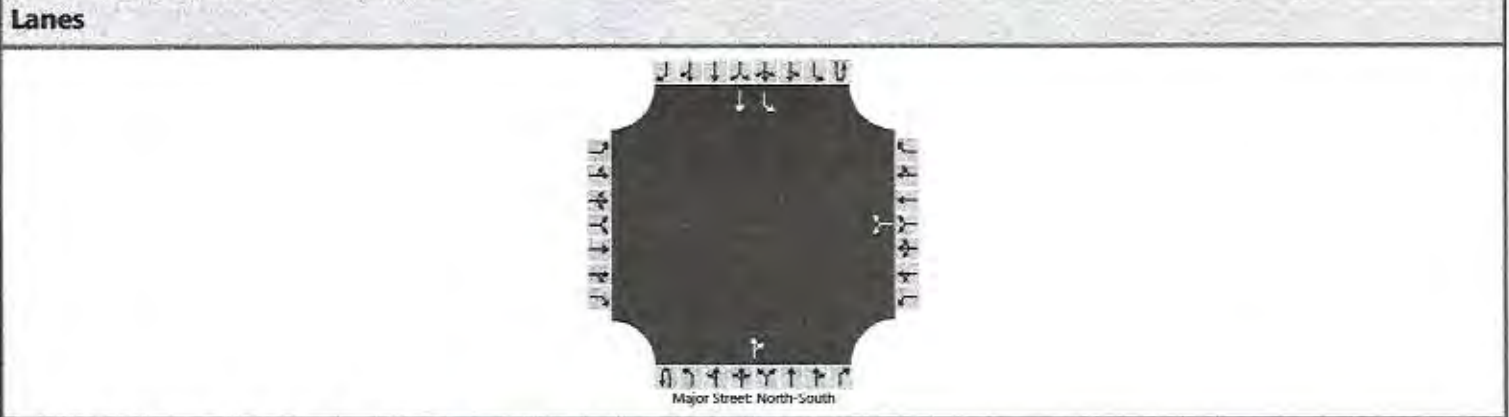
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						19									4		
Capacity, c (veh/h)						882									1500		
v/c Ratio						0.02									0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.1									0.0		
Control Delay (s/veh)						9.2									7.4		
Level of Service (LOS)						A									A		
Approach Delay (s/veh)						9.2								1.0			
Approach LOS						A											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2020	North/South Street	Village Parkway
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0		0	1	0		0	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						47		3			139	42		3	133		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage					Undivided												

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2						4.1		
Critical Headway (sec)						6.42		6.22						4.12		
Base Follow-Up Headway (sec)						3.5		3.3						2.2		
Follow-Up Headway (sec)						3.52		3.32						2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						67								4		
Capacity, c (veh/h)						615								1325		
v/c Ratio						0.11								0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.4								0.0		
Control Delay (s/veh)						11.6								7.7		
Level of Service (LOS)						B								A		
Approach Delay (s/veh)						11.6									0.2	
Approach LOS						B										



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2020
Time Analyzed	PM Existing + Project
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Village & North Driveway
Jurisdiction	Washoe County
East/West Street	North Driveway
North/South Street	Village Parkway
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						22		3			73	28		5	36		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)					7.1	6.2							4.1			
Critical Headway (sec)					6.42	6.22							4.12			
Base Follow-Up Headway (sec)					3.5	3.3							2.2			
Follow-Up Headway (sec)					3.52	3.32							2.22			

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)					28								6			
Capacity, c (veh/h)					854								1477			
v/c Ratio					0.03								0.00			
95% Queue Length, Q <sub>95</sub> (veh)					0.1								0.0			
Control Delay (s/veh)					9.4								7.4			
Level of Service (LOS)					A								A			
Approach Delay (s/veh)					9.4								0.9			
Approach LOS					A											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0		0	1	0		0	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						34		2			192	38		3	202		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

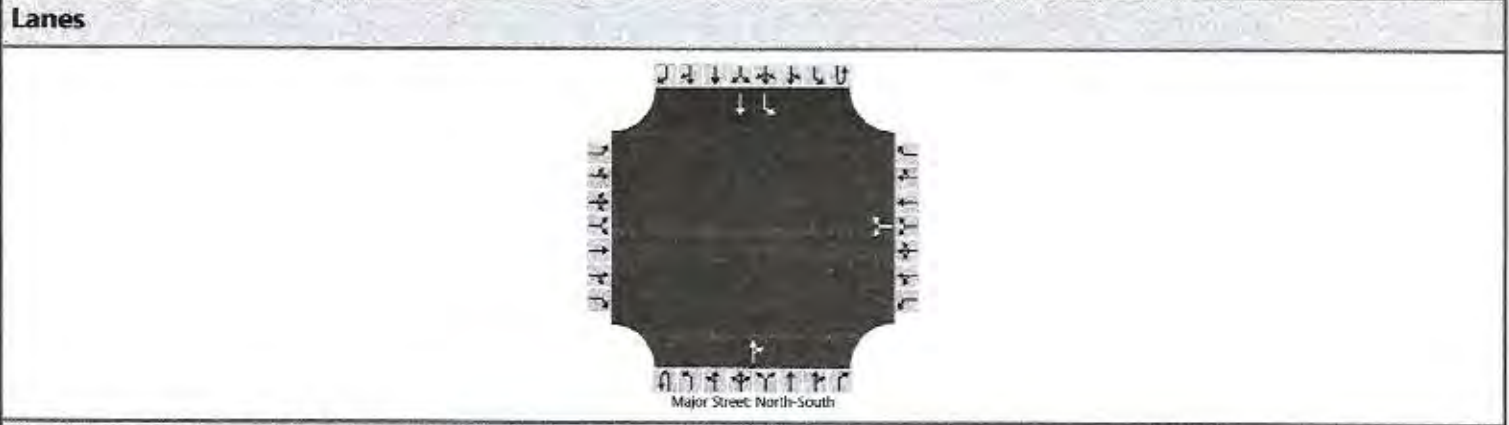
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						48									4	
Capacity, c (veh/h)						499									1254	
v/c Ratio						0.10									0.00	
95% Queue Length, Q <sub>95</sub> (veh)						0.3									0.0	
Control Delay (s/veh)						13.0									7.9	
Level of Service (LOS)						B									A	
Approach Delay (s/veh)						13.0									0.1	
Approach LOS						B										



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4	5	6		
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						15		2			92	18		4	47		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage						Undivided											

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1		
Critical Headway (sec)						6.42		6.22							4.12		
Base Follow-Up Headway (sec)						3.5		3.3							2.2		
Follow-Up Headway (sec)						3.52		3.32							2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						19									4		
Capacity, c (veh/h)						827									1465		
v/c Ratio						0.02									0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.1									0.0		
Control Delay (s/veh)						9.5									7.5		
Level of Service (LOS)						A									A		
Approach Delay (s/veh)						9.5								0.6			
Approach LOS						A											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						47		3			201	42		3	206		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage						Undivided											

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1		
Critical Headway (sec)						6.42		6.22							4.12		
Base Follow-Up Headway (sec)						3.5		3.3							2.2		
Follow-Up Headway (sec)						3.52		3.32							2.22		

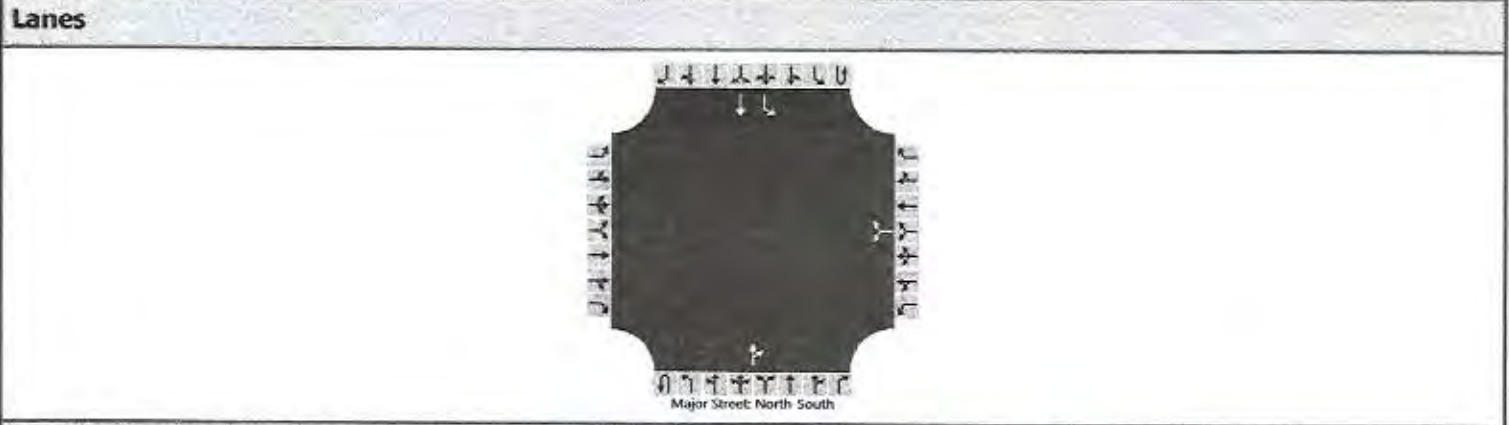
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						67									4		
Capacity, c (veh/h)						486									1236		
v/c Ratio						0.14									0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.5									0.0		
Control Delay (s/veh)						13.6									7.9		
Level of Service (LOS)						B									A		
Approach Delay (s/veh)						13.6								0.1			
Approach LOS						B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2030	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0
Configuration							LR					TR		L	T	
Volume (veh/h)						22		3			98	28		5	57	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)						0										
Right Turn Channelized																
Median Type   Storage					Undivided											

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2							4.1	
Critical Headway (sec)						6.42		6.22							4.12	
Base Follow-Up Headway (sec)						3.5		3.3							2.2	
Follow-Up Headway (sec)						3.52		3.32							2.22	

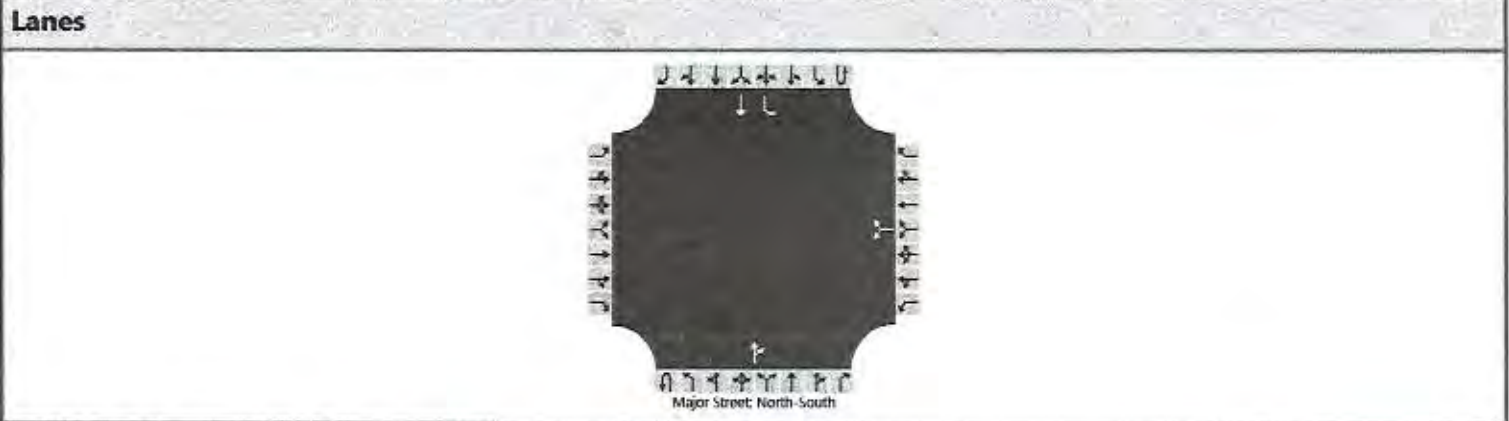
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						28									6	
Capacity, c (veh/h)						801									1443	
v/c Ratio						0.03									0.00	
95% Queue Length, Q <sub>95</sub> (veh)						0.1									0.0	
Control Delay (s/veh)						9.7									7.5	
Level of Service (LOS)						A									A	
Approach Delay (s/veh)						9.7						0.6				
Approach LOS						A										



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0
Configuration							LR					TR		L	T	
Volume (veh/h)						34		2			192	38		3	202	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)							0									
Right Turn Channelized																
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2						4.1		
Critical Headway (sec)						6.42		6.22						4.12		
Base Follow-Up Headway (sec)						3.5		3.3						2.2		
Follow-Up Headway (sec)						3.52		3.32						2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						48								4		
Capacity, c (veh/h)						499								1254		
v/c Ratio						0.10								0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.3								0.0		
Control Delay (s/veh)						13.0								7.9		
Level of Service (LOS)						B								A		
Approach Delay (s/veh)						13.0								0.1		
Approach LOS						B										



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0
Configuration							LR					TR		L	T	
Volume (veh/h)						15		2			92	18		4	47	
Percent Heavy Vehicles (%)						2		2						2		
Proportion Time Blocked																
Percent Grade (%)	0															
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)					7.1		6.2								4.1		
Critical Headway (sec)					6.42		6.22								4.12		
Base Follow-Up Headway (sec)					3.5		3.3								2.2		
Follow-Up Headway (sec)					3.52		3.32								2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)					19										4			
Capacity, c (veh/h)					827										1465			
v/c Ratio					0.02										0.00			
95% Queue Length, Q <sub>95</sub> (veh)					0.1										0.0			
Control Delay (s/veh)					9.5										7.5			
Level of Service (LOS)					A										A			
Approach Delay (s/veh)					9.5									0.6				
Approach LOS					A													



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.75
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						47		3			201	42		3	206		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage					Undivided												

## Critical and Follow-up Headways

Base Critical Headway (sec)						7.1		6.2							4.1		
Critical Headway (sec)						6.42		6.22							4.12		
Base Follow-Up Headway (sec)						3.5		3.3							2.2		
Follow-Up Headway (sec)						3.52		3.32							2.22		

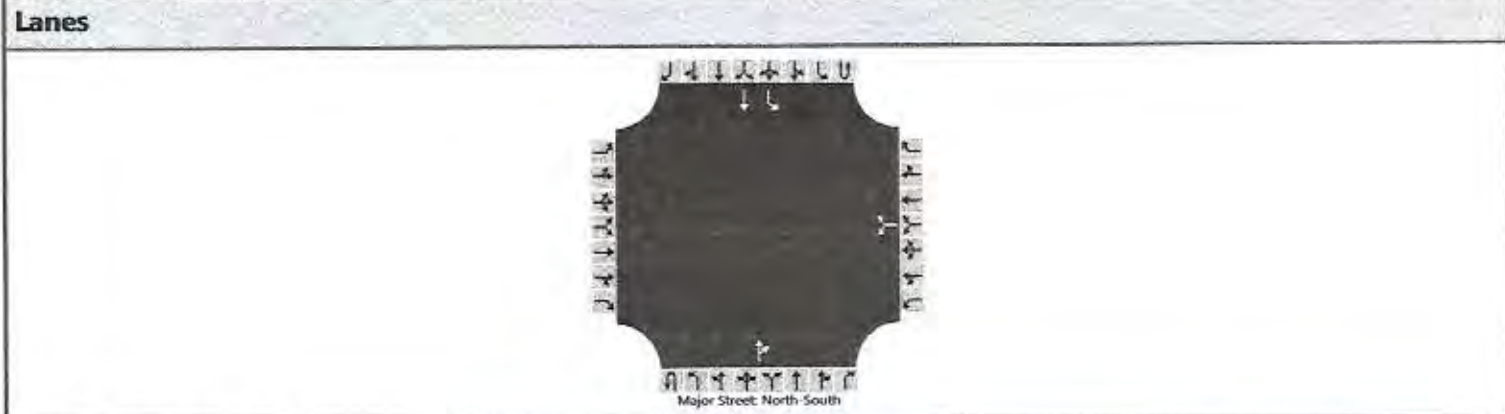
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)						67									4		
Capacity, c (veh/h)						486									1236		
v/c Ratio						0.14									0.00		
95% Queue Length, Q <sub>95</sub> (veh)						0.5									0.0		
Control Delay (s/veh)						13.6									7.9		
Level of Service (LOS)						B									A		
Approach Delay (s/veh)						13.6									0.1		
Approach LOS						B									A		



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village & North Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	North Driveway
Analysis Year	2040	North/South Street	Village Parkway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	0	0		0	1	0	0	0	1	0	0	1	1	0	
Configuration							LR					TR		L	T		
Volume (veh/h)						22		3			98	28		5	57		
Percent Heavy Vehicles (%)						2		2						2			
Proportion Time Blocked																	
Percent Grade (%)						0											
Right Turn Channelized																	
Median Type   Storage						Undivided											

**Critical and Follow-up Headways**

Base Critical Headway (sec)						7.1		6.2								4.1	
Critical Headway (sec)						6.42		6.22								4.12	
Base Follow-Up Headway (sec)						3.5		3.3								2.2	
Follow-Up Headway (sec)						3.52		3.32								2.22	

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)						28										6	
Capacity, c (veh/h)						801										1443	
v/c Ratio						0.03										0.00	
95% Queue Length, Q <sub>95</sub> (veh)						0.1										0.0	
Control Delay (s/veh)						9.7										7.5	
Level of Service (LOS)						A										A	
Approach Delay (s/veh)						9.7									0.6		
Approach LOS						A											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2020	North/South Street	Project Driveway
Time Analyzed	AM Existing	Peak Hour Factor	0.80
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR								LR
Volume (veh/h)		2	21				28	3						2		1
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

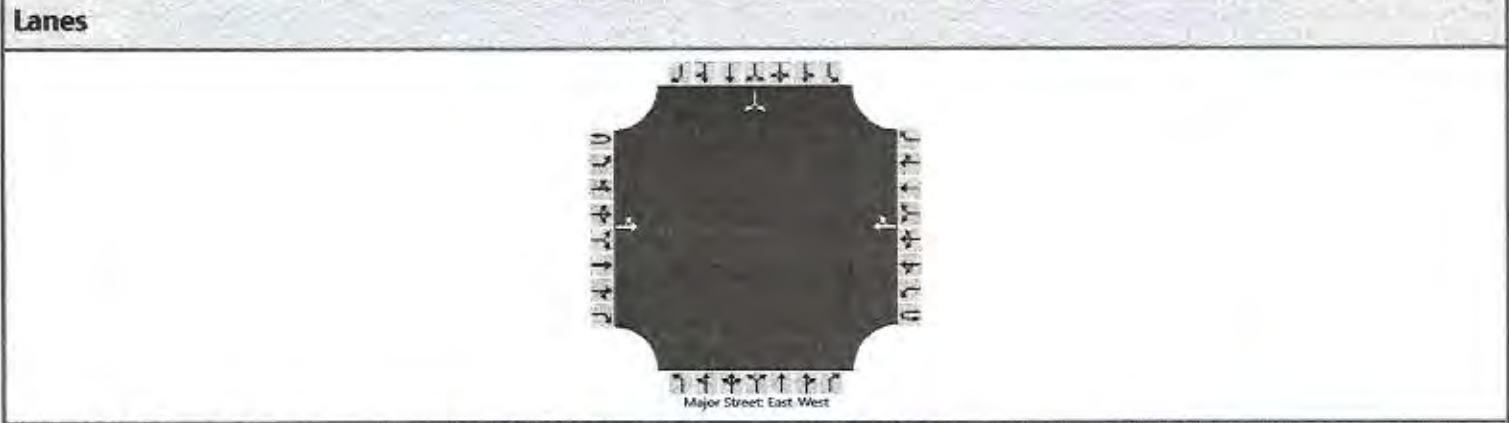
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		3														4	
Capacity, c (veh/h)		1571														966	
v/c Ratio		0.00														0.00	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.3														8.7	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.6												8.7			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2020	North/South Street	Project Driveway
Time Analyzed	PM Existing	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT					TR								LR	
Volume (veh/h)		5	19				28	6						3		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		6														6
Capacity, c (veh/h)		1573														974
v/c Ratio		0.00														0.01
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0
Control Delay (s/veh)		7.3														8.7
Level of Service (LOS)		A														A
Approach Delay (s/veh)		1.5												8.7		
Approach LOS														A		



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2020
Time Analyzed	AM Existing + Project
Intersection Orientation	East-West
Project Description	

## Site Information

Intersection	Village Center & Driveway
Jurisdiction	Washoe County
East/West Street	Village Center Drive
North/South Street	Project Driveway
Peak Hour Factor	0.80
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR								LR
Volume (veh/h)		2	29				30	6						11		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

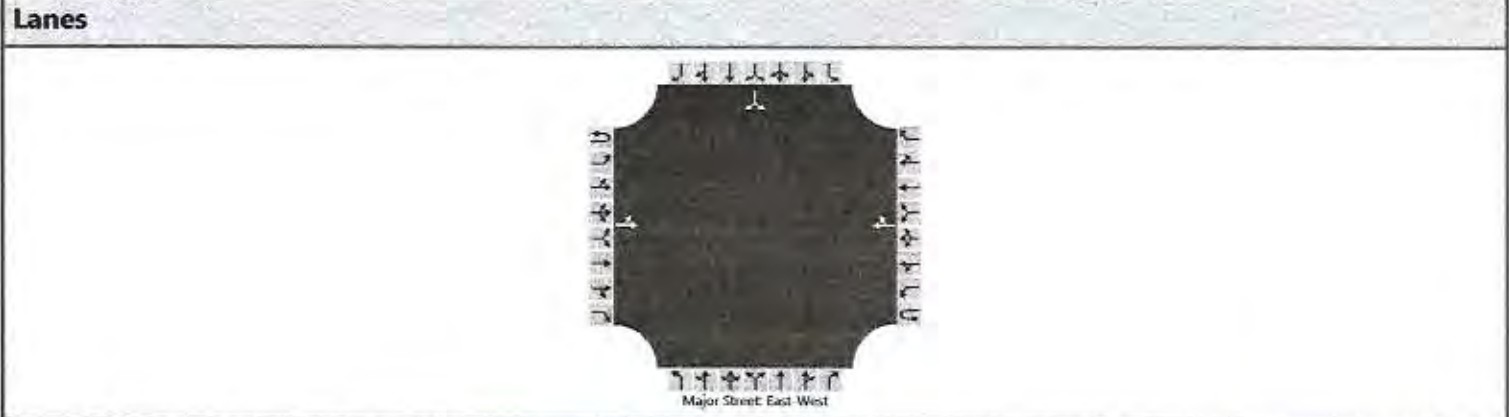
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		3														16	
Capacity, c (veh/h)		1563														933	
v/c Ratio		0.00														0.02	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.1	
Control Delay (s/veh)		7.3														8.9	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.5												8.9			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2020	North/South Street	Project Driveway
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		6	23				35	14						8		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage							Undivided									

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

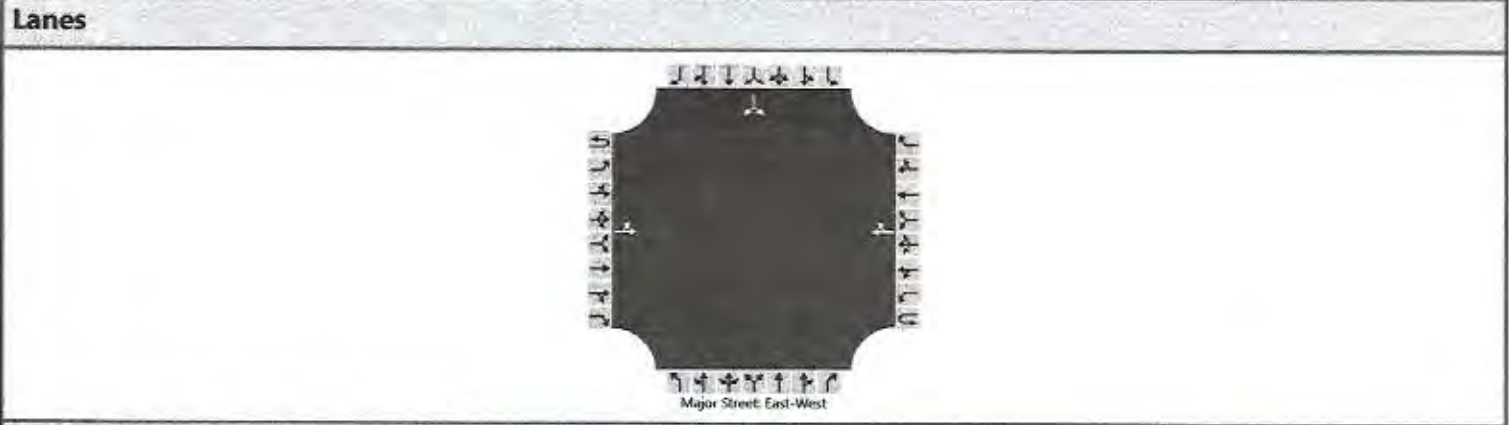
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		7														11	
Capacity, c (veh/h)		1551														932	
v/c Ratio		0.00														0.01	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.3														8.9	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		1.5												8.9			
Approach LOS		A												A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Project Driveway
Time Analyzed	AM Base	Peak Hour Factor	0.80
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		2	66				76	3						2		1
Percent Heavy Vehicles (%)		2	-											2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage		Undivided														

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		3														4	
Capacity, c (veh/h)		1494														850	
v/c Ratio		0.00														0.00	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.4														9.3	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.2												9.3			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Project Driveway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		5	35				45	6						3		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

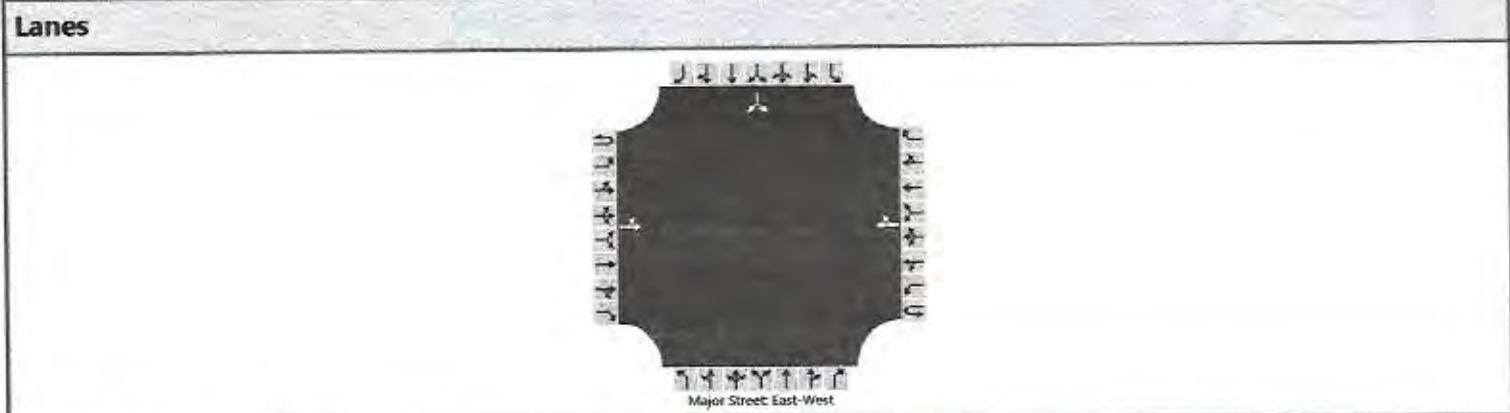
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		6														6	
Capacity, c (veh/h)		1548														937	
v/c Ratio		0.00														0.01	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.3														8.9	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.9												8.9			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Project Driveway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.80
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		2	74				78	6						11		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

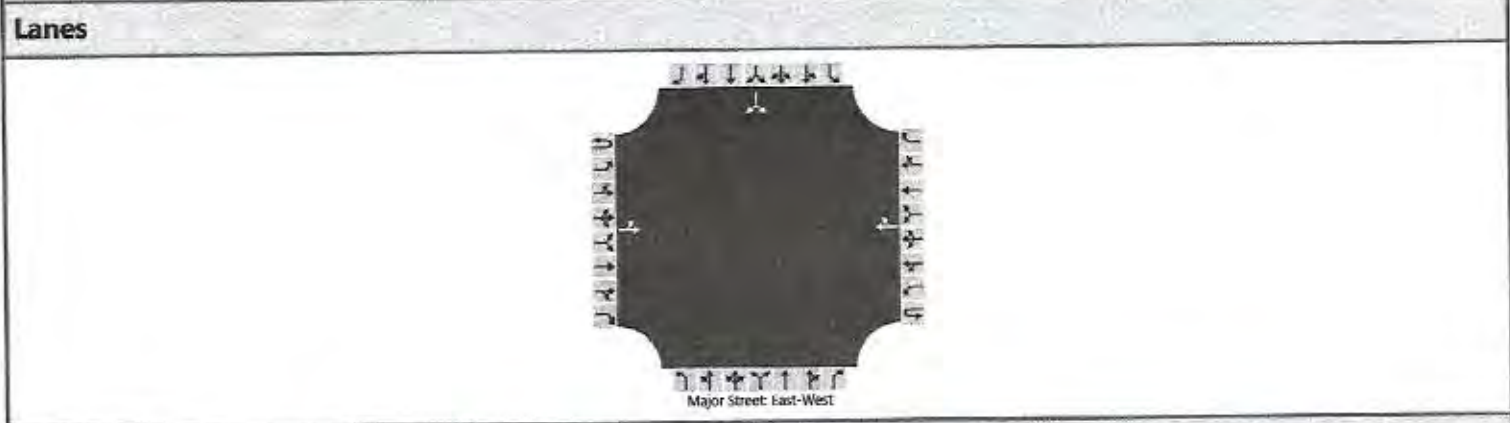
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		3														16	
Capacity, c (veh/h)		1486														810	
v/c Ratio		0.00														0.02	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.1	
Control Delay (s/veh)		7.4														9.5	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.2												9.5			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2030	North/South Street	Project Driveway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		6	39				52	14						8		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

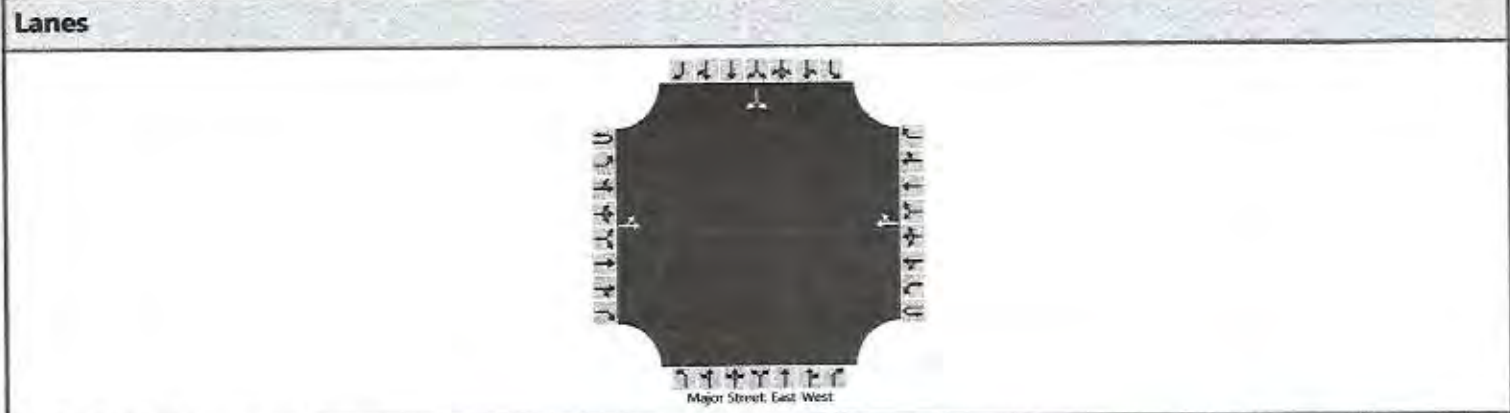
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		7														11	
Capacity, c (veh/h)		1526														892	
v/c Ratio		0.00														0.01	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.4														9.1	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		1.0												9.1			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Project Driveway
Time Analyzed	AM Base	Peak Hour Factor	0.80
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		2	66				76	3						2		1
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

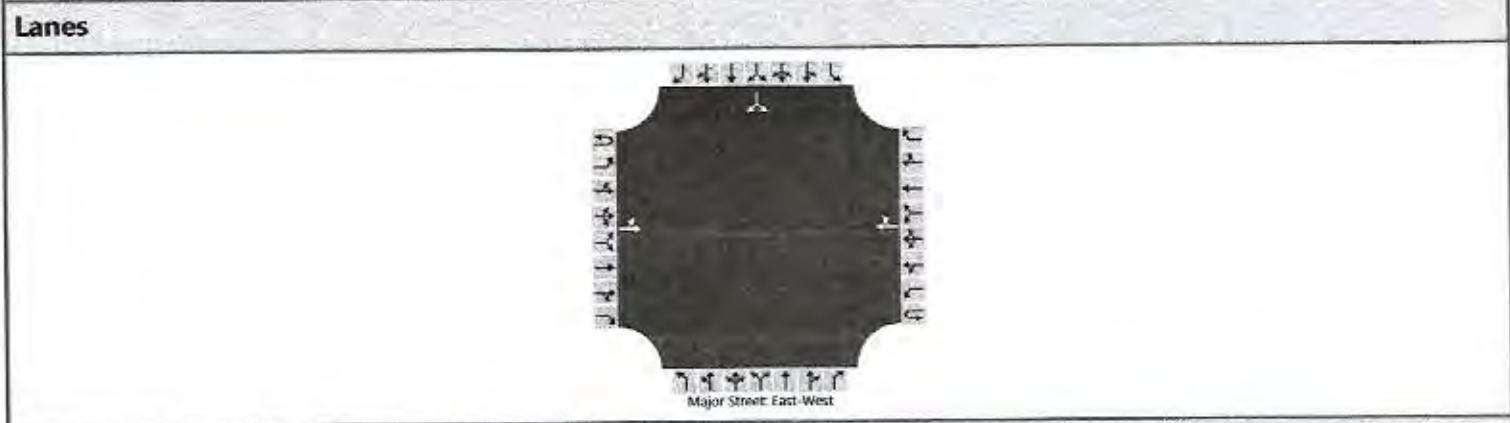
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		3														4	
Capacity, c (veh/h)		1494														850	
v/c Ratio		0.00														0.00	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.4														9.3	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.2												9.3			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Project Driveway
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		5	35				45	6						3		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

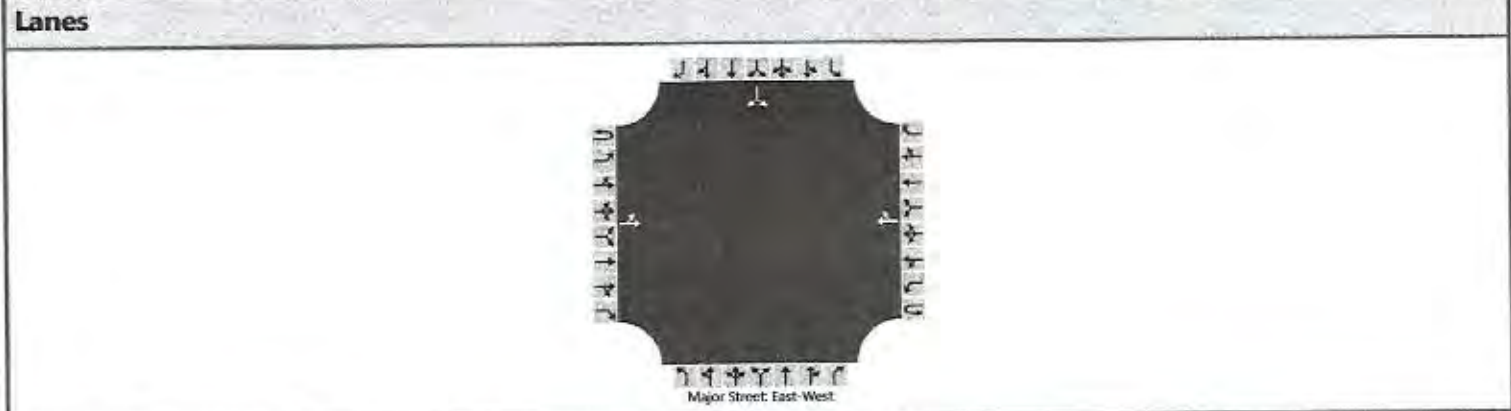
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		6														6	
Capacity, c (veh/h)		1548														937	
v/c Ratio		0.00														0.01	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0	
Control Delay (s/veh)		7.3														8.9	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.9												8.9			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Project Driveway
Time Analyzed	AM Base + Project	Peak Hour Factor	0.80
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		2	74				78	6						11		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)																0
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

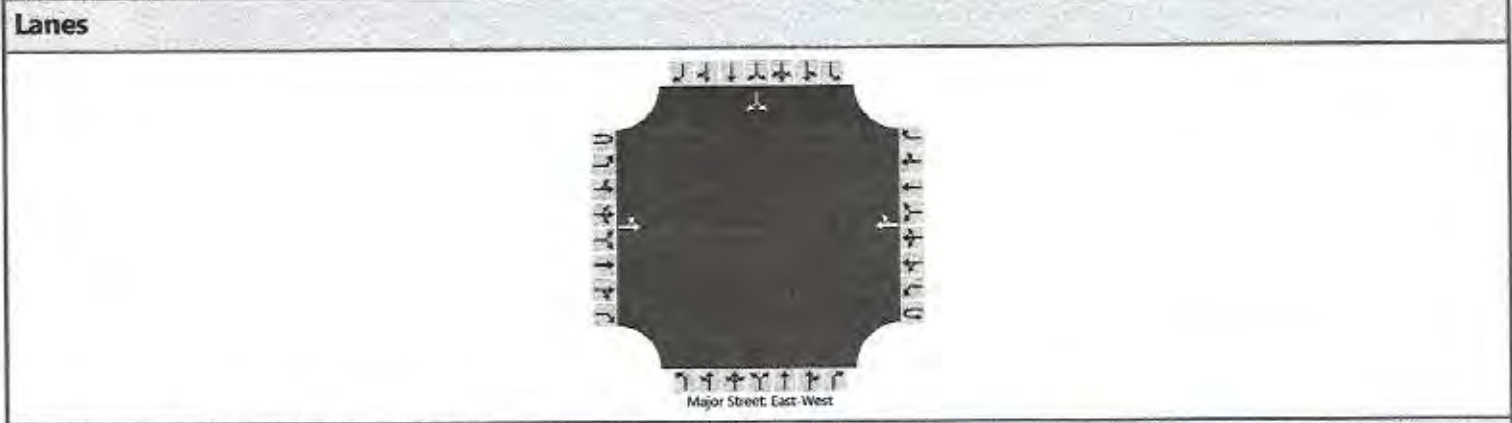
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		3														16	
Capacity, c (veh/h)		1486														810	
v/c Ratio		0.00														0.02	
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.1	
Control Delay (s/veh)		7.4														9.5	
Level of Service (LOS)		A														A	
Approach Delay (s/veh)		0.2												9.5			
Approach LOS														A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Village Center & Driveway
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Village Center Drive
Analysis Year	2040	North/South Street	Project Driveway
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Priority																
Number of Lanes	0	0	1	0	0	0	1	0		0	0	0		0	1	0
Configuration		LT						TR							LR	
Volume (veh/h)		6	39				52	14						8		2
Percent Heavy Vehicles (%)		2												2		2
Proportion Time Blocked																
Percent Grade (%)														0		
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		4.1												7.1		6.2
Critical Headway (sec)		4.12												6.42		6.22
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.22												3.52		3.32

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)		7														11
Capacity, c (veh/h)		1526														892
v/c Ratio		0.00														0.01
95% Queue Length, Q <sub>95</sub> (veh)		0.0														0.0
Control Delay (s/veh)		7.4														9.1
Level of Service (LOS)		A														A
Approach Delay (s/veh)		1.0												9.1		
Approach LOS														A		



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2020	North/South Street	Crystal Canyon Boulevard
Time Analyzed	AM Existing	Peak Hour Factor	0.85
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		2	4	95		9	2	2		48	27	1		2	66	0
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			119				15				56				2	
Capacity, c (veh/h)			956				624				1521				1579	
v/c Ratio			0.12				0.02				0.04				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.4				0.1				0.1				0.0	
Control Delay (s/veh)			9.3				10.9				7.5				7.3	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)	9.3				10.9				4.8				0.2			
Approach LOS	A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2020	North/South Street	Crystal Canyon Boulevard
Time Analyzed	PM Existing	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		3	3	40		7	2	1		112	80	13		2	31	1
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			51				11			124				2		
Capacity, c (veh/h)			916				520			1575				1488		
v/c Ratio			0.06				0.02			0.08				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1			0.3				0.0		
Control Delay (s/veh)			9.2				12.1			7.5				7.4		
Level of Service (LOS)			A				B			A				A		
Approach Delay (s/veh)	9.2				12.1				4.4				0.4			
Approach LOS	A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2020	North/South Street	Crystal Canyon Boulevard
Time Analyzed	AM Existing + Project	Peak Hour Factor	0.85
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		2	4	112		9	2	2		53	27	1		2	66	0
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

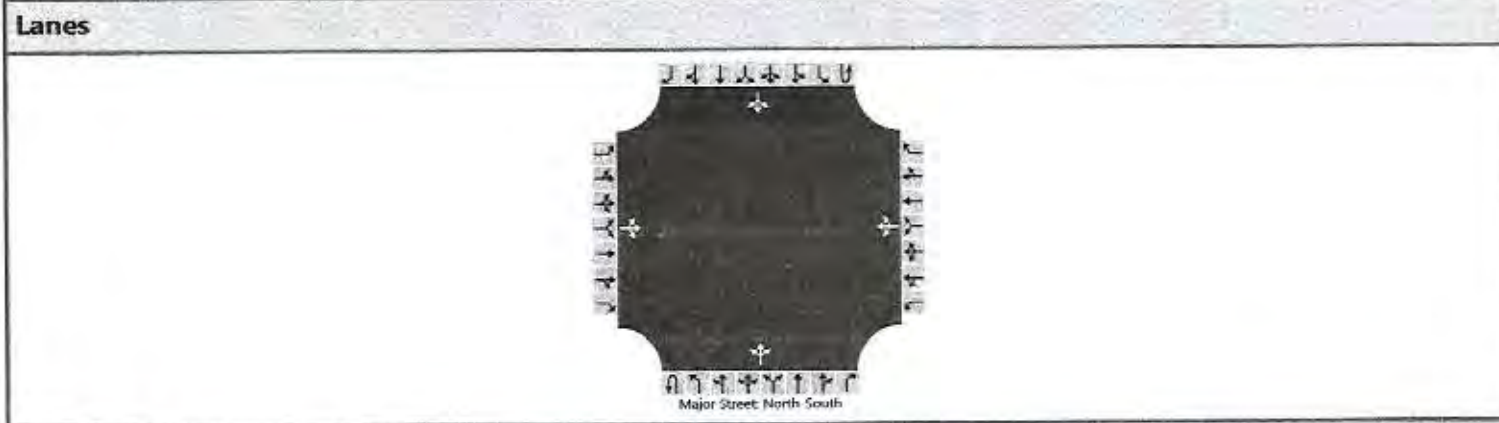
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			139				15				62				2	
Capacity, c (veh/h)			958				595				1521				1579	
v/c Ratio			0.14				0.03				0.04				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.5				0.1				0.1				0.0	
Control Delay (s/veh)			9.4				11.2				7.5				7.3	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)	9.4				11.2				5.0				0.2			
Approach LOS	A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2020	North/South Street	Crystal Canyon Boulevard
Time Analyzed	PM Existing + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		3	3	49		7	2	1		127	80	13		2	31	1
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

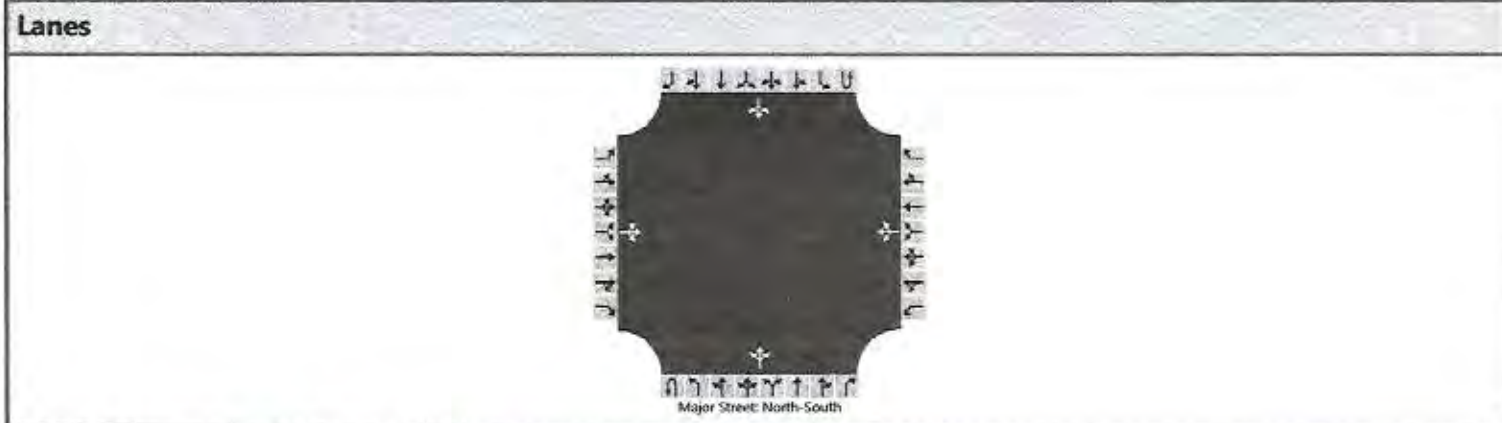
**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			61				11				141				2	
Capacity, c (veh/h)			923				485				1575				1488	
v/c Ratio			0.07				0.02				0.09				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1				0.3				0.0	
Control Delay (s/veh)			9.2				12.6				7.5				7.4	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)	9.2				12.6				4.6				0.4			
Approach LOS	A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2030	North/South Street	Crystal Canyon Boulevard
Time Analyzed	AM Base	Peak Hour Factor	0.85
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6	
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0	
Configuration			LTR				LTR				LTR				LTR		
Volume (veh/h)		2	6	113		9	5	2		65	40	1		2	112	0	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			142				19				76				2		
Capacity, c (veh/h)			880				515				1453				1559		
v/c Ratio			0.16				0.04				0.05				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.6				0.1				0.2				0.0		
Control Delay (s/veh)			9.9				12.2				7.6				7.3		
Level of Service (LOS)			A				B				A				A		
Approach Delay (s/veh)		9.9				12.2				4.8				0.1			
Approach LOS		A				B											



# HCS7 Two-Way Stop-Control Report

General Information				Site Information			
Analyst	MSH			Intersection	Crystal Canyon/Aquamarine		
Agency/Co.	Solaegui Engineers			Jurisdiction	Washoe County		
Date Performed	10/19/2020			East/West Street	Aquamarine Drive		
Analysis Year	2030			North/South Street	Crystal Canyon Boulevard		
Time Analyzed	PM Base			Peak Hour Factor	0.90		
Intersection Orientation	North-South			Analysis Time Period (hrs)	0.25		
Project Description							

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		3	4	48		7	3	1		123	132	13		2	61	1
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			61				12				137				2	
Capacity, c (veh/h)			852				428				1532				1418	
v/c Ratio			0.07				0.03				0.09				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1				0.3				0.0	
Control Delay (s/veh)			9.6				13.7				7.6				7.5	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)	9.6				13.7				3.9				0.2			
Approach LOS	A				B				A				A			



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2030	North/South Street	Crystal Canyon Boulevard
Time Analyzed	AM Base + Project	Peak Hour Factor	0.85
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		2	6	130		9	5	2		70	40	1		2	112	0
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)	0				0											
Right Turn Channelized																
Median Type   Storage	Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			162				19				82				2	
Capacity, c (veh/h)			883				492				1453				1559	
v/c Ratio			0.18				0.04				0.06				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.7				0.1				0.2				0.0	
Control Delay (s/veh)			10.0				12.6				7.6				7.3	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)	10.0				12.6				5.0				0.1			
Approach LOS	A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2030	North/South Street	Crystal Canyon Boulevard
Time Analyzed	PM Base + Project	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	1	0		0	1	0		0	1	0	
Configuration			LTR				LTR				LTR				LTR		
Volume (veh/h)		3	4	57		7	3	1		138	132	13		2	61	1	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage	Undivided																

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			71				12				153				2		
Capacity, c (veh/h)			858				399				1532				1418		
v/c Ratio			0.08				0.03				0.10				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.3				0.1				0.3				0.0		
Control Delay (s/veh)			9.6				14.3				7.6				7.5		
Level of Service (LOS)			A				B				A				A		
Approach Delay (s/veh)		9.6				14.3				4.1				0.2			
Approach LOS		A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2040	North/South Street	Crystal Canyon Boulevard
Time Analyzed	AM Base	Peak Hour Factor	0.85
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	10	1	2	3	4	5	6		
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0	
Configuration			LTR				LTR				LTR				LTR		
Volume (veh/h)		2	6	113		9	5	2		65	40	1		2	112	0	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1			
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12			
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2			
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22			

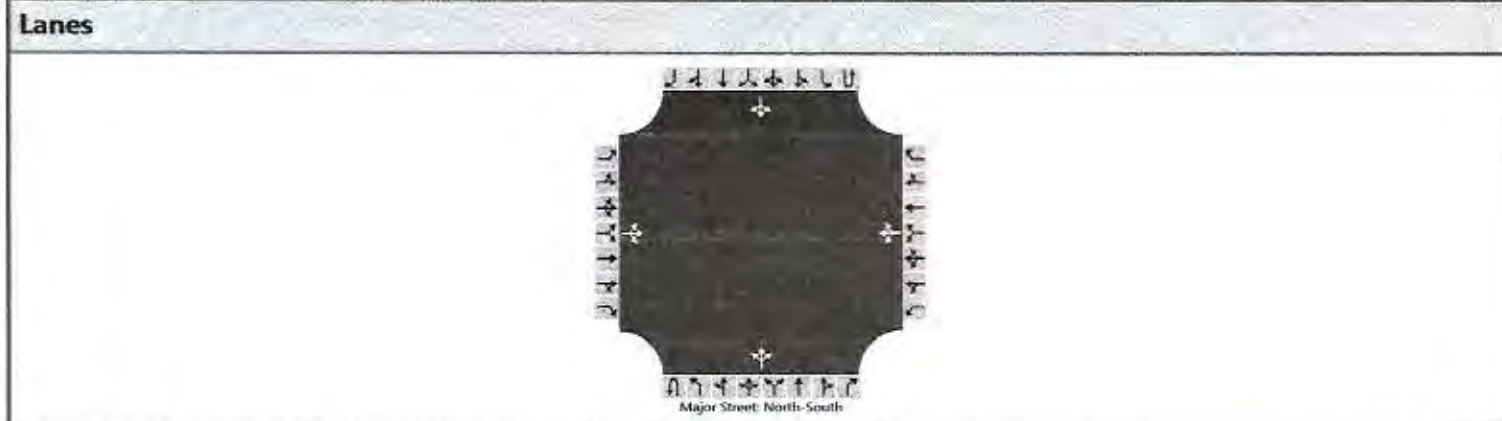
## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			142			19				76				2			
Capacity, c (veh/h)			880			515				1453				1559			
v/c Ratio			0.16			0.04				0.05				0.00			
95% Queue Length, Q <sub>95</sub> (veh)			0.6			0.1				0.2				0.0			
Control Delay (s/veh)			9.9			12.2				7.6				7.3			
Level of Service (LOS)			A			B				A				A			
Approach Delay (s/veh)		9.9				12.2				4.8				0.1			
Approach LOS		A				B											



# HCS7 Two-Way Stop-Control Report

General Information		Site Information	
Analyst	MSH	Intersection	Crystal Canyon/Aquamarine
Agency/Co.	Solaegui Engineers	Jurisdiction	Washoe County
Date Performed	10/19/2020	East/West Street	Aquamarine Drive
Analysis Year	2040	North/South Street	Crystal Canyon Boulevard
Time Analyzed	PM Base	Peak Hour Factor	0.90
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25
Project Description			



**Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound				
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R	
Movement																	
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0	
Configuration			LTR				LTR				LTR				LTR		
Volume (veh/h)		3	4	48		7	3	1		123	132	13		2	61	1	
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2			
Proportion Time Blocked																	
Percent Grade (%)		0				0											
Right Turn Channelized																	
Median Type   Storage		Undivided															

**Critical and Follow-up Headways**

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

**Delay, Queue Length, and Level of Service**

Flow Rate, v (veh/h)			61				12				137				2		
Capacity, c (veh/h)			852				428				1532				1418		
v/c Ratio			0.07				0.03				0.09				0.00		
95% Queue Length, Q <sub>95</sub> (veh)			0.2				0.1				0.3				0.0		
Control Delay (s/veh)			9.6				13.7				7.6				7.5		
Level of Service (LOS)			A				B				A				A		
Approach Delay (s/veh)		9.6				13.7				3.9				0.2			
Approach LOS		A				B											



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	AM Base + Project
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Crystal Canyon/Aquamarine
Jurisdiction	Washoe County
East/West Street	Aquamarine Drive
North/South Street	Crystal Canyon Boulevard
Peak Hour Factor	0.85
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	10	1	2	3	4	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		2	6	130		9	5	2		70	40	1		2	112	0
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized																
Median Type   Storage		Undivided														

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			162				19				82				2	
Capacity, c (veh/h)			883				492				1453				1559	
v/c Ratio			0.18				0.04				0.06				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.7				0.1				0.2				0.0	
Control Delay (s/veh)			10.0				12.6				7.6				7.3	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)		10.0				12.6				5.0				0.1		
Approach LOS		A				B										



# HCS7 Two-Way Stop-Control Report

## General Information

Analyst	MSH
Agency/Co.	Solaegui Engineers
Date Performed	10/19/2020
Analysis Year	2040
Time Analyzed	PM Base + Project
Intersection Orientation	North-South
Project Description	

## Site Information

Intersection	Crystal Canyon/Aquamarine
Jurisdiction	Washoe County
East/West Street	Aquamarine Drive
North/South Street	Crystal Canyon Boulevard
Peak Hour Factor	0.90
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Movement																
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		3	4	57		7	3	1		138	132	13		2	61	1
Percent Heavy Vehicles (%)		2	2	2		2	2	2		2				2		
Proportion Time Blocked																
Percent Grade (%)		0				0										
Right Turn Channelized																
Median Type   Storage		Undivided														

## Critical and Follow-up Headways

Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.12	6.52	6.22		7.12	6.52	6.22		4.12				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.52	4.02	3.32		3.52	4.02	3.32		2.22				2.22		

## Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)			71				12				153				2	
Capacity, c (veh/h)			858				399				1532				1418	
v/c Ratio			0.08				0.03				0.10				0.00	
95% Queue Length, Q <sub>95</sub> (veh)			0.3				0.1				0.3				0.0	
Control Delay (s/veh)			9.6				14.3				7.6				7.5	
Level of Service (LOS)			A				B				A				A	
Approach Delay (s/veh)		9.6				14.3				4.1				0.2		
Approach LOS		A				B										

## UPDATED TRAFFIC SIGNAL WARRANT ANALYSIS

### Traffic Volumes

Traffic volumes for the warrant analysis at the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections were obtained by adding traffic generated by the unbuilt Woodland Village dwelling units, unbuilt Cold Springs Elementary School, and Village Parkway and Village Center Residential developments to the existing traffic volumes.

The existing hourly traffic volumes and unbuilt Woodland Village hourly traffic volumes were obtained from the original warrant analysis letter dated January 15, 2020 with updated peak hour counts conducted at the Village Parkway/White Lake Parkway intersection in October 2020. The peak hour traffic volumes for the elementary school were obtained from the Cold Springs Elementary School Traffic Study dated March 2019. The peak hour traffic volumes for the Village Parkway and Village Center Residential developments were calculated based on *ITE Trip Generation*. Trips generated by the school and the proposed Village Parkway and Village Center Residential developments during the remaining hours were estimated based on hourly percentages of daily traffic obtained from *ITE Trip Generation*. The entering and departing trips during the non-peak hours were estimated based on existing traffic volume splits on the key roadways.

Table 1A shows the hourly traffic volumes at the White Lake Parkway/Crystal Canyon Boulevard intersection for the period between 7:00 AM and 6:00 PM.

Table 1A Hourly Traffic Volumes White Lake Parkway/Crystal Canyon Boulevard Intersection								
Time Period	White Lake Parkway (Major Street)					Crystal Canyon Blvd. (Minor Street)		
	NB Thru	NB Right	SB Left	SB Thru	Total	WB Left	WB Right	Total
7:00 AM - 8:00 AM	50	93	3	224	370	317	10	327
8:00 AM - 9:00 AM	86	61	2	176	325	191	12	203
9:00 AM - 10:00 AM	51	49	2	115	217	133	6	139
10:00 AM - 11:00 AM	67	64	4	109	244	145	7	152
11:00 AM - 12:00 PM	99	73	6	96	274	106	9	115
12:00 PM - 1:00 PM	118	147	6	85	356	86	9	95
1:00 PM - 2:00 PM	140	159	8	79	386	102	8	110
2:00 PM - 3:00 PM	143	165	9	81	398	106	9	115
3:00 PM - 4:00 PM	227	226	9	176	638	105	7	112
4:00 PM - 5:00 PM	279	313	13	89	694	96	8	104
5:00 PM - 6:00 PM	249	301	7	92	649	94	9	103



Table 1B shows the hourly traffic volumes at the Village Parkway/White Lake Parkway intersection for the period between 6:00 AM and 6:00 PM.

Time Period	Village Parkway (Major Street)					White Lake Parkway (Minor Street)		
	NB Thru	NB Right	SB Left	SB Thru	Total	WB Left	WB Right	Total
6:00 AM - 7:00 AM	81	8	27	412	528	20	15	35
7:00 AM - 8:00 AM	188	15	49	516	768	16	49	65
8:00 AM - 9:00 AM	97	15	31	328	471	33	18	51
9:00 AM - 10:00 AM	97	11	31	282	421	13	24	37
10:00 AM - 11:00 AM	94	11	28	234	367	15	23	38
11:00 AM - 12:00 PM	149	8	29	280	466	17	30	47
12:00 PM - 1:00 PM	300	12	28	219	559	17	37	54
1:00 PM - 2:00 PM	287	16	37	213	553	20	48	68
2:00 PM - 3:00 PM	284	23	26	215	548	25	55	80
3:00 PM - 4:00 PM	367	27	37	215	646	19	42	61
4:00 PM - 5:00 PM	496	22	39	240	797	25	70	95
5:00 PM - 6:00 PM	528	51	41	258	878	24	76	100

The hourly traffic volumes shown in Tables 1A and 1B were subsequently used in the traffic signal warrant analysis at the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections. These hourly traffic volumes represent 2030 and 2040 base plus project conditions.

#### **Warrant Analysis at the White Lake Parkway/Crystal Canyon Boulevard Intersection**

Traffic Signal Warrants 1 through 3 as presented in the 2009 Edition of the Manual on Uniform Traffic Control Devices (MUTCD) were reviewed at the White Lake Parkway/Crystal Canyon Boulevard intersection. The intersection is an unsignalized three-leg intersection with stop sign control at the east approach. The intersection contains one shared left turn-through lane at the north approach, one through lane and one right turn lane at the south approach, and one shared left turn-right turn lane at the east approach. White Lake Parkway (major street) therefore has two lanes for moving traffic and Crystal Canyon Boulevard (minor street) has one lane for moving traffic. The speed limit is posted for 35 miles per hour on White Lake Parkway.

Warrant 1 - Eight Hour Vehicular Volume includes a review of two conditions. Condition A, Minimum Vehicular Volume, is intended for application at locations where a large volume of intersecting traffic is the principal reason to consider installing a traffic signal. Condition B, Interruption of Continuous Traffic, is intended for application at locations where Condition A is not satisfied and where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street. The need for a traffic signal shall be considered if one of the following conditions exist for each of any eight hours of an average day:

- A. The major street volume (total of both approaches) exceeds 600 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 150 vehicles per hour for a one lane approach for Condition A; or
- B. The major street volume (total of both approaches) exceeds 900 vehicles per hour for a one lane approach while the minor street volume (higher volume approach) exceeds 75 vehicles per hour for a one lane approach for Condition B.

The results of warrant 1 are shown in Table 2 for the highest hourly traffic volumes.

Table 2 Warrant 1 Results at White Lake Parkway/Crystal Canyon Boulevard Intersection									
Condition A – Minimum Vehicular Volume									
	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	150
Major Volume	370	325	244	386	398	638	694	649	600
Hour Met?	No	No	No	No	No	No	No	No	8
Condition B – Interruption of Continuous Traffic									
	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	75
Major Volume	370	325	244	386	398	638	694	649	900
Hour Met?	No	No	No	No	No	No	No	No	8

As shown in Table 2, no hours are met for Condition A and no hours are met for Condition B. The combination of Conditions A and B was subsequently reviewed. The combination of Conditions A and B indicates that the need for a traffic signal shall be considered if both of the following conditions exist for each of any eight hours of an average day:

- A. The major street volume (total of both approaches) exceeds 480 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 120 vehicles per hour for a one lane approach for Condition A; and
- B. The major street volume (total of both approaches) exceeds 720 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 60 vehicles per hour for a one lane approach for Condition B.

The results of warrant 1 for the combination of conditions A and B are shown in Table 3.

Table 3 Warrant 1 Combination Results at White Lake Parkway/Crystal Canyon Boulevard Intersection									
Condition A – Minimum Vehicular Volume									
	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	120
Major Volume	370	325	244	386	398	638	694	649	480
Hour Met?	No	No	No	No	No	No	No	No	8
Condition B – Interruption of Continuous Traffic									
	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	60
Major Volume	370	325	244	386	398	638	694	649	720
Hour Met?	No	No	No	No	No	No	No	No	8

As shown in Table 3, no hours are met for Condition A and no hours are met for Condition B. Traffic signal warrant 1 is not met for the hourly traffic volumes.

Warrant 2 – Four Hour Vehicular Volume is intended to be applied where the volume of the intersecting traffic is the principal reason to consider installing a traffic signal. The need for a traffic signal shall be considered if for each of any four hours of an average day the plotted points representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the minor street (higher volume approach) all fall above the applicable curve in Figure 4C-1 of the Manual on Uniform Traffic Control Devices for the existing combination of approach lanes. The curve shown in Figure 4C-1 levels out at a minor street lower threshold volume of 80 vehicles per hour for a one lane approach and a major street volume of approximately 1,300 vehicles per hour for two approach lanes.

The results of warrant 2 are shown in Table 4 for the highest hourly traffic volumes.

Table 4 Warrant 2 Results at White Lake Parkway/Crystal Canyon Boulevard Intersection									
	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	80
Major Volume	370	325	244	386	398	638	694	649	1300±
Hour Met?	No	No	No	No	No	No	No	No	4

As shown in Table 4, no hours are met for warrant 2. The minor street approach volumes meet the lower threshold volume but the low major street approach volumes result in the plotted points falling below the applicable curve. Traffic signal warrant 2 is not met for the hourly traffic volumes.



Warrant 3 - Peak Hour is intended for use at a location where traffic conditions are such that for a minimum of one hour of an average day, the minor street traffic suffers undue delay when entering or crossing the major street. The need for a traffic signal shall be considered if the criteria in either of the following two categories are met:

- A. If all three of the following conditions exist for the same hour of an average day:
  1. The total stopped time delay experienced by the traffic on one minor street approach (one direction only) controlled by a stop sign equals or exceeds 4 vehicle-hours for a one lane approach, and
  2. The volume on the same minor street approach (one direction only) equals or exceeds 100 vehicles per hour for one moving lane of traffic, and
  3. The total entering volume serviced during the hour equals or exceeds 650 vehicles per hour for intersections with three approaches.
  
- B. If the plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor street approach for one hour of an average day falls above the applicable curve in Figure 4C-3 for the existing combination of approach lanes. The curve in Figure 4C-3 levels out at a minor street lower threshold volume of 100 vehicles per hour for a one lane approach and a major street volume of approximately 1,700 vehicles per hour.

Category A was first reviewed for Warrant 3. The maximum delay on the minor street approach is approximately 1.5 vehicle-hours for the highest hour which is well below the 4 vehicle-hour threshold so category A is not met. Category B was subsequently reviewed. The results of warrant 3, category B are shown in Table 5 for the highest hourly traffic volumes.

	7-8 AM	8-9 AM	10-11 AM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	327	203	152	110	115	112	104	103	100
Major Volume	370	325	244	386	398	638	694	649	1700±
Hour Met?	No	No	No	No	No	No	No	No	1

As shown in Table 5, no hours are met for warrant 3. The minor street approach volume meets the lower threshold volume for multiple hours but the low major street approach volumes result in the plotted points falling below the applicable curve. Traffic signal warrant 3 is not met for the hourly traffic volumes.

## Warrant Analysis at the Village Parkway/White Lake Parkway Intersection

Traffic Signal Warrants 1 through 3 as presented in the 2009 Edition of the Manual on Uniform Traffic Control Devices (MUTCD) were reviewed at the Village Parkway/White Lake Parkway intersection. The Village Parkway/White Lake Parkway intersection is an unsignalized three-leg intersection with stop sign control at the east approach. The intersection contains one left turn lane and one through lane at the north approach, one through lane and one right turn lane at the south approach, and one shared left turn-right turn lane at the east approach. Village Parkway (major street) therefore has two lanes for moving traffic and White Lake Parkway (minor street) has one lane for moving traffic. The speed limit is posted for 35 miles per hour on Village Parkway.

Warrant 1 - Eight Hour Vehicular Volume includes a review of two conditions. Condition A, Minimum Vehicular Volume, is intended for application at locations where a large volume of intersecting traffic is the principal reason to consider installing a traffic signal. Condition B, Interruption of Continuous Traffic, is intended for application at locations where Condition A is not satisfied and where the traffic volume on a major street is so heavy that traffic on a minor intersecting street suffers excessive delay or conflict in entering or crossing the major street. The need for a traffic signal shall be considered if one of the following conditions exist for each of any eight hours of an average day:

- A. The major street volume (total of both approaches) exceeds 600 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 150 vehicles per hour for a one lane approach for Condition A; or
- B. The major street volume (total of both approaches) exceeds 900 vehicles per hour for a one lane approach while the minor street volume (higher volume approach) exceeds 75 vehicles per hour for a one lane approach for Condition B.

The results of warrant 1 are shown in Table 6 for the highest hourly traffic volumes.

Table 6 Warrant 1 Results at Village Parkway/White Lake Parkway Intersection									
Condition A – Minimum Vehicular Volume									
	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	150
Major Volume	768	471	559	553	548	646	797	878	600
Hour Met?	No	No	No	No	No	No	No	No	8
Condition B – Interruption of Continuous Traffic									
	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	75
Major Volume	768	471	559	553	548	646	797	878	900
Hour Met?	No	No	No	No	No	No	No	No	8

As shown in Table 6, no hours are met for Condition A and no hours are met for Condition B. The combination of Conditions A and B was subsequently reviewed. The combination of Conditions A and B indicates that the need for a traffic signal shall be considered if both of the following conditions exist for each of any eight hours of an average day:

- A. The major street volume (total of both approaches) exceeds 480 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 120 vehicles per hour for a one lane approach for Condition A; and
- B. The major street volume (total of both approaches) exceeds 720 vehicles per hour for a two lane approach while the minor street volume (higher volume approach) exceeds 60 vehicles per hour for a one lane approach for Condition B.

The results of warrant 1 for the combination of conditions A and B are shown in Table 7 for the highest hourly traffic volumes.

Table 7 Warrant 1 Combination Results at Village Parkway/White Lake Parkway Intersection									
Condition A – Minimum Vehicular Volume									
	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	120
Major Volume	768	471	559	553	548	646	797	878	480
Hour Met?	No	No	No	No	No	No	No	No	8
Condition B – Interruption of Continuous Traffic									
	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	60
Major Volume	768	471	559	553	548	646	797	878	720
Hour Met?	Yes	No	No	No	No	No	Yes	Yes	8

As shown in Table 7, no hours are met for Condition A and three hours are met for Condition B. Traffic signal warrant 1 is not met for the hourly traffic volumes.

Warrant 2 – Four Hour Vehicular Volume is intended to be applied where the volume of the intersecting traffic is the principal reason to consider installing a traffic signal. The need for a traffic signal shall be considered if for each of any four hours of an average day the plotted points representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the minor street (higher volume approach) all fall above the applicable curve in Figure 4C-1 of the Manual on Uniform Traffic Control Devices for the existing combination of approach lanes. The curve shown in Figure 4C-1 levels out at a minor street lower threshold volume of 80 vehicles per hour for a one lane approach and a major street volume of approximately 1,300 vehicles per hour for two approach lanes.



The results of warrant 2 are shown in Table 8 for the highest hourly traffic volumes.

	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	80
Major Volume	768	471	559	553	548	646	797	878	1300±
Hour Met?	No	No	No	No	No	No	No	No	4

No hours are met for warrant 2. The minor street approach volume meets the lower threshold volume for some hours but the low major street approach volumes result in the plotted points falling below the applicable curve. Traffic signal warrant 2 is not met for hourly traffic volumes.

Warrant 3 - Peak Hour is intended for use at a location where traffic conditions are such that for a minimum of one hour of an average day, the minor street traffic suffers undue delay when entering or crossing the major street. The need for a traffic signal shall be considered if the criteria in either of the following two categories are met:

- A. If all three of the following conditions exist for the same hour of an average day:
  1. The total stopped time delay experienced by the traffic on one minor street approach (one direction only) controlled by a stop sign equals or exceeds 4 vehicle-hours for a one lane approach, and
  2. The volume on the same minor street approach (one direction only) equals or exceeds 100 vehicles per hour for one moving lane of traffic, and
  3. The total entering volume serviced during the hour equals or exceeds 650 vehicles per hour for intersections with three approaches.
  
- B. If the plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor street approach for one hour of an average day falls above the applicable curve in Figure 4C-3 for the existing combination of approach lanes. The curve in Figure 4C-3 levels out at a minor street lower threshold volume of 100 vehicles per hour for a one lane approach and a major street volume of approximately 1,700 vehicles per hour.

Category A was first reviewed for warrant 3. The maximum delay on the minor street approach is approximately 0.5 vehicle-hours for the highest hour which is well below the 4 vehicle-hour threshold so category A is not met. Category B was subsequently reviewed. The results of warrant 3, category B are shown in Table 9 for the highest hourly traffic volumes.

	7-8 AM	8-9 AM	12-1 PM	1-2 PM	2-3 PM	3-4 PM	4-5 PM	5-6 PM	Req'd
Minor Volume	65	51	54	68	80	61	95	100	100
Major Volume	768	471	559	553	548	646	797	878	1700±
Hour Met?	No	No	No	No	No	No	No	No	1

As shown in Table 9, no hours are met for warrant 3. The minor street approach volume meets the lower threshold volume for one hour but the low major street approach volumes result in the plotted points falling below the applicable curve. Traffic signal warrant 3 is not met for the hourly traffic volumes.

### Findings

The traffic signal warrant analysis indicates that vehicular warrants 1 through 3 are not met at the White Lake Parkway/Crystal Canyon Boulevard and Village Parkway/White Lake Parkway intersections for the hourly traffic volumes.



**OWNER / DEVELOPER**  
LIFESTYLE HOMES TND LLC  
ATTN: ROBERT LISSNER  
4750 CAUGHLIN PARKWAY, #519  
RENO, NEVADA 89519

**BASIS OF ELEVATIONS**

NORTH AMERICA VERTICAL DATUM (NAVD83) 1002' WITH NORTH AT CORNER OF SECTION 14 (ELEVATION WITH 100' BENCH) HAS AN ELEVATION 5068.56  
NORTH AMERICAN DATUM OF 1983 IS BASED ON MEAN SEA LEVEL  
NETWORK COOPERATIVE BASE NETWORK OBSERVATIONS IN 1994 (AKA MARIKUSA)  
WASHOE COUNTY PUBLISHED LATITUDE AND LONGITUDE COORDINATES FOR THE  
NORTH AND 130° 01' 18.889" WEST FOR REGIONAL GRID CORNER 37EA (WASHOE  
OF 1.0007897) IS USED TO SCALE THE STATE PLANE GRID COORDINATES TO  
GROUND.

**GENERAL CONSTRUCTION NOTES:**

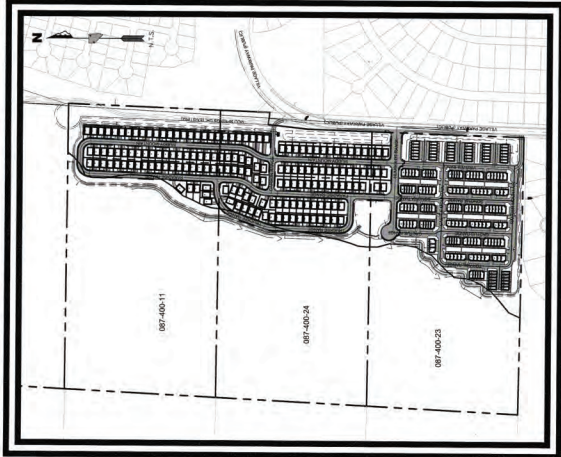
1. THESE NOTES APPLY TO ALL WORK UNDER CONTRACT. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS, LICENSES, AND APPROVALS FROM THE APPLICABLE AGENCIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS, LICENSES, AND APPROVALS FROM THE APPLICABLE AGENCIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS, LICENSES, AND APPROVALS FROM THE APPLICABLE AGENCIES.
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# TENTATIVE MAP PLANS FOR VILLAGE PARKWAY HOMES

COLD SPRINGS WASHOE COUNTY NEVADA



VICINITY MAP N.T.S.



SITE PLAN N.T.S.

**SHEET INDEX**

T-1	TITLE SHEET
S-0	OVERALL SITE PLAN
S-1	PRELIMINARY SITE PLAN
S-2	PRELIMINARY SITE PLAN
S-3	PRELIMINARY SITE PLAN
S-4	PRELIMINARY SITE PLAN
G-0	OVERALL GRADING PLAN
G-1	PRELIMINARY GRADING PLAN
G-2	PRELIMINARY GRADING PLAN
G-3	PRELIMINARY GRADING PLAN
G-4	PRELIMINARY GRADING PLAN
G-5	PRELIMINARY GRADING PLAN
C-0	CUT/FILL MAP
U-1	UTILITY PLAN
U-2	PRELIMINARY UTILITY PLAN
U-3	PRELIMINARY UTILITY PLAN
U-4	PRELIMINARY UTILITY PLAN
X-1	PRELIMINARY CROSS SECTIONS
X-2	CROSS SECTIONS
X-3	CROSS SECTIONS
L-1	PRELIMINARY LANDSCAPE PLAN

**PROJECT DATA**

166 LOTS
SINGLE FAMILY ATTACHED LOTS
TOTAL LOTS
TOTAL AREA
COMMON OPEN SPACE AREA
PUBLIC RIGHT OF WAY
TOTAL LOT AREA
GROSS DENSITY
AVERAGE ATTACHED LOT SIZE
LARGEST ATTACHED LOT
SMALLEST ATTACHED LOT

**ABBREVIATIONS**

A.C.	ASPHALTIC CONCRETE
B.C.	BEST PRACTICES
B.F.	BEST MANAGEMENT PRACTICES
B.M.	BEST MANAGEMENT PRACTICES
B.P.	BEST PRACTICES
B.S.	BEST MANAGEMENT PRACTICES
B.T.	BEST MANAGEMENT PRACTICES
B.V.	BEST MANAGEMENT PRACTICES
B.W.	BEST MANAGEMENT PRACTICES
B.Y.	BEST MANAGEMENT PRACTICES
B.Z.	BEST MANAGEMENT PRACTICES
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B.50.	BEST MANAGEMENT PRACTICES

**ENGINEER'S STATEMENT**

THESE PLANS SHEETS 1-1 THROUGH 1-22 HAVE BEEN PREPARED IN ACCORDANCE WITH ACCREDITED ENGINEERING PROCEDURES AND GUIDELINES, AND ARE IN SUBSTANTIAL COMPLIANCE WITH APPLICABLE LOCAL, STATE AND FEDERAL REGULATIONS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS, LICENSES, AND APPROVALS FROM THE APPLICABLE AGENCIES.

ROBERT GELU P.E. #17141



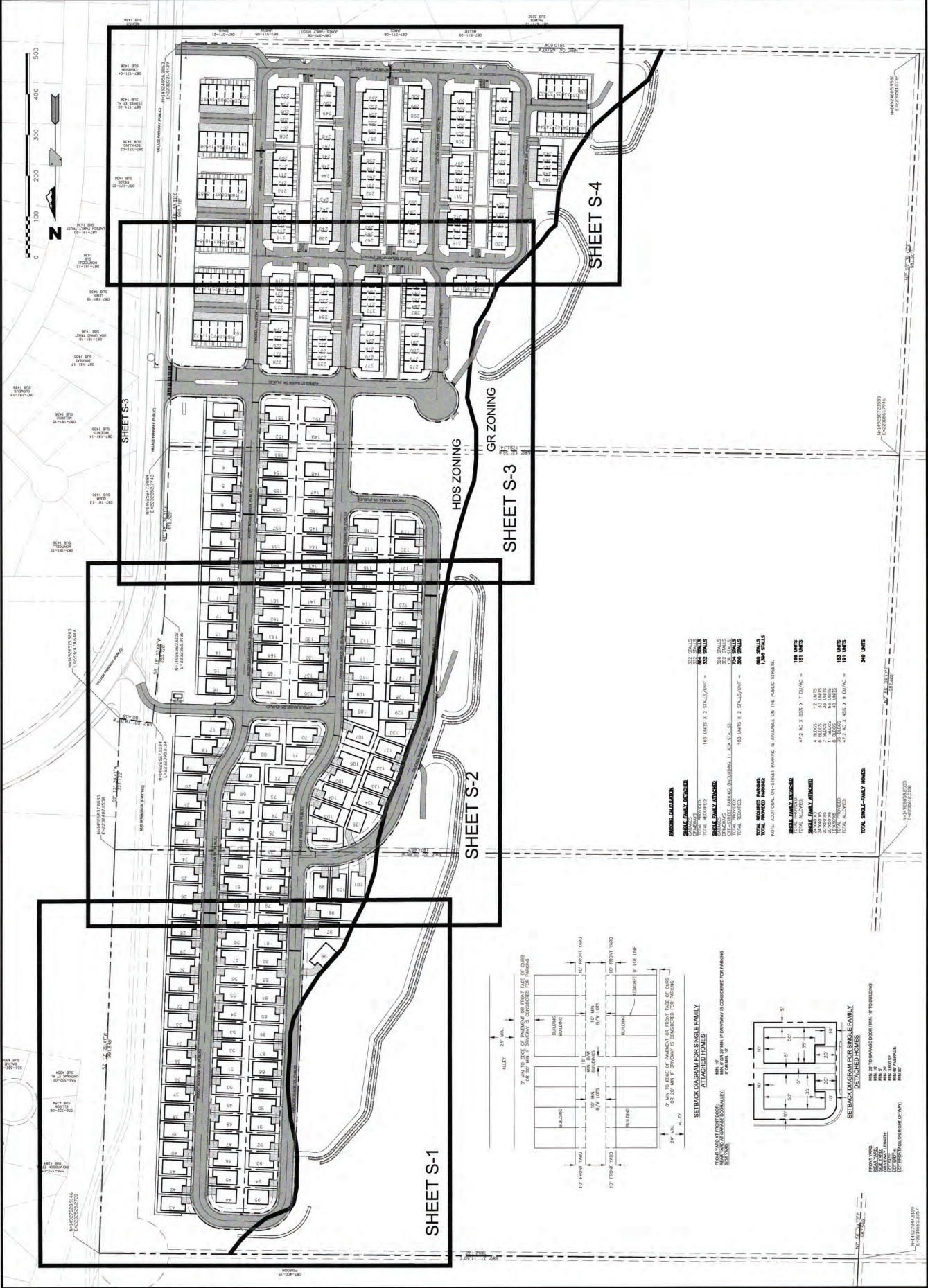
**SUMMIT ENGINEERING CORPORATION**  
 5405 MAE ANNE AVENUE, RENO, NV 89423  
 PHONE: (775) 747-8550 FAX: (775) 747-8559

REV.	DATE	DESCRIPTION	BY	APP'D

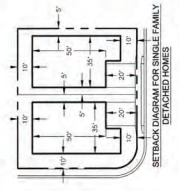
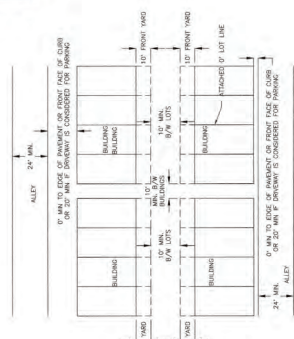
NEVADA  
 WASHOE COUNTY  
 COLD SPRINGS  
**TENTATIVE MAP PLANS FOR VILLAGE PARKWAY HOMES OVERALL SITE PLAN**

DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE: 1"=100'  
 HORIZ. 1"=100'  
 VERT. 1"=100'  
 JOB NO: 31097

**S-0**  
 SHEET 22 OF 22

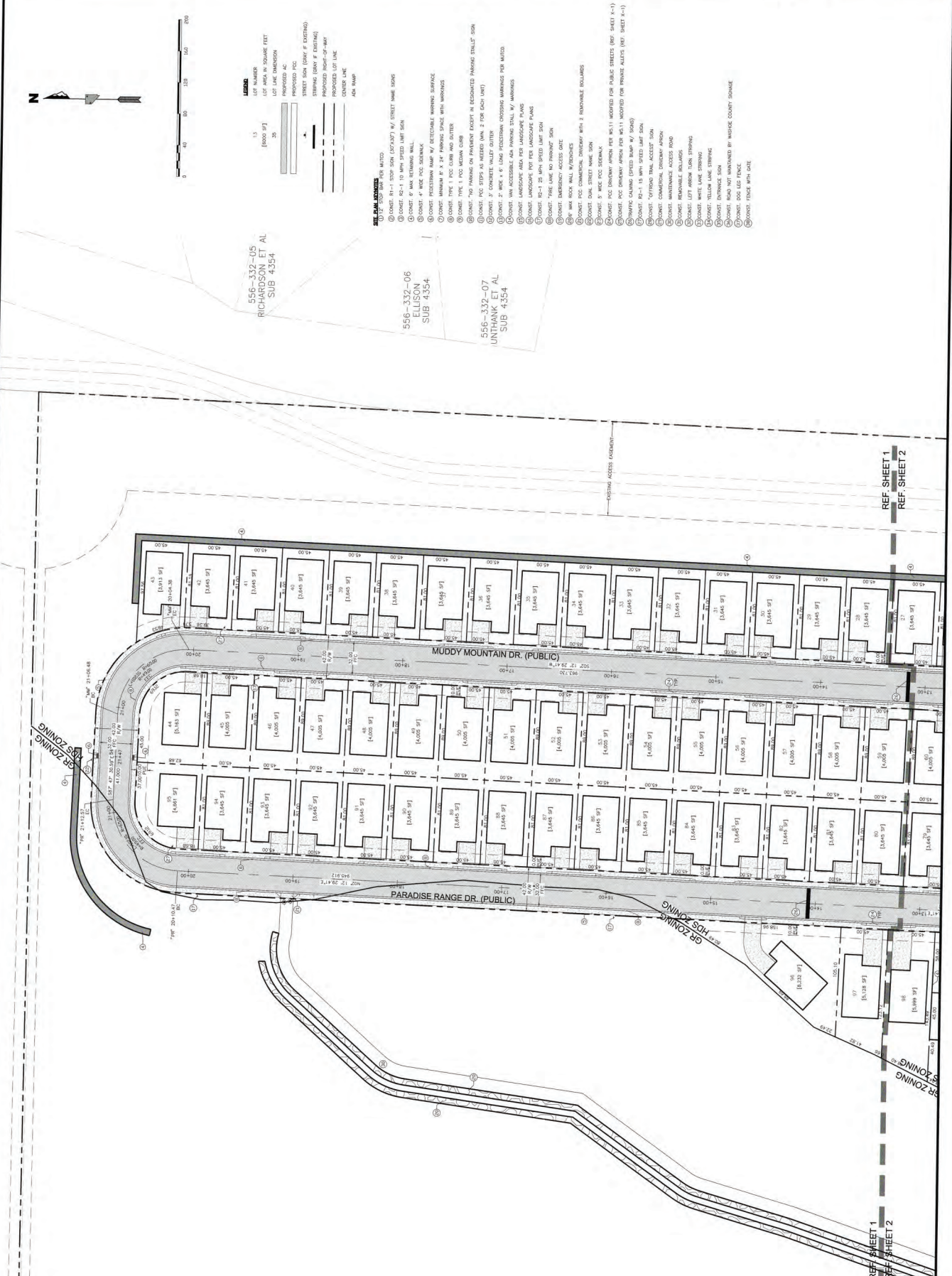


FAMILY CALCULATION	
<b>SINGLE FAMILY DETACHED</b>	332 UNITS
TOTAL UNITS	332 UNITS
TOTAL REQUIRED	166 UNITS X 2 STALLS/UNIT = 332 STALLS
<b>SINGLE FAMILY ATTACHED</b>	206 UNITS
TOTAL UNITS	206 UNITS
TOTAL REQUIRED	103 UNITS X 2 STALLS/UNIT = 206 STALLS
<b>TOTAL UNITS</b>	538 UNITS
<b>TOTAL REQUIRED PARKING</b>	269 STALLS
NOTE: ADDITIONAL ON-STREET PARKING IS AVAILABLE ON THE PUBLIC STREETS.	
<b>SINGLE FAMILY ATTACHED</b>	188 UNITS
TOTAL UNITS	188 UNITS
TOTAL REQUIRED	94 UNITS X 2 STALLS/UNIT = 188 STALLS
<b>SINGLE FAMILY DETACHED</b>	472 UNITS
TOTAL UNITS	472 UNITS
TOTAL REQUIRED	236 UNITS X 2 STALLS/UNIT = 472 STALLS
<b>TOTAL UNITS</b>	660 UNITS
<b>TOTAL REQUIRED PARKING</b>	330 STALLS
NOTE: ADDITIONAL ON-STREET PARKING IS AVAILABLE ON THE PUBLIC STREETS.	
<b>TOTAL SINGLE-FAMILY HOMES</b>	340 UNITS





REV.	DATE	DESCRIPTION	BY	APPD.



- NOTES:**
1. ALL DIMENSIONS ARE IN FEET.
  2. ALL DIMENSIONS ARE TO THE CENTERLINE OF THE ROAD UNLESS OTHERWISE NOTED.
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556-332-05  
 RICHARDSON ET AL  
 SUB 4354

556-332-06  
 ELLISON  
 SUB 4354

556-332-07  
 LINTHANK ET AL  
 SUB 4354

REF. SHEET 1  
 REF. SHEET 2

REF. SHEET 1  
 REF. SHEET 2

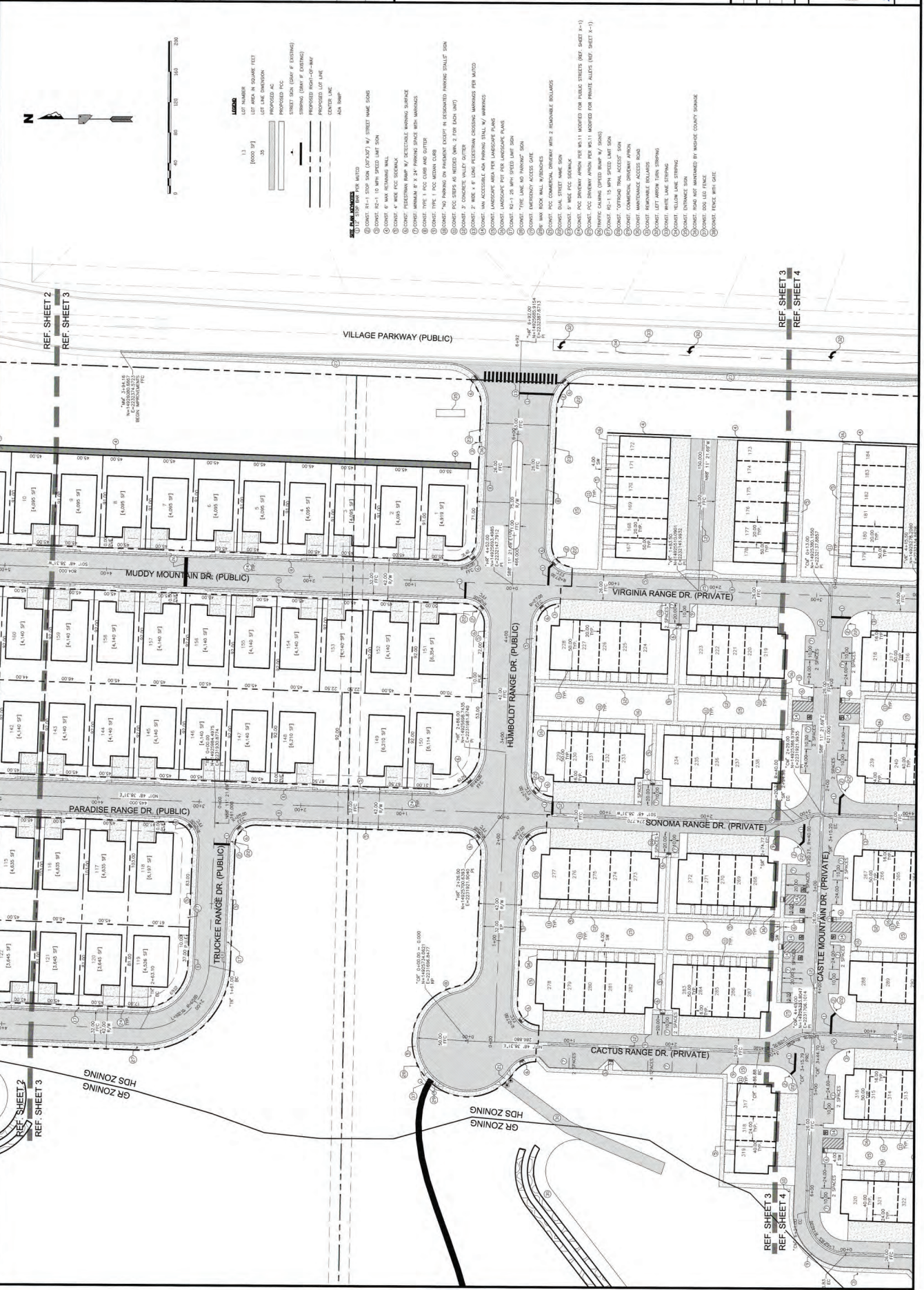








REV.	DATE	DESCRIPTION	BY	APPD.



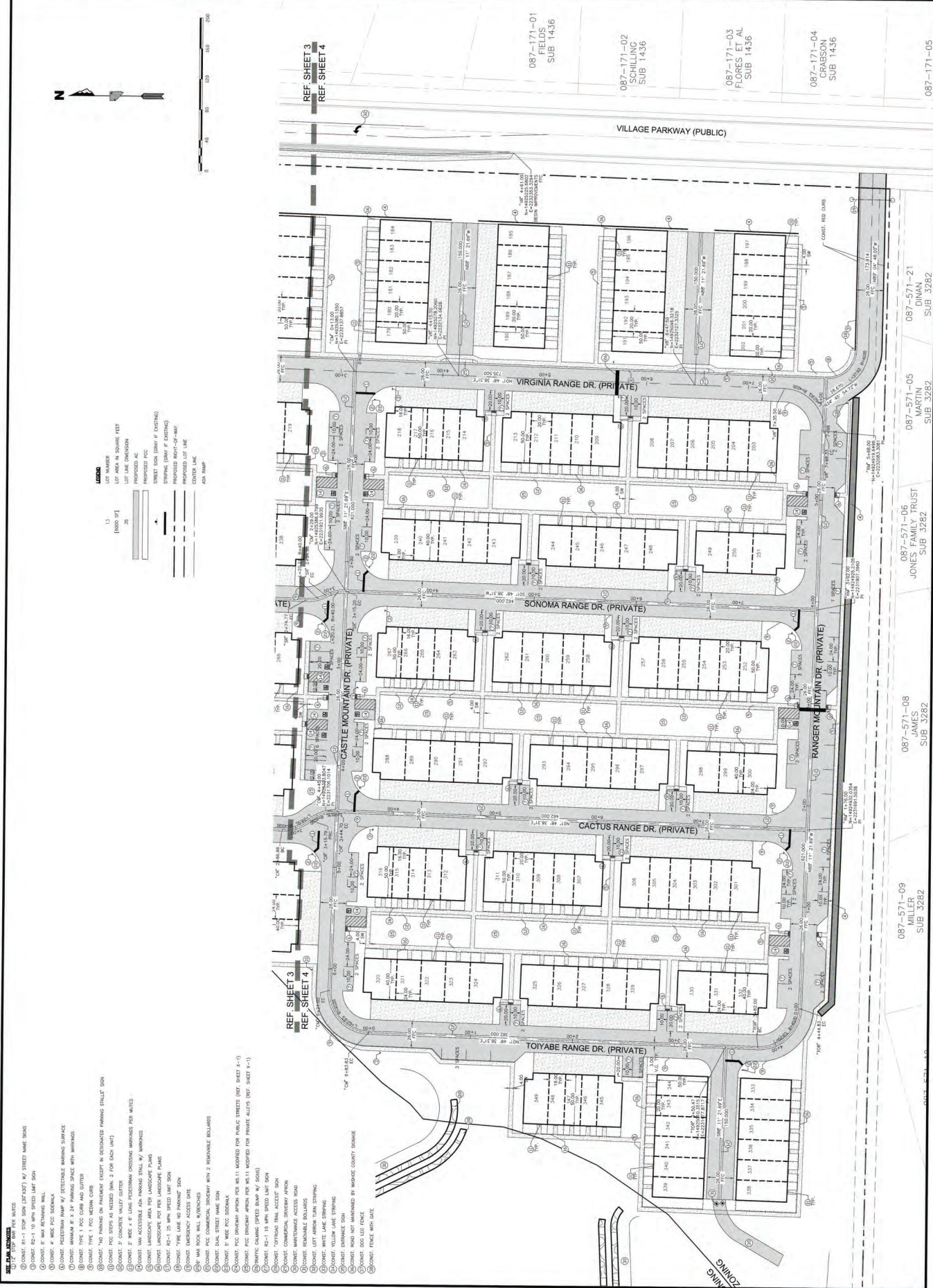


REV.	DATE	DESCRIPTION	BY	APPD.

COLD SPRINGS WASHOE COUNTY NEVADA  
**TENTATIVE MAP PLANS FOR VILLAGE PARKWAY HOMES PRELIMINARY SITE PLAN**

DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ. 1"=40'  
 VERT. 1"=10'  
 JOB NO. 31087

  
 ROBERT J. SCHILLING  
 LICENSE NO. 68-003  
 CIVIL ENGINEER  
 STATE OF NEVADA



- SEE PLAN NOTES**
- 1. CONE: 10' STOP SIGN (REF. SHEET 3) W/ STREET NAME SIGNS
  - 2. CONE: 10' X 10' STOP SIGN
  - 3. CONE: 4' WIDE SPEED LIMIT SIGN
  - 4. CONE: 4' WIDE POC SIGN
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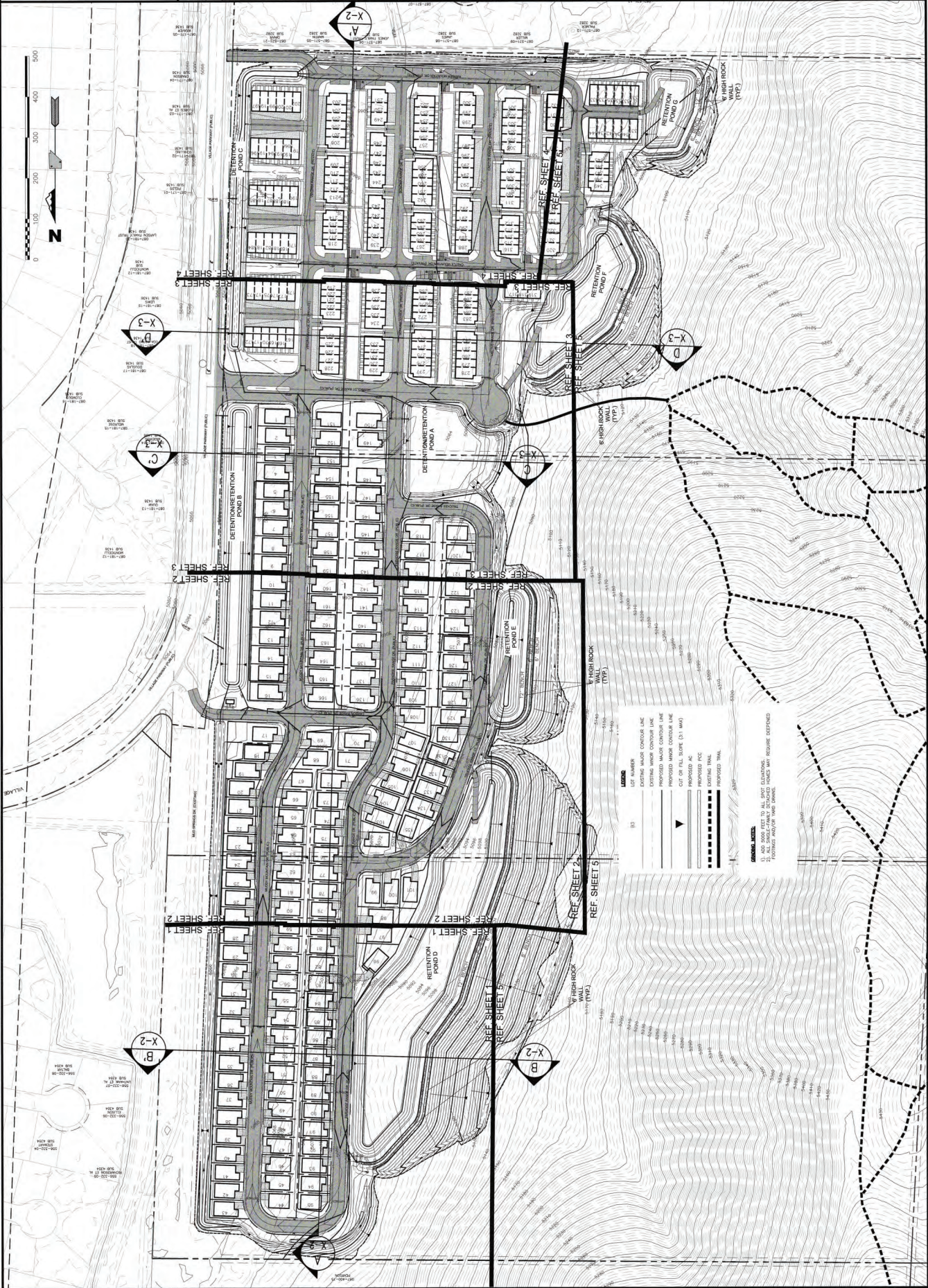


REV.	DATE	DESCRIPTION	BY	APP'D

NEVADA  
 WASHOE COUNTY  
 COLD SPRINGS  
**TENTATIVE MAP PLANS FOR  
 VILLAGE PARKWAY HOMES  
 OVERALL GRADING PLAN**

DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ: 1"=100'  
 VERT:  
 JOB NO: 31097

7-8-21  
  
 SHEET OF 22  
 G-0









REV.	DATE	DESCRIPTION	BY	APPD.

NEVADA  
 WASHOE COUNTY  
**TENTATIVE MAP PLANS FOR  
 VILLAGE PARKWAY HOMES**  
 COLD SPRINGS  
 PRELIMINARY GRADING PLAN

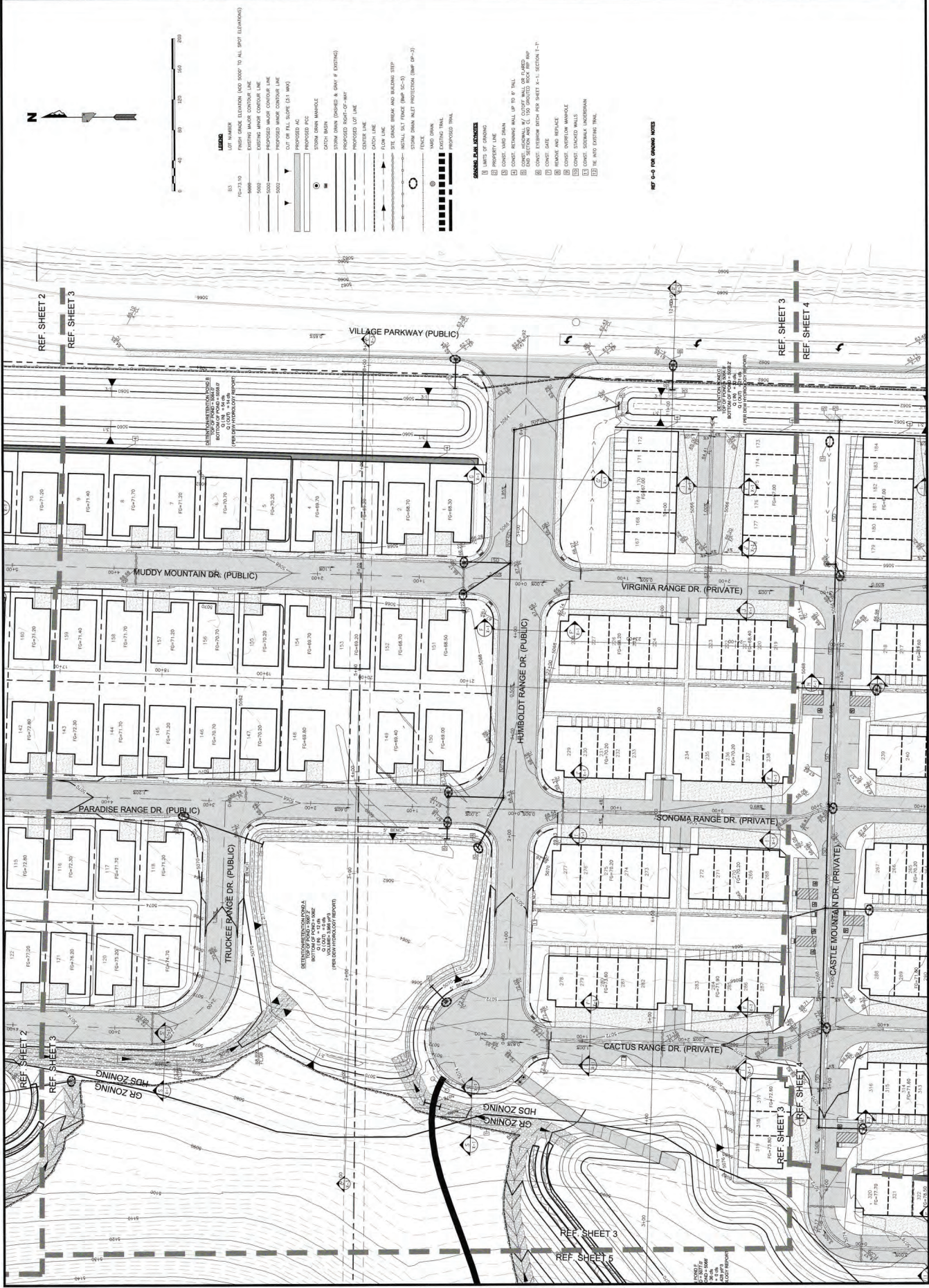
DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ: 1"=40'  
 VERT: 1"=4'  
 JOB NO: 21097  
 SHEET G-2 of 22





REV.	DATE	DESCRIPTION	BY	APP'D

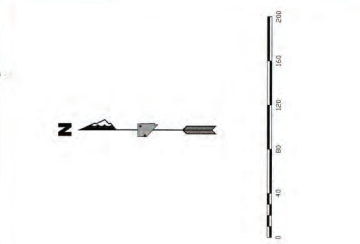
DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ: 1"=40'  
 VERT: 1"=4'  
 JOB NO. 31097



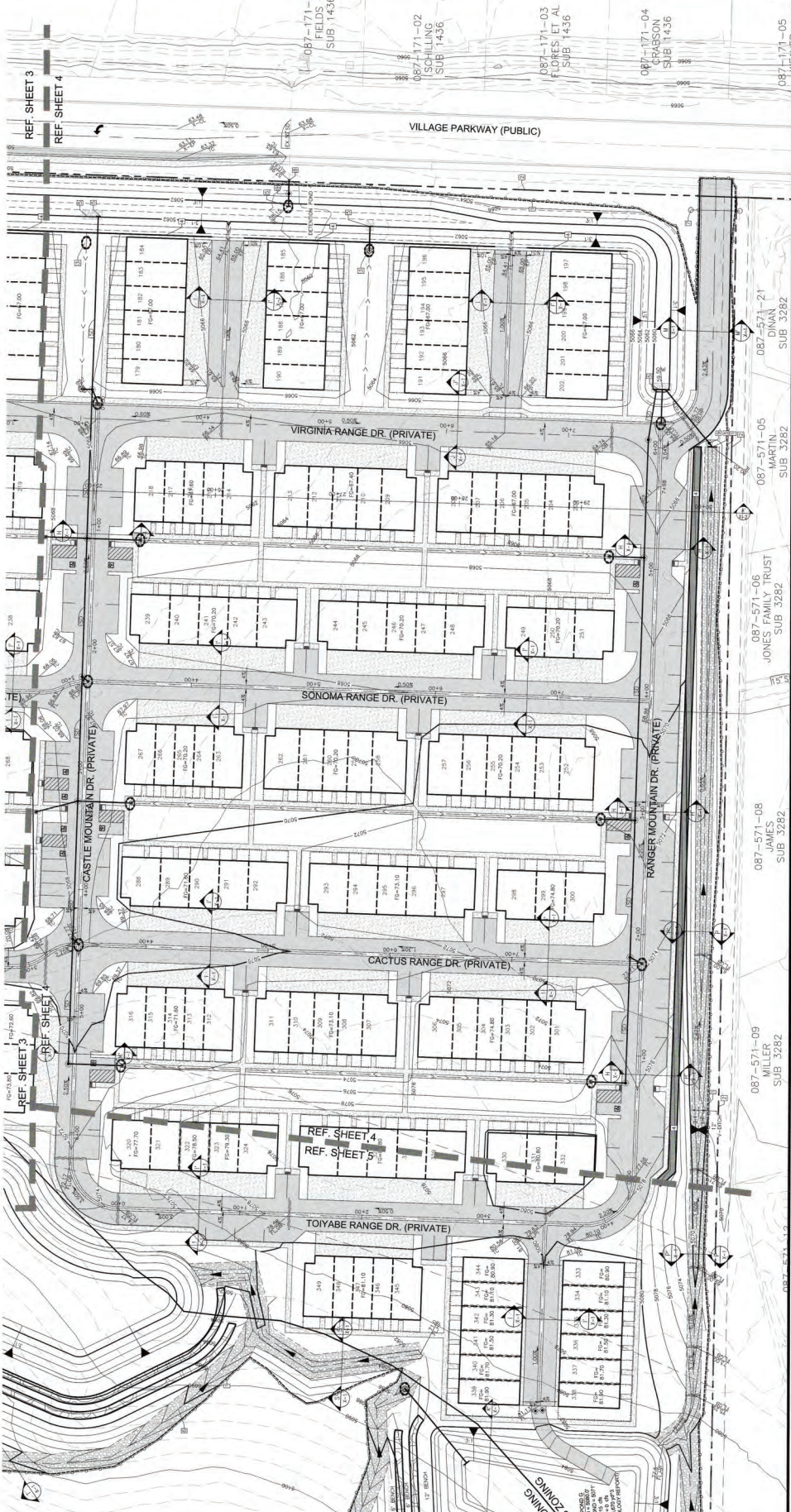
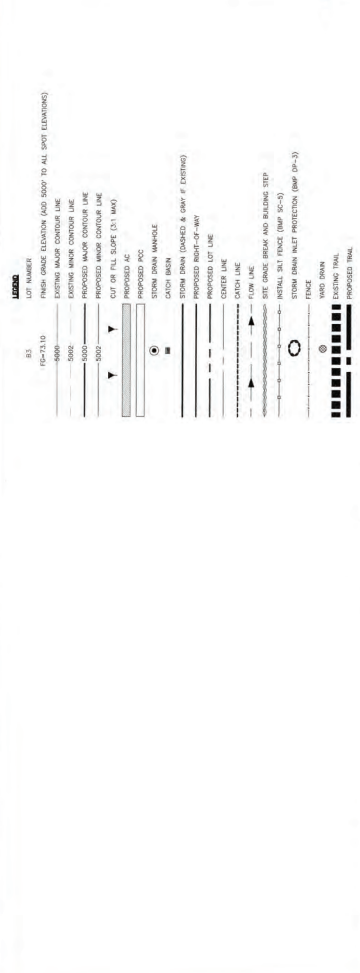


REV.	DATE	DESCRIPTION	BY	APP'D.

DESIGNED BY: RG	CHECKED BY: RG
SCALE	HORIZ: 1"=40'
VERT: 1"=4'	JOB NO. 31097



- GENERAL NOTES**
1. ALL ELEVATIONS UNLESS OTHERWISE NOTED ARE IN FEET.
  2. FINISH GRADE ELEVATION (F&G) SHOWN TO ALL SPOTS (ELEVATIONS).
  3. EXISTING MAJOR CONTOUR LINE.
  4. EXISTING MINOR CONTOUR LINE.
  5. PROPOSED MAJOR CONTOUR LINE.
  6. PROPOSED MINOR CONTOUR LINE.
  7. CUT OR FILL SLOPE (3:1 MAX).
  8. STORM DRAIN MANHOLE.
  9. CATCH BASIN.
  10. STORM DRAIN (DASHED & GRAY IF EXISTING).
  11. PROPOSED RIGHT-OF-WAY.
  12. PROPOSED LOT LINE.
  13. EXISTING LOT LINE.
  14. EXISTING FLOW LINE.
  15. SITE GRADE BREAK AND BUILDING STEP.
  16. INSTALL S&I FENCE (RMP (S-3)).
  17. STORM DRAIN INLET PROTECTION (RMP (S-3)).
  18. FENCE.
  19. WIND ZONE.
  20. EXISTING TRAIL.
  21. PROPOSED TRAIL.









REV.	DATE	DESCRIPTION	BY	APPD.

DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ: 1"=100'  
 VERT:  
 JOB NO. 31087



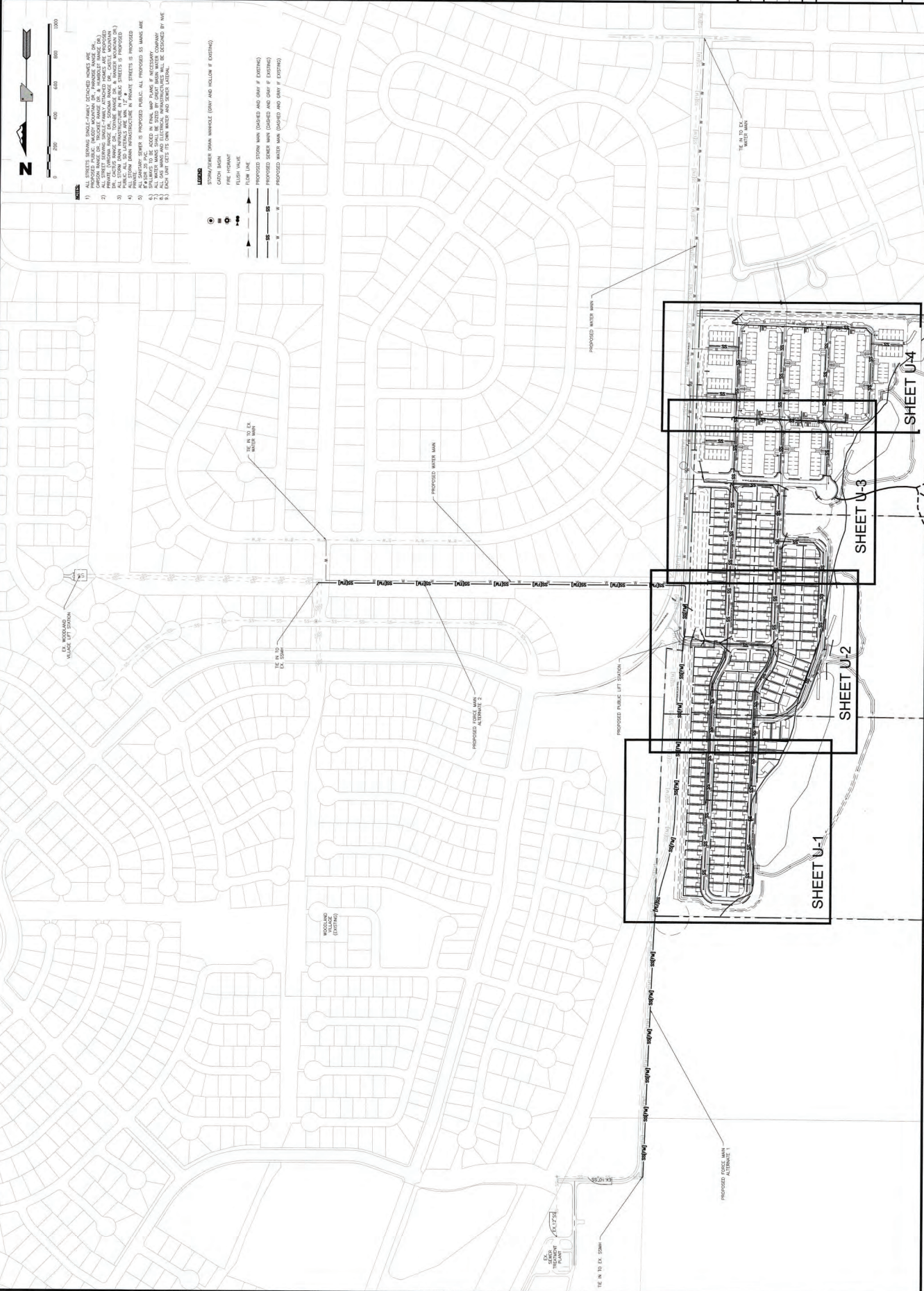
**EARTHWORK QUANTITIES:**

TOTAL DISTURBED AREA = 57.5 AC
TOTAL CUT = 326,548 CY
TOTAL FILL = 255,214 CY
NET CUT = 71,334 CY
DEEPEST CUT = 35 FT
DEEPEST FILL = 10 FT

- LEGEND:**
- 35'-10" CUT
  - 0'-10" CUT
  - 0'-10" FILL



REV.	DATE	DESCRIPTION	BY	APPD.







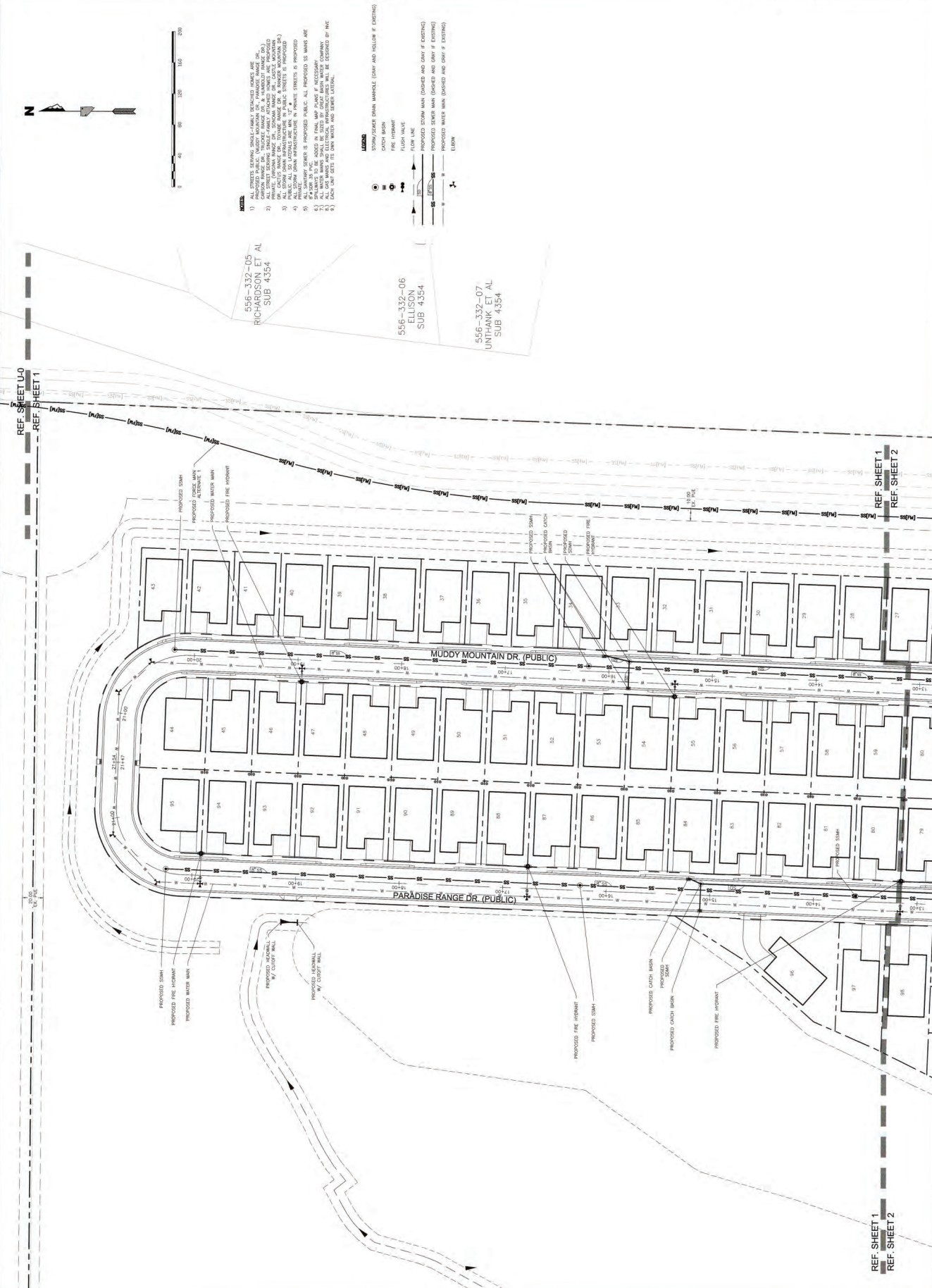
REV.	DATE	DESCRIPTION	BY	APPD.

WASHOE COUNTY  
COLD SPRINGS  
PRELIMINARY UTILITY PLAN  
VILLAGE PARKWAY HOMES  
NEVADA

DESIGNED BY: RG  
CHECKED BY: RG  
SCALE  
HORIZ: 1"=40'  
VERT:  
JOB NO. 31087



SHEET OF U-1 22



- NOTES:**
- 1) ALL STREETS BEARING DRINKING WATER SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY WATER MAIN DESIGN SPECIFICATIONS.
  - 2) ALL STREETS BEARING SEWER SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY SEWER DESIGN SPECIFICATIONS.
  - 3) ALL STREETS BEARING STORM DRAINAGE SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY STORM DRAINAGE DESIGN SPECIFICATIONS.
  - 4) ALL STREETS BEARING FIRE WATER SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY FIRE WATER DESIGN SPECIFICATIONS.
  - 5) ALL STREETS BEARING PUBLIC UTILITY SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY PUBLIC UTILITY DESIGN SPECIFICATIONS.
  - 6) ALL STREETS BEARING PRIVATE UTILITY SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY PRIVATE UTILITY DESIGN SPECIFICATIONS.
  - 7) ALL UTILITY LINES SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY UTILITY DESIGN SPECIFICATIONS.
  - 8) ALL UTILITY LINES SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY UTILITY DESIGN SPECIFICATIONS.
  - 9) ALL UTILITY LINES SHALL BE DESIGNED TO MEET THE REQUIREMENTS OF THE WASHOE COUNTY UTILITY DESIGN SPECIFICATIONS.



656-332-06  
RICHARDSON ET AL  
SUB 4354

556-332-06  
ELLISON  
SUB 4354

556-332-07  
UNTHANK ET AL  
SUB 4354















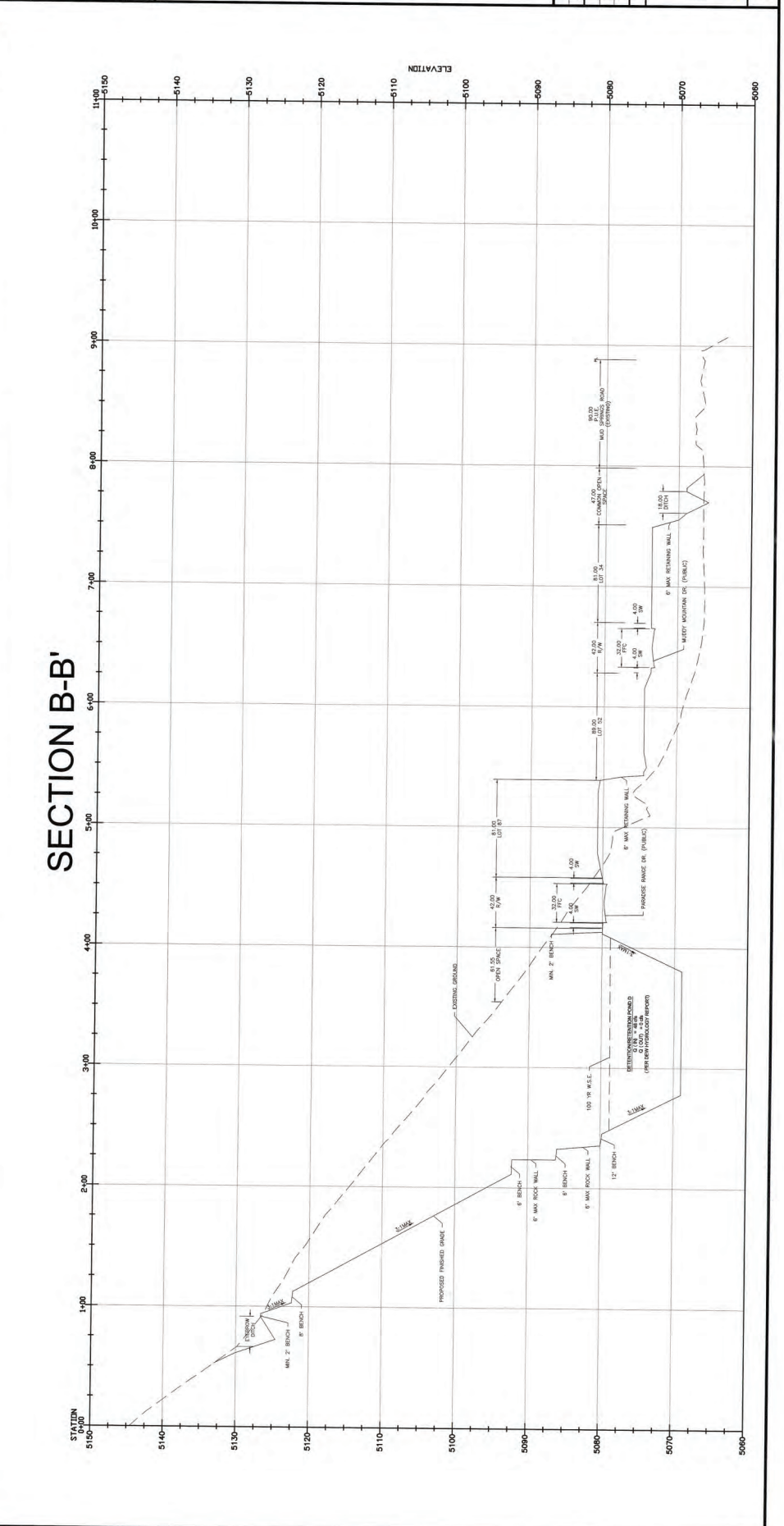
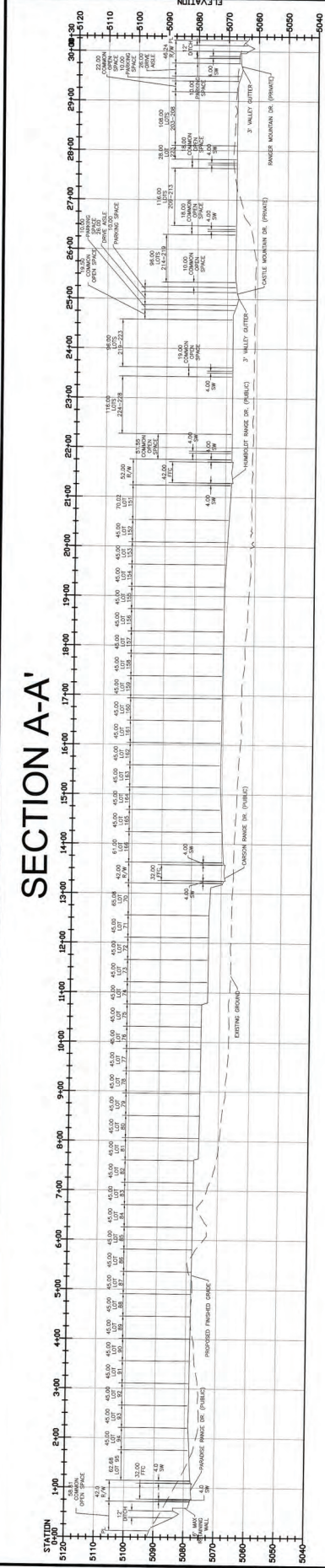




REV	DATE	DESCRIPTION	BY	APP'D

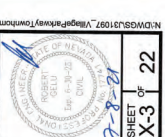
TENTATIVE MAP PLANS FOR  
 VILLAGE PARKWAY HOMES  
 CROSS SECTIONS  
 WASHOE COUNTY  
 NEVADA

COLD SPRINGS  
 DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORIZ: N.T.S.  
 VERT:  
 JOB NO. 31097

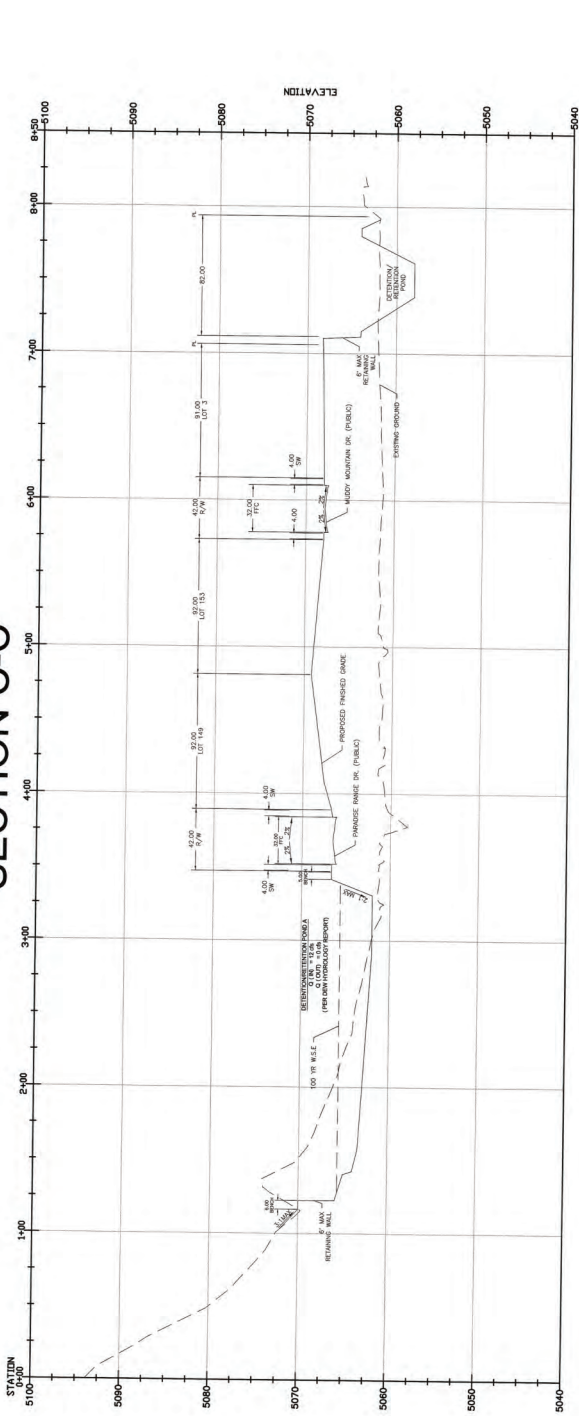


REV.	DATE	DESCRIPTION	BY	APPD.

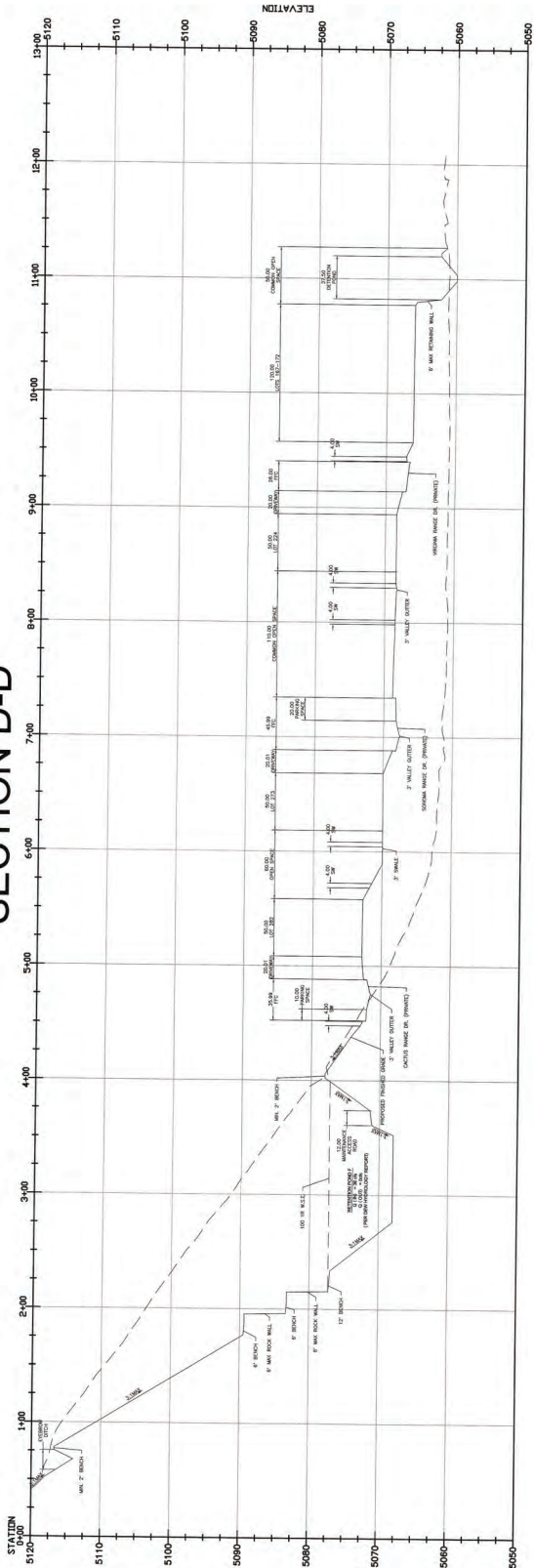
DESIGNED BY: RG  
 CHECKED BY: RG  
 SCALE  
 HORZ: N.T.S.  
 VERT:  
 JOB NO: 31087



**SECTION C-C'**



**SECTION D-D'**











July 7, 2021

Dan Cahalane  
Washoe County Planning and Building Division  
1001 East 9<sup>th</sup> Street, Building A  
Reno, Nevada 89512

**RE: Village Parkway Tentative Map**

Dear Dan,

As discussed in our previous meetings, attached are updated plan sets for the Village Parkway Tentative Map. Overall, the design and layout of the subdivision is very similar to that of the previously submitted map. The primary change is that cuts will now occur along the western edge of the site to generate the fill material that was previously proposed to be imported. The overall unit count remains the same and amenities such as trails are very similar in scope and location.

With the proposed grading on the west side of the site a Directors Modification is requested to allow for cuts over 10 feet and slopes over 10 feet. This is reflected on the attached plans. Additionally, a completed the Director’s Modification questionnaire (completed by Summit Engineering) and application filing fee are also included as an attachment to this letter.

Proposed setbacks for the project are included on the tentative map title sheet, as requested. Also, the overall project summary table from the planning report has been updated and is included below:

<b>Village Parkway Tentative Map - Development Summary</b>	
<b>Project Component</b>	<b>Proposed with Tentative Map</b>
Project Area	124.6± acres
Development Area (HDS zoning)	47.2± acres
Townhome Units (Single Family Attached)	183 units
Detached Single Family Units	166 units
Total Units	349 units
Gross Project Density	2.8 dwelling units per acre
Net Project Density (Tentative Map Area)	7.4 dwelling units per acre
Smallest Detached Lot Size	3,645± square feet
Largest Detached Lot Size	8,257± square feet
Average Detached Lot Size	4,250± square feet
Smallest Attached Lot Size	800± square feet
Largest Attached Lot Size	1,348± square feet
Average Attached Lot Size	1,047± square feet
Total Lot Area	20.45± acres
Public Right-of-Way Area	6.57± acres
Common Area <sup>1</sup>	97.58± acres

<sup>1</sup> – includes private roadway area.

The table demonstrates that the overall project statistics and design is virtually identical to the previously submitted map. The only true change is to the grading design, as detailed on the attached plans.

Please do not hesitate to contact me at [mike@christynv.com](mailto:mike@christynv.com) or (775) 250-3455 with any questions or concerns. Thank you for your ongoing assistance with the project.

Sincerely,

A handwritten signature in black ink, appearing to read "Mike Railey". The signature is fluid and cursive, with the first name "Mike" being more prominent than the last name "Railey".

Mike Railey  
Planning Manager

cc: Bob and Peter Lissner – Lifestyle Homes TND, LLC  
Robert Gelu, P.E. – Summit Engineering Corporation

**SOLAEGUI**  
ENGINEERS

April 13, 2021

Mitchell Fink, P.E.  
Washoe County Community Development  
P.O. Box 11130  
Reno, Nevada 89520

**Re: Village Parkway Residential – Trip Generation Letter**

Dear Mitch:

This letter contains the findings of our trip generation review of the proposed Village Parkway Residential development project located on the west side of Village Parkway north of Cold Springs Drive in Washoe County, Nevada. We completed the original traffic study on November 2, 2020. Subsequent to our analysis the project the site plan was modified and the unit mix changed. The original study was based on 428 residential dwelling units with 385 of them being attached units plus 43 single family detached. The application was submitted showing a total of 347 dwelling units with 166 single family detached homes and 183 attached units. The new project site plan is attached. The purpose of this letter is to document the trip generation attributable to the new site plan with a comparison against the original unit mix.

Trip generation calculations for the project are based on the Tenth Edition of *ITE Trip Generation*, published by the Institute of Transportation Engineers. The calculation sheets are attached for ITE land use #210 Single Family Detached Housing and #220 Multifamily Detached Housing. Table 1 shows trip generation totals for the initial and current unit mix.

TABLE 1  
TRIP GENERATION

<u>LAND USE</u>	<u>ADT</u>	<u>AM PEAK HOUR TOTAL</u>	<u>PM PEAK HOUR TOTAL</u>
Original Report			
Single Family Detached Housing			
43 Dwelling Units	478	35	45
Low Rise Multifamily Housing			
385 Dwelling Units	2,870	172	196
Subtotal 428 Dwelling Units	3,348	207	241
Updated Site Plan			
Single Family Detached Housing			
166 Dwelling Units	1,567	123	165
Low Rise Multifamily Housing			
183 Dwelling Units	1,340	84	101
Subtotal 349 Dwelling Units	2,907	207	266
Change with Updated Plan -79DU	-441	0	+25



As indicated in Table 1, the original traffic report showed trip generation totals including 3,348 average daily trips with 207 AM peak hour trips and 241 PM peak hour trips. The updated site plan trip generation totals include 2,907 average daily trips with 207 AM peak hour trips and 266 PM peak hour trips. These totals when compared to the original traffic report are 441 less average daily trips with the same number during the AM peak hour period and 25 more trips during the PM peak hour. The PM peak hour is the only time period of increased trips and the change is only a 10 percent change. A copy of the Regional Transportation Commission comment letter is attached. It noted these totals. They characterized the report recommendations as still being valid. We concur with that description.

We trust that this information will be helpful to you. Please contact us if you have questions or comments.

Very truly yours,  
SOLAEGUI ENGINEERS LTD  
PAUL W.  
SOLAEGUI  
CIVIL P.E.  
No. 7163  
STATE OF NEVADA  
REGISTRATION



4-13-21  
EXP 6-30-22

Enclosures  
Letters/ Village Parkway Residential Trip Generation Letter







# Single-Family Detached Housing (210)

**Vehicle Trip Ends vs: Dwelling Units**  
**On a: Weekday**

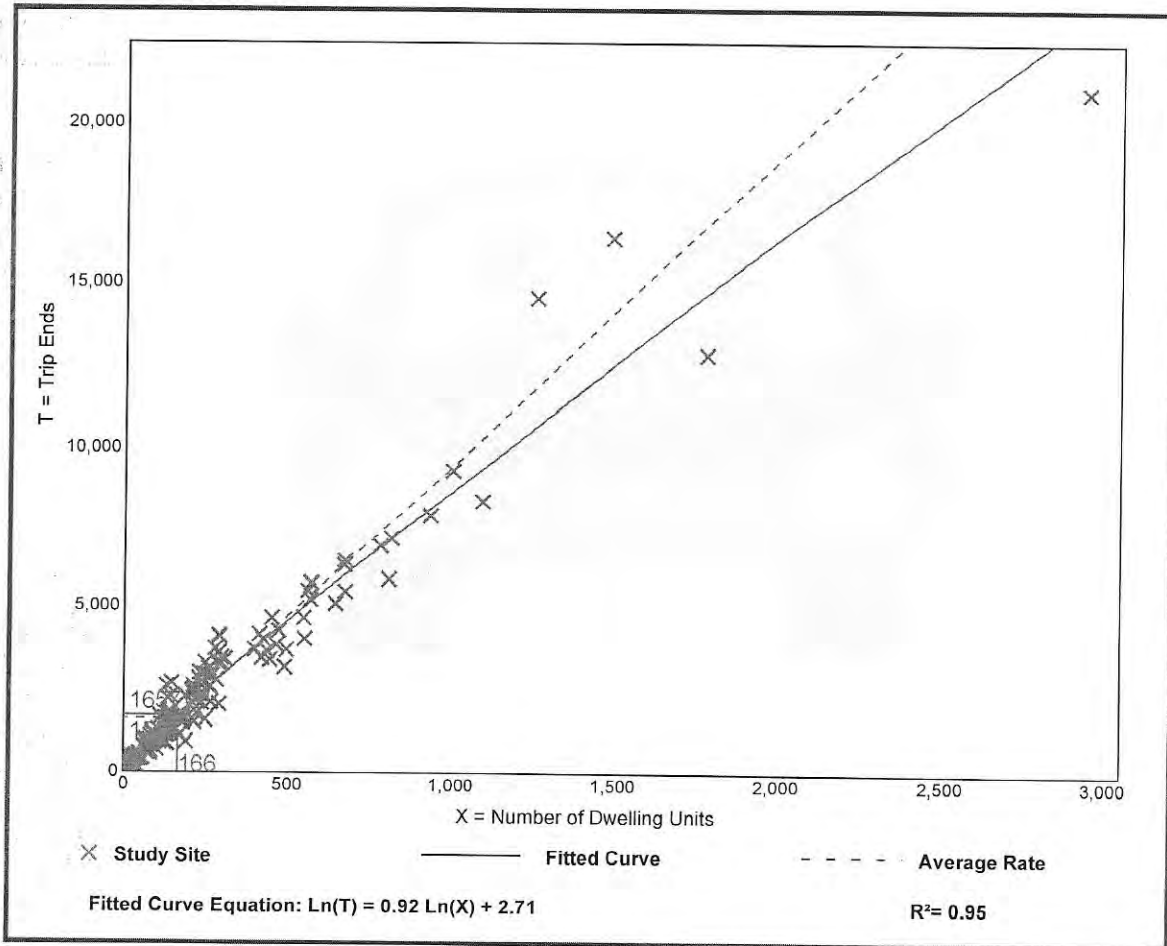
**Setting/Location: General Urban/Suburban**

Number of Studies: 159  
Avg. Num. of Dwelling Units: 264  
Directional Distribution: 50% entering, 50% exiting

## Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
9.44	4.81 - 19.39	2.10

## Data Plot and Equation



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## Single-Family Detached Housing (210)

**Vehicle Trip Ends vs: Dwelling Units**  
**On a: Weekday,**  
**Peak Hour of Adjacent Street Traffic,**  
**One Hour Between 7 and 9 a.m.**

**Setting/Location: General Urban/Suburban**

Number of Studies: 173

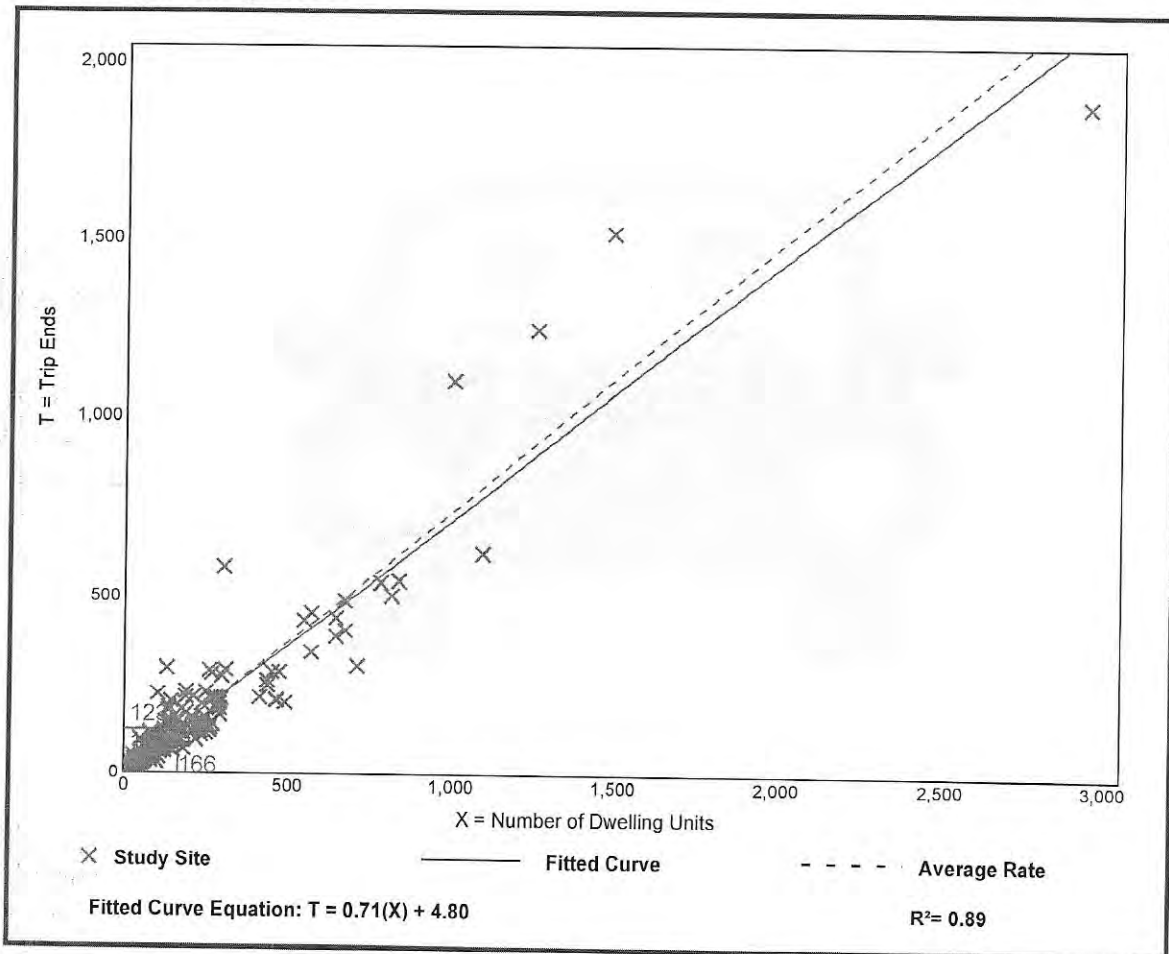
Avg. Num. of Dwelling Units: 219

Directional Distribution: 25% entering, 75% exiting

### Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.74	0.33 - 2.27	0.27

### Data Plot and Equation



## Single-Family Detached Housing (210)

**Vehicle Trip Ends vs: Dwelling Units**  
**On a: Weekday,**  
**Peak Hour of Adjacent Street Traffic,**  
**One Hour Between 4 and 6 p.m.**

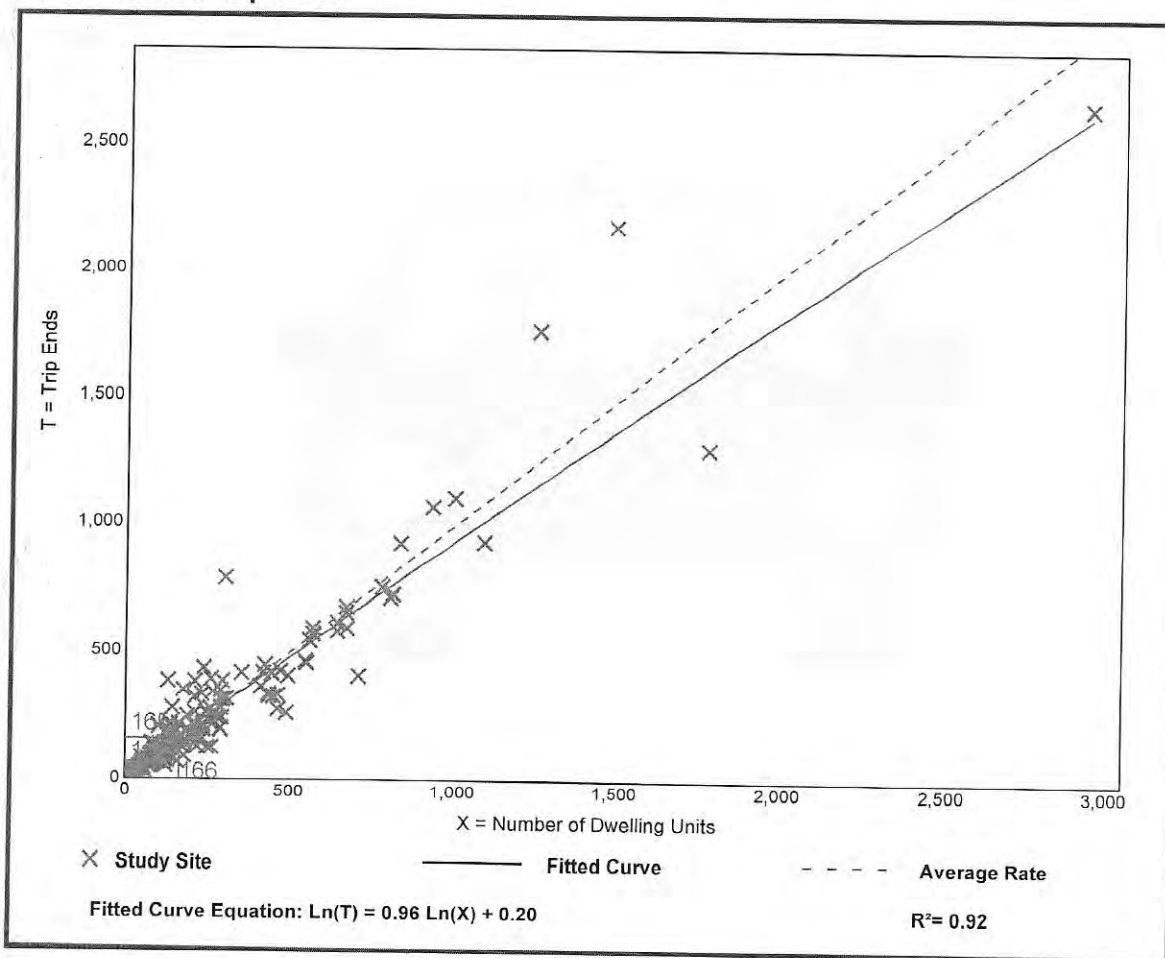
**Setting/Location: General Urban/Suburban**

Number of Studies: 190  
 Avg. Num. of Dwelling Units: 242  
 Directional Distribution: 63% entering, 37% exiting

### Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.99	0.44 - 2.98	0.31

### Data Plot and Equation



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## Multifamily Housing (Low-Rise) (220)

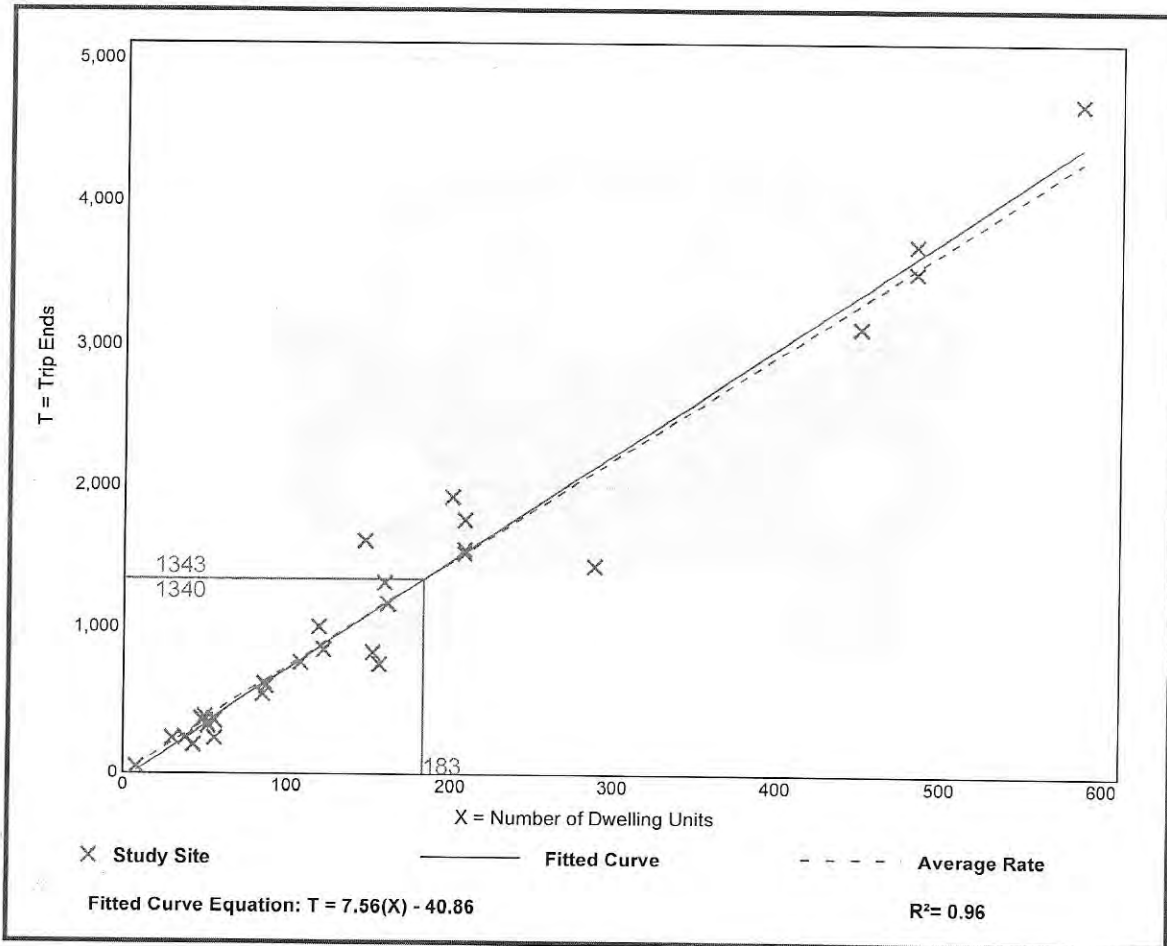
**Vehicle Trip Ends vs: Dwelling Units**  
**On a: Weekday**

**Setting/Location: General Urban/Suburban**  
Number of Studies: 29  
Avg. Num. of Dwelling Units: 168  
Directional Distribution: 50% entering, 50% exiting

### Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
7.32	4.45 - 10.97	1.31

### Data Plot and Equation



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## Multifamily Housing (Low-Rise) (220)

**Vehicle Trip Ends vs: Dwelling Units**  
**On a: Weekday,**  
**Peak Hour of Adjacent Street Traffic,**  
**One Hour Between 7 and 9 a.m.**

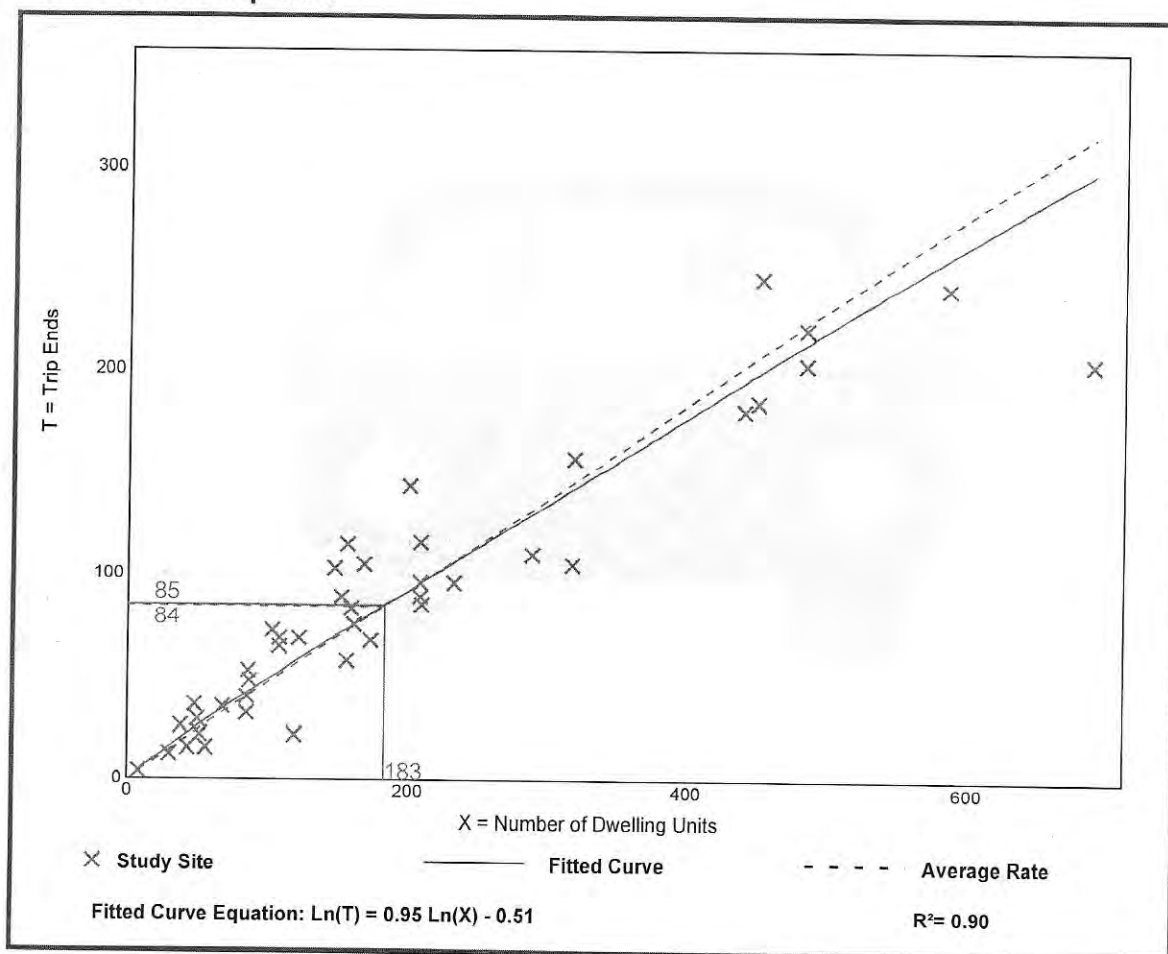
**Setting/Location: General Urban/Suburban**

Number of Studies: 42  
 Avg. Num. of Dwelling Units: 199  
 Directional Distribution: 23% entering, 77% exiting

### Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.46	0.18 - 0.74	0.12

### Data Plot and Equation



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## Multifamily Housing (Low-Rise) (220)

Vehicle Trip Ends vs: Dwelling Units  
On a: Weekday,  
Peak Hour of Adjacent Street Traffic,  
One Hour Between 4 and 6 p.m.

Setting/Location: General Urban/Suburban

Number of Studies: 50

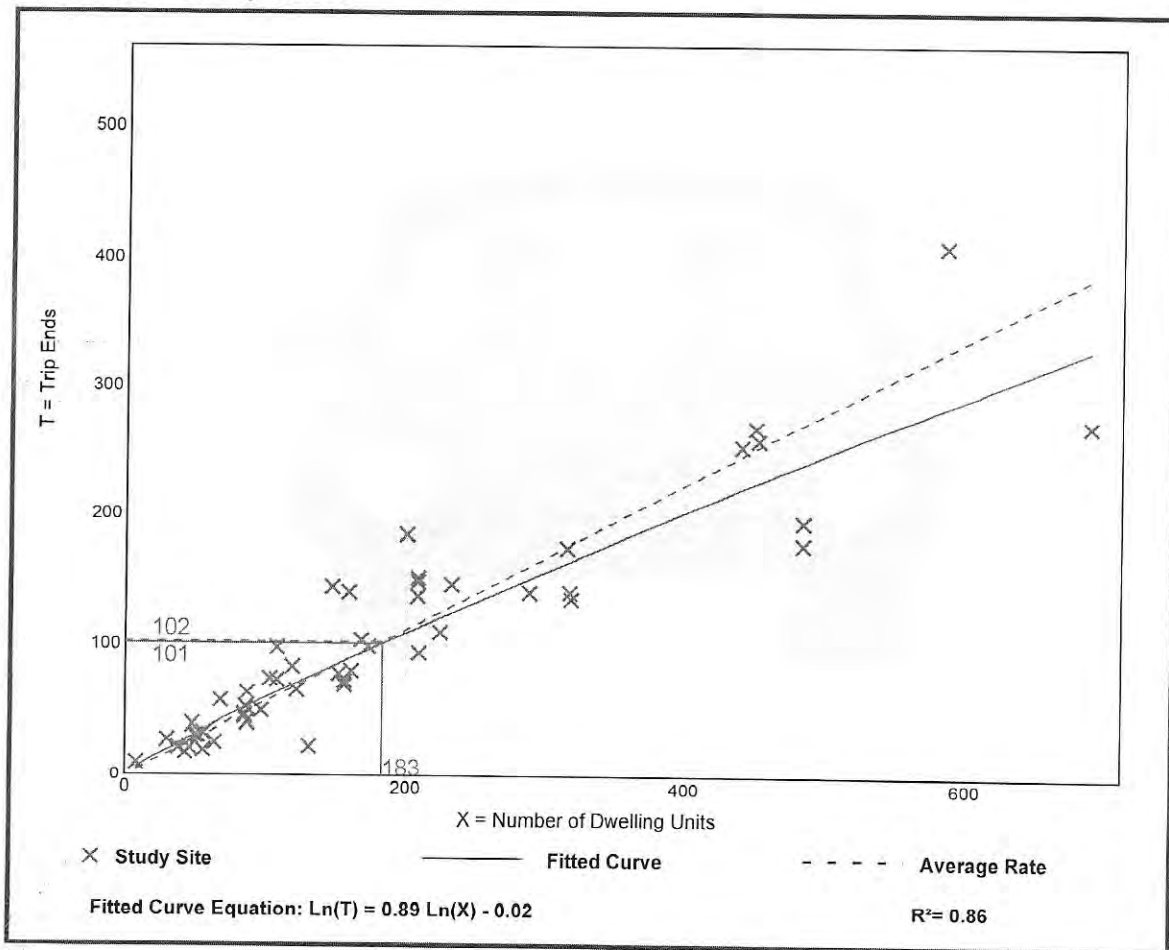
Avg. Num. of Dwelling Units: 187

Directional Distribution: 63% entering, 37% exiting

### Vehicle Trip Generation per Dwelling Unit

Average Rate	Range of Rates	Standard Deviation
0.56	0.18 - 1.25	0.16

### Data Plot and Equation



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**REGIONAL TRANSPORTATION COMMISSION**

*Metropolitan Planning • Public Transportation & Operations • Engineering & Construction*

Metropolitan Planning Organization of Washoe County, Nevada

March 26, 2021

FR: Chrono/PL 181-21

Mr. Dan Cahalane, Planner  
Community Services Department  
Washoe County  
PO Box 11130  
Reno, NV 89520

Dear Mr. Cahalane,

RE: WTM21-007 (Village Parkway)

The Regional Transportation Commission (RTC) has reviewed this request to approve a tentative map for 166 detached single-family dwelling units and 183 attached single-family dwelling units in a common open space subdevelopment, and major grading permit for the proposed tentative map. This project is planned for the west side of Village Parkway, north of Cold Springs Drive.

The project site access is located on Village Parkway, a regional road, identified by the 2050 Regional Transportation Plan (RTP) as an Arterial with moderate access control. New accesses on Village Parkway should be designed to meet the criteria outlined in the table below.

Access Management Standards-Arterials <sup>1</sup> and Collectors							
Access Management Class	Posted Speeds	Signals Per Mile and Spacing <sup>2</sup>	Median Type	Left From Major Street? (Spacing from signal)	Left From Minor Street or Driveway?	Right Decel Lanes at Driveways?	Driveway Spacing <sup>3</sup>
Moderate Access Control	40-45 mph	3 or less Minimum spacing 1590 feet	Raised or painted w/turn pockets	Yes 500 ft. minimum	No, on 6 or 8-lane roadways w/o signal	Yes <sup>4</sup>	200 ft./300 ft.

<sup>1</sup> On-street parking shall not be allowed on any new arterials. Elimination of existing on-street parking shall be considered a priority for major and minor arterials operating at or below the policy level of service.

<sup>2</sup> Minimum signal spacing is for planning purposes only; additional analysis must be made of proposed new signals in the context of planned signalized intersections, and other relevant factors impacting corridor level of service.

<sup>3</sup> Minimum spacing from signalized intersections/spacing other driveways.

<sup>4</sup> If there are more than 60 inbound, right-turn movements during the peak-hour.

The application requests to approve a tentative map for 166 detached single-family dwelling units and 183 attached single-family dwelling units. Though the number and type of units evaluated in the applicant's traffic study does not match the number and type of units proposed in the application, the overall trip generation for the number proposed in the application is largely the same as shown in the traffic study. Therefore, the recommendations/mitigations provided in the traffic study are still valid. The proposed 166 detached single-family units and 183 attached single-family units are anticipated to generate approximately 2907 daily trips, 207 AM peak hour trips, and 266 PM peak hour trips.

The policy Level of Service (LOS) standard for Village Parkway and White Lake Parkway is LOS D. Intersections shall be designed to provide a level of service consistent with maintaining the policy level of service of the intersecting corridor. This project should be required to complete roadway improvements necessary to maintain policy LOS standards. The traffic study shows that the intersection of the Project Access/ Village Parkway will operate at LOS B or better in the 2040 Plus Project Scenario with the construction of a 340' exclusive northbound to westbound left turn lane on Village Parkway. **The applicant should be required to construct this left turn lane and any necessary accompanying improvements on Village Parkway as a condition of approval.** The traffic generated by the project will also impact the intersection of regional roadways Village Parkway and White Lake Parkway. The applicant's traffic study shows that with no improvements, the intersection will operate at LOS C or better in the 2040 Plus Project Scenario, which meets the policy level of service of LOS D.

The applicant should assess the available stopping and intersection sight distance at the proposed project access intersections using guidelines provided in AASHTO's Policy on Geometric Design of Highways and Streets (Green Book). Landscaping and buildings should be placed so that clear sight triangles are provided.

It is recommended that this development be required to provide a 10-space Park-n-Ride near the entrance of the development. This is a way to promote and encourage carpooling and vanpooling to the residents and it is beneficial to help reduce air pollution and traffic congestion. For information on the Smart Trips program, please contact Scott Miklos, Trip Reduction Analyst at 775-3535-1920 or email [smiklos@rtcwashoe.com](mailto:smiklos@rtcwashoe.com).

The RTP, RTC Bicycle/Pedestrian Master Plan and the Nevada Department of Transportation Pedestrian Safety Action Plan, all indicate that new development and re-development will be encouraged to construct pedestrian and bicycle facilities, internal and/or adjacent to the development, within the regional road system. In addition, these plans recommend that the applicant be required to design and construct any sidewalks along the frontage of the property in conformance with the stated ADA specifications.

Thank you for the opportunity to comment on this application. Please feel free to contact me at 775-332-0174 or email me at [rkapuler@rtcwashoe.com](mailto:rkapuler@rtcwashoe.com) if, you have any questions or comments.

Sincerely,



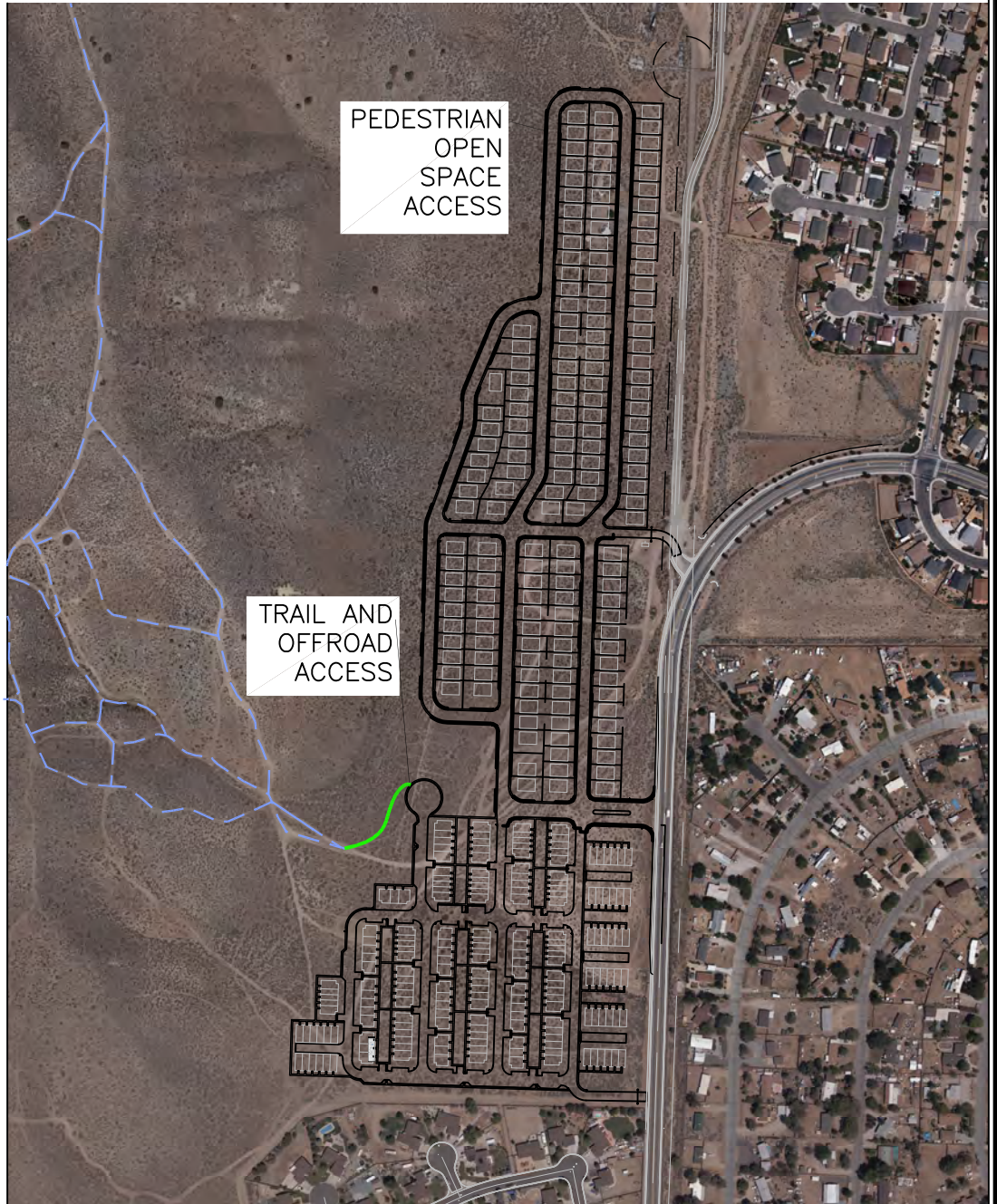
Rebecca Kapuler  
Senior Planner

CC: Dale Keller, Regional Transportation Commission  
Blaine Petersen, Regional Transportation Commission,  
Sara Going, Regional Transportation Commission  
Tina Wu, Regional Transportation Commission  
Andrew Jankayura, Regional Transportation Commission  
Scott Miklos, Regional Transportation Commission  
Alex Wolfson, Nevada Department of Transportation



LEGEND

- - - EXISTING TRAIL
- PROPOSED TRAIL



VILLAGE PARKWAY  
TOWN HOMES  
TRAIL MAP

SCALE: N.T.S.

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**SUMMIT** ENGINEERING CORPORATION  
5405 MAE ANNE AVENUE, RENO, NV. 89523  
PHONE: (775) 747-8550 FAX: (775) 747-8559

SHEET  
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# Director's Modification of Standards Supplemental Information

(All required information may be separately attached)

1. What modification or deviation are you requesting? **Be specific.**

Cuts over 10', slopes over 10' in height with the use of retaining walls and benches.

2. Why is the modification or deviation necessary to the success of the project/development? **Be specific.** Are there any extenuating circumstances or physical conditions on the proposed project/development site?

The cuts and slopes are necessary to provide the required retention volume for the project.

3. Are you proposing to mitigate the effect of the modification or reduction?

The cut material will be used onsite to balance earthwork. Meetig all requirements of 110.438.45 (c)(1)(i) through (v).

4. What section of code are you requesting to modify or deviate? **Be specific.** List the code section and if there are specific requirements for the modification, provide detailed information. For deviation, provide the percentage of the deviation.

Meeting all requirements of 110.438.48(c)(1)(i) through (v).

5. For Minor Deviation request; list what properties/parcels are affected by the deviation? Explain if there will be any impacts to the affected neighboring properties. (At a minimum, affected property owners are those owners of parcels that immediately abut the location of the proposed minor deviation.)

N/A